# Schaft Creek Project Prediction of Metal Leaching and Acid Rock Drainage, Phase 1 

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## P.Geo. and A.Sc.T. Notice

This study is based on detailed technical information interpreted through standard and advanced chemical and geoscientific techniques available at this time. As with all geoscientific investigations, the findings are based on data collected at discrete points in time and location. In portions of this report, it has been necessary to infer information between and beyond the measured data points using established techniques and scientific judgement. In our opinion, this report contains the appropriate level of geoscientific information to reach the conclusions stated herein.

This study has been conducted in accordance with British Columbia provincial legislation as stated in the Engineers and Geoscientists Act and in the Applied Science Technologists and Technicians Act.

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## Executive Summary

This first-phase report predicts metal leaching (ML) and acid rock drainage (ARD) at Copper Fox Metal’s Schaft Creek Project. As specified in the British Columbia Policy, Guidelines, and draft Prediction Manual, ML-ARD predictions are being developed in phases, with each phase focussing on resolving uncertainties identified in earlier phases. It is too early at this stage to reach any major or clear conclusions about ML-ARD potential.

In this first phase of ML-ARD testing, 59 samples of core rejects from the 2005 drilling program were submitted for expanded Sobek (EPA 600) acid-base accounting and for total-element analyses. Some major observations were:

- Previous observations of weathered core reported little evidence of oxidation and reaction.
- Schaft Creek rock contains abundant aluminosilicate minerals, which can provide some neutralization in addition to carbonate minerals.
- Based on the 59 core samples and generic criteria, only $0-2 \%$ of the samples were net acid generating and $5-14 \%$ were currently "uncertain", and thus most samples were net neutralizing. Additional testwork is needed to resolve the ARD status of the uncertain samples, and to examine other portions of the deposit.
- Although up to $2 \%$ of samples were net acid generating, none were acidic at the time of analysis, and years to decades may have to pass before they became acidic.
- Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so additional testwork is needed on metal leaching.

Recommendations were offered to improve the accuracy and to reduce the uncertainty in the current ML-ARD predictions for the Schaft Creek Project.

## Report Summary

Whenever mined rock is exposed to air and moisture, the rates of weathering, oxidation, and leaching can accelerate. If sulphide minerals like pyrite are exposed, the oxidation will release acidity, some metals, sulphate, and heat. If the acidity is not neutralized by minerals like calcite or feldspar in the rock, the resulting acidic water is called "acid rock drainage" (ARD) in British Columbia. Whether sulphide minerals are present or not, weathering can still lead to accelerated metal leaching (ML). For example, the simple dissolution of carbonate minerals can release metals like manganese.

The provincial ML-ARD Policy, Guidelines, and draft Prediction Manual contain the recommendations and the expectations of the government for ML-ARD prediction and control. One recommendation is that ML-ARD studies are carried out in phases, with each phase focussing on the uncertainties identified in the previous ones.

This report contains the first phase of ML-ARD studies for the Schaft Creek Project. Previous relevant information was compiled. Also, 59 samples of core rejects, from 11 holes drilled in 2005, were collected from cold storage. This set included two duplicates for QA/QC checks. All 59 samples were analyzed for expanded Sobek (EPA 600) acid-base accounting, and for totalelement contents using ICP-MS after four-acid digestion and using x-ray fluorescence whole rock.

## Previous Information

The compilation of existing information relevant to ML-ARD led to the following important observations.

- The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as a porphyry copper deposit. It contains three mineral zones: the Liard, West Breccia, and Paramount Zones.
- During an examination of existing core, "It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering." Thus, the oxidation rate of Schaft Creek rock may be relatively slow.
- Based on 16 acid-base accounts from a previous, metallurgical study, all 16 samples were net acid neutralizing, with sulphide between 0.1 and $0.9 \%$ S, and Neutralization Potentials from 53 to $114 \mathrm{~kg} / \mathrm{t}$. Flotation recovery of sulphide reduced the sulphide levels in the synthetic tailings.
- Detailed mineralogy was examined in 18 thin sections, representing feldspar quartz porphyry (rock code PPFQ), tourmaline breccia, pneumatolytic breccia, and volcanics. Even one rock unit (PPFQ) was not entirely intrusive. Some PPFQ samples were porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic), and one sample was a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar. Groundmass in these samples was generally around one-half of the
total, with the groundmass consisting of more than $90 \%$ feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, and opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified and were sometimes seen as feldspar replacement/alteration.


## Results of Acid-Base Accounting (ABA)

As part of the ABA procedure, paste pH is measured in a mixture ("paste") of pulverized sample and deionized water. Paste pH in the 59 core samples for Schaft Creek ranged from 7.6 to 8.6. Thus, no samples were acidic at the time of analysis.

Total sulphur in the 59 Schaft Creek rock samples ranged from 0.02 to $1.91 \%$ S, with a mean of $0.45 \%$ S and a median of $0.26 \%$ S. In most samples, total sulphur and sulphide were similar, and thus the two parameters were typically interchangeable. Because a few samples did contain elevated leachable sulphate, sulphide is a better indicator of acid potential than total sulphur for Schaft Creek rock. However, in many samples, most sulphide was copper-bound sulphide (chalcopyrite) which may have less capacity to generate acidity. Therefore, each sample has a maximum "worst-case" Sulphide-Based Acid Potential (SAP) and a minimum "best-case" Pyrite-Calculated Acid Potential (PAP).

Sobek (EPA 600) Neutralization Potential (NP) ranged from 40 to $219 \mathrm{~kg} / \mathrm{t}$ in the 59 Schaft Creek samples, with a mean of 97 and a median of $92 \mathrm{~kg} / \mathrm{t}$. These are relatively high values. They explain why no acidic paste pH values were detected, and suggest there could be a long lag time (years to decades) before these samples might become acidic. A certain amount of measured NP is typically "unavailable" for neutralization, and thus should be subtracted from measured values. The lack of acidic paste pH values precluded an initial estimate of Unavailable Neutralization Potential, so the common value of $10 \mathrm{~kg} / \mathrm{t}$ is used here. NP was typically greater than inorganic carbonate in many samples, meaning NP also reflected the presence of non-carbonate aluminosilicate minerals. These minerals have been documented in Schaft Creek rock. Also, NP did not correlate well with solid-phase calcium plus magnesium levels, but some samples showed that calcium-bearing minerals could account for their NP levels.

Best-case and worst-case net balances of acid-generating and acid-neutralizing capacities were calculated for each of the 59 Schaft Creek samples. Overall, only $0-2 \%$ of the samples were net acid generating and $5-14 \%$ were "uncertain" based on generic criterion. Thus, most samples were net neutralizing. PPAU and PPFQ were the major rock units with uncertain samples, while net-acid-generating or uncertain samples were found in the minor rock units of ANDS, TOBR, BRIV, and DIOR.

To generally assess the spatial distribution of net balances, a general east-west cross-section showed the center area was net-neutralizing, while net-acid-generating and uncertain samples were found on the periphery. The general north-south cross-section showed uncertain samples were found in three adjacent holes. Based on this limited information, the net-acid-generating and
uncertain samples may be spatially restricted in the Schaft Creek Deposit, but additional samples and geostatistical modelling are needed to confirm this.

## Results of Total-Element Analyses

Total-element levels in the 59 Schaft Creek samples were measured by ICP-MS analysis after strong four-acid digestion and by x-ray-fluorescence whole-rock analysis. The 59 samples of Schaft Creek core were predominantly composed of silicon and aluminum, reflecting the abundant aluminosilicate minerals. Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were also relatively abundant. Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so additional testwork is needed on metal leaching. Only copper showed some correlation with sulphide, reflecting the copper-bound sulphide discussed under Acid-Base Accounting. For Sobek Neutralization Potential, calcium showed some correlation. Samples of some rock units, particularly tourmaline breccia (TOBR), stood out as a distinct group for some elements like gallium, phosphorus, thallium, tungsten, and uranium.

## Recommendations for Future ML-ARD Work

A phased approach, with each focussing on resolving uncertainties raised in previous ones, is recommended in the provincial ML-ARD Prediction Manual. Thus, based on the preceding initial information, we offer the following recommendations for the next phase of ML-ARD studies at the Schaft Creek Project.

- Overburden should be analyzed for ML-ARD potential. Up to several tens of meters of overburden have been reported in drillholes. This overburden in the pit area would be disturbed and oxidized during mining, and might be used for reclamation during and after operation.
- Unavailable Neutralization Potential (UNP) could not be reliably estimated from available data (Section 4.1.3), but affects net balances. Therefore, UNP should be determined better for Schaft Creek. This would likely require humidity cells (see below).
- Most samples with NPR < 2 were between 1.0 and 2.0, meaning their ARD potential is "uncertain" at this time (Section 4.1.5). This uncertain range should be resolved for proper planning of waste management and water management. Humidity cells would help with this (see next recommendation).
- Six laboratory-based kinetic tests, known as humidity cells, should be conducted for at least 40 weeks on $1-\mathrm{kg}$ samples of Schaft Creek rock. These would provide bulk rates of acid generation, neutralization, and metal leaching, and would help in resolving UNP and "uncertain" samples (see above). Previous information on weathered core suggested reaction rates in Schaft Creek rock were low.
- Four on-site leach tests, each containing up to approximately one tonne of disturbed rock or broken core, should be set up at Schaft Creek and periodically sampled as part of routine on-site water-quality monitoring. These would provide on-site drainage-chemistry data and are important for upscaling the smaller-scale humidity cells.
- At this time, the net-acid-generating and "uncertain" samples may be clustered in portions of the deposit, which would focus waste management and any special handling onto specific zones. To examine this clustering further, additional core samples, including 2006 holes, should be collected from across the deposit and submitted for expanded acid-base accounting and totalelement contents. The results would be used in geostatistical modelling (see next recommendation).
- Three-dimensional geostatistical modelling should be carried out to calculate total tonnages and year-by-year tonnages of net-acid-generating, currently "uncertain", and net-neutralizing rock. This is important for identifying the most cost-effective options for waste management and water management.


## 1. INTRODUCTION

Whenever mined rock is exposed to air and moisture, the rates of weathering, oxidation, and leaching can accelerate. If sulphide minerals like pyrite are exposed, the oxidation will release acidity, some metals, sulphate, and heat. If the acidity is not neutralized by minerals like calcite or feldspar in the rock, the resulting acidic water is called "acid rock drainage" (ARD) in British Columbia.

Whether sulphide minerals are present or not, weathering can still lead to accelerated metal leaching (ML). For example, the simple dissolution of carbonate minerals can release metals like manganese.

ML-ARD is often associated with minesites, where it is well documented (e.g., Morin and Hutt, 1997 and 2001). As a result, the accurate prediction and control of ML-ARD at minesites in British Columbia are high priorities of the provincial government, as explained in its formal Policy, Guidelines, and draft Prediction Manual (Price and Errington, 1998; Price, 1998; Price et al., 1997). This report follows the recommendations of those documents.

Because the provincial documents recommend a phased approach, this report compiles and interprets the currently existing information related to ML-ARD at the Schaft Creek Project. General background information is provided in Chapter 2. The ML-ARD samples, and the static analyses applied to them, are described in Chapter 3. The analytical results are discussed in Chapter 4. Chapter 5 concludes with recommendations for the next phase of ML-ARD work, including additional testwork as discussed in the provincial Prediction Manual. All relevant data are compiled in the appendices.

## 2. GENERAL INFORMATION AND PREVIOUS ML-ARD-RELATED STUDIES

The information presented below has been extracted mostly from the Project Description (Copper Fox Metals Ltd., 2006), a resource estimate by Giroux and Ostensoe (2003), and the 2005 drilling report (Fischer and Hanych, 2006).

### 2.1 Location and History

The Schaft Creek property is located in the mountainous terrain of northwestern British Columbia, approximately $1,000 \mathrm{~km}$ northwest of Vancouver. The area is located 80 kilometers southwest of Telegraph Creek and approximately 76 kilometers west of the Stewart-Cassiar paved highway (Highway 37). The mineral claims of interest are situated near the headwaters of Schaft Creek, a tributary of Mess Creek, which flows into the Stikine River downstream of the community of Telegraph Creek.

Schaft Creek is located in the coastal climate zone of British Columbia and is characterized by cool summers and cold humid winters. Elevations on the property range from 500 to $2,000 \mathrm{~m}$ above sea level. Average annual precipitation is estimated to be 640 mm or roughly $84 \%$ greater than that recorded at Telegraph Creek. Temperatures are strongly influenced by the Coast Mountains and may range from above $+20^{\circ} \mathrm{C}$ in the summer to below $-20^{\circ} \mathrm{C}$ in winter.

The Schaft Creek copper-gold-molybdenum-silver prospect was identified in 1957 by prospector Nick Bird while employed by the BIK Syndicate. Three diamond drill holes were drilled to moderate depths. Sample results from two of the holes returned sufficient copper values and resulted in further work. The prospecting syndicate was re-organized in 1966 into Liard Copper Mines Ltd. (" Liard") with Silver Standard Mines Limited, holding a 66\% interest, acting as the manager. In 1966 ASARCO obtained an option to explore the Liard Copper Mines Ltd. ground and carried out geological and induced polarization surveys. The program included drilling 10,939 feet (3,335 metres) over 24 holes. The option was not maintained despite encouraging drill results and in 1968 Hecla Mining Company of Canada Ltd., a subsidiary of Hecla Mining Company of Wallace, Idaho, entered an option agreement to earn a $75 \%$ property interest and commenced drilling and other exploration work with Hecla operating company as its agent.

From 1968 through 1977, Hecla completed a total of 34,500 metres of diamond drilling, 6,500 metres of percussion drilling, induced polarization and resistivity surveys, geological mapping, air photography, and engineering studies related to the development of a large open pit copper-gold-molybdenum mine. In 1978 Wright Engineers Ltd. was contracted by Hecla to update a preliminary feasibility assessment initially completed in 1970. Exploration work at the property ceased in 1977 and in 1978 Hecla sold its interest to Teck Corporation ("Teck") (now Teck Cominco Limited).

In 1980 Teck commenced a program of exploration and drilling designed to confirm and expand Hecla's work. A total of 26,000 metres of diamond drilling was completed by 1981. Teck then undertook an engineering study to determine the feasibility of mine development. Further data
reviews were completed by Western Copper Holdings in 1988 and Teck in 1993. A total of 230 core holes with a total length of 60,200 metres and percussion holes with total length 6,500 metres have been completed at the Schaft Creek property. Copper Fox Metals has completed 15 large diameter (PQWL) drill holes across the Main Liard and West Breccia zones for a total of 3,161 meters. A total of 50,000 pounds of core is presently undergoing geological assessment and reporting before metallurgical testing of this new core is initiated.

The feasibility work completed on the Schaft Creek site has been focussed on the development of an open pit within the Liard Zone. The present plan would see mining of up to 70,000 tonnes per day of ore using conventional drill and blast mining methods with a maximum estimated strip ratio of 1.13.

### 2.2 Geology

The Schaft Creek copper-gold-molybdenum property is located in the northern part of the Intermontane Belt of the Canadian Cordillera. It is part of the northwesterly trending suite of porphyry-style mineral deposits that extends in Canada from the Copper Mountain/Ingerbelle deposit near the southern International Boundary to Casino in west-central Yukon. Globally, such deposits typically exhibit a few characteristics in common and many variations.

The Schaft Creek copper-gold-molybdenum deposit is hosted principally by Upper Triassic age volcaniclastic rocks. They have been variously altered and disrupted by emplacement of feldspar porphyry dykes and, possibly, sills and by several northwest-trending faults. Augite porphyry basalt is present in proximity to the west of the deposit area and also in the Liard mineral zone but its relationship to mineralization has not been determined. The mineralized area is, arguably, in fault contact, or disconformably or unconformably overlain by unmineralized, comparatively unaltered and undisturbed purple weathering andesitic volcanic rocks. Geological mapping at surface, aided by diamond drill core information, has failed to reveal any strong overall pattern of stratigraphic or petrologic controls to mineralization.

The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. The deposit consists of three distinct but connected zones: (a) the Liard (Main) zone hosted mainly by andesite flows and epiclastic rocks; (b) the West Breccia zone, a faultbounded tourmaline-sulphide matrix breccia; and (c) the Paramount zone, an intrusive breccia in altered andesite, granodiorite and quartz monzonite.

The broad, northerly plunging Liard, or Main, zone extends 1,000 metres in a northerly direction, 700 metres east-west, and has average thickness of 300 metres. It is a weakly altered stockwork system in volcanics (andesite flows and fragmentals) with minor felsic intrusive dykes carrying disseminated sulphide mineralization. A pyrite halo surrounds chalcopyrite, bornite and molybdenite mineralization in altered and faulted andesite. The zone has a low grade phyllic core and to the northwest is progressively down dropped on faults.

The West Breccia zone exhibits tourmaline, silicification and sericitization and is controlled by north-trending faults. Mineralization is contained within tourmaline and sulphide rich hydrothermal breccia. The Zone has a length of 500 metres, averages 100 metres in width and has been drilled to depths greater than 300 metres. Pyrite is the principal sulphide mineral, with lesser quantities of chalcopyrite and molybdenite. Copper and molybdenum contents are erratic but often high.

The Paramount zone of intrusive breccia occurs in granodiorite and quartz monzonite and has dimensions of 700 metres length, 200 metres width and +500 metres thickness. Exploration to the north has been constrained by practical considerations: rapidly increasing thicknesses of overlying apparently barren purple volcanic rocks challenge drilling methods and mitigate against practical conceptual open pit designs. The mineralization is contained in an intrusive breccia in altered andesite, granodiorite and quartz monzonite. Pyrite, bornite and chalcopyrite are present in equal proportions and molybdenite values exceed those found in the other two zones.

Additional information comes from the provincial Minfile website (http://minfile.gov.bc.ca/ Summary.aspx?minfilno=104G++015):
"Mineralization occurs partly within a basin-like structure of fragmental and undivided green andesites, 900 metres in diameter. The basin is intruded by augite porphyry basalt and by vertical north striking quartz diorite dykes. A breccia cuts the western edge of the basin and trends north for at least 2700 metres. Post-mineralization mafic dykes are common. Later flat-lying fragmental purple andesites unconformably overlie the northeastern part of the deposit.
"In general, pyrite, chalcopyrite, bornite and molybdenite occur predominantly in fractured andesites. Less than 10 per cent of the mineralization occurs in felsic intrusives. Pyrite and bornite are mutually exclusive and most of the main deposit occurs within the bornite zone, with pyrite on the periphery. A barren zone, which contains no sulphides, conformably underlies the main deposit.
"Feldspathization and hydrothermal alteration are associated with mineralization. A quartz vein stockwork with biotite and some potassium feldspar coincides with the low-grade core of the main deposit. The biotite has a potassium/argon age of $182 \mathrm{Ma}+/-5 \mathrm{Ma}$. Epidote appears abruptly near the boundaries of the main deposit. Most mineralization occurs in an intermediate zone marked by chlorite- sericite alteration and the absence of epidote. Tourmaline and gypsum are locally abundant.
"The distribution of most sulphide minerals is fracture-controlled. They occur in dry fractures or combined with quartz or quartz-calcite veinlets within the andesitic volcanics. The sulphides within the felsic intrusives are usually disseminated and seem to have replaced the mafic minerals. Trace amounts of covellite, chalcocite, tetrahedrite and native copper have been identified. Minor amounts of galena and sphalerite occur in the breccia zone and in small calcite veins. Gold and silver are associated with the sulphides and average 0.34
grams per tonne and 1.71 grams per tonne, respectively."

### 2.3 Past ML-ARD-Related Work

During an examination of existing core, Associated Mining Consultants Ltd. (2004) observed, "It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering."

Also, after a visual assessment of the integrity of the core samples, Associated Mining Consultants Ltd. (2004) selected 16 samples for assay validation based on prior documentation of assays, lithology, and spatial distributions. These 16 samples selected were subjected to standard Acid-Base accounting procedures to assess any acid generation and environmental impact concerns (Table 2-1). Because only statistical summaries but no individual analyses were presented, these analyses were not added to the Phase 1 database in this study (Appendix B).

Table 2-1. Statistical Results of Previous Acid-Base Accounting for Sixteen Samples (from Associated Mining Consultants Ltd., 2004)

| Parameter | Average | Range |
| :---: | :---: | :---: |
| Sulphide (\%S) | 0.43 | $0.1-0.9$ |
| Paste pH | 8.8 | $7.5-9.3$ |
| Acid Potential (kg CaCO ${ }_{3}$ eq/tonne) | 13.4 | $3.4-28.6$ |
| Neutralization Potential ( $\mathrm{kg} \mathrm{CaCO}_{3}$ eq/tonne) | 75.5 | $53-114$ |
| Net Potential Ratio (NPR or NP/AP) | 7.36 | $3.0-16.9$ |
| Net Neutralization Potential (NP-AP, $\mathrm{kg} \mathrm{CaCO}_{3}$ eq/tonne) | +62.2 | +45 to +91 |

Then, five samples were selected from the suite of 16 for metallurgical validation using standard batch grinding and rougher flotation procedures for sulphides. The five samples selected for metallurgical validation were taken from drill holes H61, T182, T186, T172, and T176.

Based on all this work, Associated Mining Consultants Ltd. (2004) concluded,
"The mineralogy is unlikely to pose acid generation concerns based on the analysis of the 16 selected core samples. Acid-Base accounting results indicated an excess neutralization potential of over twice the estimated acid potential in all cases and the paste pH ranged from neutral to alkaline. With the low head sulphide content in the samples to start and high flotation recoveries, the total sulphur in the tailings was reduced to below $0.03 \%$ to further reduce concerns on environmental impact."

As an addendum to Fischer and Hanych (2006), mineralogy was visually determined, using thin-section petrography, on 18 samples. This work focussed on feldspar quartz porphyry (rock code PPFQ, Table 3-1), with a few samples from tourmaline breccia, pneumatolytic breccia and volcanics. It was not meant to be representative of the Schaft Creek lithologic suite. Major observations from this work follow.
"- Not all samples logged as PPFQ are intrusives. Some are porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic); one sample is a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar.

- All rocks classified as FQP [PPFQ] are porphyritic, felsic, massive igneous rocks.
- All have plagioclase as the predominant phenocryst mineral. Quartz phenocrysts ('quartz eyes') are relatively rare, very subordinate to plagioclase phenocrysts.
- A few samples have no quartz phenocrysts (quartz eyes) and therefore are feldspar porphyry.
- Ferromagnesian ('Femag') phenocrysts are consistently completely replaced by secondary minerals, generally chlorite and accessory leucoxene, opaques, in places by sericite and skeletal fine grained opaques and highly refracting brown minerals.
- The groundmass makes up a variable portion of the rock, generally $1 / 2$.
- The groundmass consists of $>90 \%$ feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques.
- The groundmass in all cases is fine grained to very fine grained, generally 100 to 200 microns ( $0.1-0.2 \mathrm{~mm}$ ) grain size, in some samples extremely fine grained (20-50 microns). Differences in grain size of the groundmass feldspar is noticeable and attributed to varying cooling rates.
- The shape of groundmass feldspar and other minerals is generally anhedral, interlocking. Lathy and feathery feldspar are rare but were observed.
- Only accessory amounts of fresh potassic feldspar (microcline) and albite were observed in some feldspar-quartz-porphyries and are interpreted as very limited, secondary, potassic alteration.
- The common pink to orange colour of the samples is attributed to ubiquitous micron-size sericite grains within plagioclase phenocrysts and to a lesser degree in groundmass feldspar. It is pointed out that 'sericite' is a synonym for fine grained muscovite which is a potassic phyllosilicate. It appears justified to describe this partial alteration as 'potassic'.
- Fast cooling of the liquid that formed the groundmass is interpreted for all Liard Zone FQP samples. This is in contrast to the grains size of the interstitial minerals in the Hickman /Yeheniko samples which are medium grained (0.3-1 mm)
- This fast cooling of the inter-phenocryst liquid can be interpreted either as due to relatively small intrusive bodies or surface-near (subvolcanic) bodies.
- Alteration is weak to moderate. Mostly sericite, minor carbonate, chlorite, rare potassic, i.e., microcline.
- Sulphides in feldspar-quartz-porphyry and volcanics occur both in veins; and as disseminations, associated with hairline fractures and grain boundaries, and with minor quartz, carbonate, chlorite and sericite.

Other observations from the individual thin sections include:

- Undifferentiated plagioclase was typically the major mineral, with fine-grained sericite and quartz often significant.
- Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite
- Pyrite was typically $0.05-1.0 \mathrm{~mm}$ in size as subhedral to anhedral grains, but variable among samples.
- Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified and were sometimes seen as feldspar replacement/alteration.


### 2.4 Important ML-ARD Observations from Previous Studies

Based on the preceding subsections, important observations pertaining to ML-ARD were:

- The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. It contains three mineral zones: the Liard, West Breccia, and Paramount Zones.
- During an examination of existing core, "It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering." Thus, the oxidation rate of Schaft Creek rock may be relatively slow.
- Based on 16 acid-base accounts from a previous, metallurgical study, all 16 samples were net acid neutralizing, with sulphide between 0.1 and $0.9 \%$ S, and Neutralization Potentials from 53 to $114 \mathrm{~kg} / \mathrm{t}$. Flotation recovery of sulphide reduced the sulphide levels in the synthetic tailings.
- Detailed mineralogy was examined in 18 thin sections, representing feldspar quartz porphyry (rock code PPFQ), tourmaline breccia, pneumatolytic breccia, and volcanics. Even one rock unit (PPFQ) was not entirely intrusive. Some PPFQ samples were porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic), and one sample was a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar. Groundmass in these samples was generally around one-half of the total, with the groundmass consisting of more than $90 \%$ feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified, and were sometimes seen as feldspar replacement/alteration.


## 3. SAMPLING AND ANALYSIS

### 3.1 Sample Selection and Collection

Based on the 2005 diamond-drillhole Report (Fischer and Hanych, 2006), the important rock units and their total footages in the core are listed in Table 3-1. Results from the 2006 drilling program were not available for this Phase 1 study, and were thus not included here.

Table 3-1. Important Rock Units and Their Observed Abundances in 2005 Drill Core (based on Fischer and Hanych, 2006)

| Rock-Unit Code | Description | Percentage of <br> Footage in 2005 Core |
| :---: | :---: | :---: |
| PPAU | Plagioclase-Augite-phyric Andesite | $32.1 \%$ |
| ANPL (and ANLP) | Andesitic Lapilli Tuff | $19.6 \%$ |
| ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | $14.4 \%$ |
| PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | $6.6 \%$ |
| ANDS | Andesite | $4.5 \%$ |
| BRVL | Volcanic Breccia | $4.4 \%$ |
| TOBR | Tourmaline Breccia | $4.2 \%$ |
| FAUL and SHER | Faults, and Shear Zone / Faults | $3.7 \%$ |
| PPPL | Plagioclase or Feldspar Porphyry | $3.0 \%$ |
| ANTF | Andesitic Tuff | $2.1 \%$ |
| BRIV | Intrusive Breccia or Felsic Igneous Breccia | $1.8 \%$ |
| D/BS | Diabase/Basic dyke | $1.5 \%$ |
| DIOR | Diorite | $1.1 \%$ |
| BRXX | Diorite Breccia | $0.6 \%$ |
| PNBX | Pneumatolytic Breccia | $0.5 \%$ |
| VN | Vein | NR |
| ANNX | Altered Andesite | NR |

Phase 1 ML-ARD sampling of the 2005 core was based on two objectives. First, approximately 60 samples would be collected to generally match the percentage abundance in the 2005 core (Table 3-2 and Appendices A and B), although ANPL was under-represented. Second, these samples would be collected from several 2005 holes, from various depths, generally within the proposed mining area (eleven holes, from 05CF234 to 05CF248) to provide three-dimensional spatial coverage.

| Rock-Unit Code | Description | Number of ML-ARD Samples (Percentage of Total) ${ }^{1}$ |
| :---: | :---: | :---: |
| PPAU | Plagioclase-Augite-phyric Andesite | 16 (27.1\%) |
| ANPL (and ANLP) | Andesitic Lapilli Tuff | 5 (8.5\%) |
| ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | 11 (18.6\%) |
| PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | 5 (8.5\%) |
| ANDS | Andesite | 4 (6.8\%) |
| BRVL | Volcanic Breccia | 2 (3.4\%) |
| TOBR | Tourmaline Breccia | 4 (6.8\%) |
| FAUL and SHER | Faults, and Shear Zone / Faults | 3 (5.1\%) |
| PPPL | Plagioclase or Feldspar Porphyry | 2 (3.4\%) |
| ANTF | Andesitic Tuff | 2 (3.4\%) |
| BRIV | Intrusive Breccia or Felsic Igneous Breccia | 1 (1.7\%) |
| D/BS | Diabase/Basic dyke | 1 (1.7\%) |
| DIOR | Diorite | 2 (3.4\%) |
| BRXX | Diorite Breccia | 0 (0\%) |
| PNBX | Pneumatolytic Breccia | 0 (0\%) |
| VN | Vein | 0 (0\%) |
| ANNX | Altered Andesite | 1 (1.7\%) |
|  | TOTAL | 59 |
| ${ }^{1}$ Total includes two duplicates: 14578B from Hole 246 of PPAU, and 14685B from Hole 245 of DIOR. |  |  |

The Paramount Zone was not sampled as part of this Phase 1 study.
Each sample was approximately a few hundred grams in weight. It was collected from the uppermost material (already ground to gravel and finer grain sizes) in a sealed plastic bucket that had been in unheated storage in Smithers. Each sample was collected with a fiberglass hand shovel, cleaned with soap and water between samples, and placed into a labelled ziploc bag. All samples were relatively dry, except three saturated and one moist (Appendix A).

Two duplicate samples were collected, with a " $B$ " suffix in Appendices A and B. These duplicate samples were taken from the bottoms of the buckets, instead of the top. Therefore, differences between these duplicates can reflect analytical inaccuracy as well as any variability within theoretically homogenized buckets.

### 3.2 Sample Analysis

Based on the provincial ML-ARD Prediction Manual (Chapter 1), the Phase 1 samples (Section 3.1) were subjected to several geochemical "static" (one-time) analyses. The 59 samples were sent to ALS Chemex Labs in North Vancouver for:

1) Chemex Package ABA-PKG05A plus C-IR07, which is standard-Sobek (U.S. EPA 600) expanded acid-base accounting (ABA), providing measured and/or calculated values of:

- paste pH in a mixture of pulverized rock and water,
- total sulphur,
- measured sulphide,
- leachable sulphate (both HCl and carbonate leach techniques),
- calculated sulphide by subtracting sulphate from total sulphur,
- barium-bound sulphate calculated from barium analyses,
- calculation of acid potentials based on sulphide levels plus any unaccounted-for sulphur (Sulphide Acid Potential, SAP),
- standard-Sobek neutralization potential (NP) by acid bath and base titration,
- inorganic carbonate for mathematical conversion to Carbonate NP (Inorg CaNP),
- total carbon for mathematical conversion to Carbonate-equivalent NP (Total CaNP),
- excess carbon calculated from the difference between total carbon and inorganic carbon,
- CaNP calculated from calcium (Ca CaNP),
- CaNP calculated from $\mathrm{Ca}+\mathrm{Mg}(\mathrm{Ca}+\mathrm{Mg} \mathrm{CaNP})$,
- various Net Neutralization Potential (NNP) balances of acid neutralizing capacities minus various acid generating capacities, and
- various Net Potential Ratio (NPR) balances of acid neutralizing capacities divided by various acid generating capacities.

2) total-element contents by:

- Chemex Package ME-MS41m: 48-element analysis after strong four-acid digestion, and
- Chemex Package ME-XRF-06: XRF (x-ray-fluorescence) whole rock for 14 elements and parameters.

Mercury was determined separately by digesting a prepared sample with aqua regia for at least one hour in a graphite heating block. After cooling, the resulting solution was diluted with demineralized water and was treated with stannous chloride to reduce the mercury. The resulting mercury was volatilized by argon purging and measured by atomic absorption spectrometry.

ABA and total-element results are compiled in Appendix B and are discussed in Chapter 4.

## 4. RESULTS OF GEOCHEMICAL STATIC TESTS

As explained in Chapter 3, 57 samples plus two duplicates from Schaft Creek core, drilled in 2005, were subjected to various geochemical static (one-time) analyses. This chapter discusses the results of those analyses, and the analyses are compiled in Appendix B.

### 4.1 Acid-Base Accounting

As explained in Section 3.2, acid-base accounting (ABA) comprises several individual analyses and calculations. The major categories are paste pH (Section 4.1.1), sulphur species and acid potentials (Section 4.1.2), neutralization potentials (Section 4.1.3), and net balances of acid potentials and neutralization potentials (Section 4.1.4).

### 4.1.1 Paste pH

Paste pH is measured in a mixture ("paste") of pulverized sample and deionized water. If samples were well weathered and oxidized before analysis, then sometimes acidic pH values are measured, meaning the samples were already generating net acidity. QA/QC data showed the initial deionized water had a pH of $6.0-6.1$, and values were reproducible to within $\pm 0.2 \mathrm{pH}$ units.

Paste pH in the 59 core samples for Schaft Creek ranged from 7.6 to 8.6 (Appendix B and Figure 4-1). Thus, no samples were acidic at the time of analysis.

### 4.1.2 Sulphur Species and Acid Potentials

Possible sulphur species that could be found in Schaft Creek rock are: sulphide including pyrite and chalcopyrite (Section 2.3), leachable sulphate like gypsum or anhydrite, and nonleachable sulphate like barite. The sum of these species theoretically equals total sulphur, although analytical inaccuracy and the existence of other sulphur species rarely yield an exact balance.

Total sulphur in the 59 rock samples ranged from 0.02 to $1.91 \%$, with a mean of $0.45 \%$ S and a median of $0.26 \%$ S (Figure $4-1$ and Appendix B). In most samples, total sulphur and sulphide were similar (Figure 4-2), with sulphide representing $87 \%$ of total sulphur on average. Thus, the two parameters were typically interchangeable. Internal blanks, internal duplicates, and the two external duplicates showed acceptable QA/QC for total sulphur and sulphide, with RPD values less than $10 \%$.

However, four samples contained more HCl -leachable sulphate than sulphide (Figure 4-3), with two from the major rock unit PPAU (Table 3-1). Carbonate-leachable sulphate, which is an alternative method, showed that only three samples contained more leachable sulphate than sulphide (Appendix B). In any case, a few percent of samples contained significant sulphate, so for better accuracy sulphide is used here instead of total sulphur to calculate acid potential.


Figure 4-1. Paste pH vs. Total Sulphur in the 59 Schaft Creek Rock Samples.


Figure 4-2. Sulphide vs. Total Sulphur in the 59 Schaft Creek Rock Samples.


Figure 4-3. HCl-Leachable Sulphate vs. Total Sulphur in the 59 Schaft Creek Rock Samples.


Figure 4-4. Sulphur Mass Imbalance vs. Total Sulphur in the 59 Schaft Creek Rock Samples.

Non-leachable sulphide as barite $\left(\mathrm{BaSO}_{4}\right)$ was calculated by assuming all barium from the ICP-MS analysis occurred as barite. This worst-case assumption showed that maximum nonleachable barium-bound sulphate would be $0.031 \%$ S with a mean of $0.01 \%$ (Appendix B). On average, non-leachable sulphide as barite was $5.4 \%$ of total sulphur and thus not a major part of the sulphur mass balance.

A QA/QC mass-balance equation for sulphur species is:
 Large negative values of $\% S\left(\mathrm{del}_{\text {actual }}\right)$ indicate the sum of sulphur species exceeds the measured total sulphur, sometimes due to analytical inaccuracy and detection limits. Large positive values indicate either (1) total sulphur was overestimated and/or (2) one or more sulphur species were underestimated. Positive values ("missing sulphur") can be added to acid-generating sulphide for safer calculations. This approach was used here for Schaft Creek rock, to calculate Sulphide-Based Acid Potentials (SAP, Section 4.1.4 and Appendix B).

Based on an allowable inaccuracy of 20\% of total sulphur, 55 of 59 samples had acceptable balances (Figure 4-4). The four samples with significant imbalances had relatively low sulphur, including the sample with the lowest total sulphur. Low sulphur levels have higher probabilities of greater inaccuracies because they are closer to detection limits. In total, 32 of 59 samples had positive values of $\% \mathrm{~S}\left(\mathrm{del}_{\text {actual }}\right)$, so this "missing sulphur" was added to sulphide as a safety factor before calculating Sulphide-Based Acid Potential (SAP, Section 4.1.4 and Appendix B).

Because sulphide minerals in Schaft Creek rock are predominantly pyrite and chalcopyrite, and chalcopyrite does not necessarily generate as much acidity as pyrite upon oxidation, it is worthwhile to separate sulphide into individual sulphide minerals. To do this with ABA and totalelement data (Section 3.2), the following steps were used.

1) Any "missing" sulphur due to mass imbalance (see \%S(del) above) was added to measured/ calculated sulphide;
2) All measured zinc was assumed to occur as sphalerite; all measured molybdenum as molybdenite; all measured mercury as cinnabar; all measured arsenic as arsenopyrite or realgar; and all measured copper as chalcopyrite or proportionally as $\mathrm{CuS}_{2}$; and
3) All the sulphide minerals from Step 2, converted to \%S, were subtracted from Step 1, to obtain calculated pyrite in \%S.
It is important to note that this approach can underestimate pyrite. It can even result in physically impossible negative pyrite concentrations due to analytical inaccuracy, detection limits, and the assumptions of the selected metals occurring only as the stated sulphides.

While several samples have more pyrite (as \%S) than copper-bound sulphide as chalcopyrite and proportionally as $\mathrm{CuS}_{2}$ (as \%S), most contain more copper-bound sulphide (Figure 4-5). In fact, most have negative amounts of pyrite. Thus, this approach is not highly reliable. Nevertheless, two different sulphide values will be used in this study to calculate acid potential.

1) The aforementioned Sulphide-Based Acid Potential (SAP) which includes positive values of $\% S\left(\operatorname{del}_{\text {actual }}\right)$ and represents the maximum ("worst case") amount of acid potential.
2) The "Pyrite-Calculated Acid Potential" (PAP) which is based only on calculated pyrite-bound
sulphide, with any value less than one-half the typical detection limit, including negative values, set at one-half the limit ( $0.005 \% \mathrm{~S}$ ); this represents the minimum ("best case") acid potential.

As a result, SAP represented the maximum ("worst case") acid potential, whereas PAP was the minimum ("best case") acid potential. Actual acid potential would be somewhere at or between these two endpoints, but additional testwork would be needed to determine this (Chapter 5).

A scatterplot of SAP and PAP showed that many samples had the low, default PAP value based on $0.005 \%$ S (Figure 4-6). A few samples had nearly equivalent values, meaning most of their sulphide was pyrite.

In summary, total sulphur in the 59 Schaft Creek rock samples ranged from 0.02 to $1.91 \%$ S, with a mean of $0.45 \%$ S and a median of $0.26 \%$ S. In most samples, total sulphur and sulphide were similar (Figure 4-2), and thus the two parameters were typically interchangeable. Because a few samples did contain elevated leachable sulphate, sulphide is a better indicator of acid potential than total sulphur for Schaft Creek rock. However, in many samples, most sulphide was copper-bound sulphide (chalcopyrite) which may have less capacity to generate acidity. Therefore, each sample has a maximum Sulphide-Based Acid Potential (SAP) and a minimum Pyrite-Calculated Acid Potential (PAP).

### 4.1.3 Neutralization Potentials

There are various types of neutralizing capacities in rock samples, all expressed in units of kg CaCO 3 equivalent/tonne ( $\mathrm{kg} / \mathrm{t}$ ). These include:
(1) Sobek "bulk neutralization potential" (NP) based on an hours-long acid bath to determine how much acid was neutralized in the short term (EPA 600 technique),
(2) carbonate-equivalent neutralization potential (CaNP) calculated from measured solid-phase levels of inorganic carbonate (Inorg CaNP) or total carbon (Total CaNP), and
(3) calculated CaNP assuming all calcium occurs as calcite (Ca CaNP) or all calcium + magnesium occurs as calcite and dolomite ( $\mathrm{Ca}+\mathrm{Mg} \mathrm{CaNP}$ ).

Each can reveal important aspects of a sample’s capacity to neutralize the acidity generated by sulphide oxidation. All values are compiled in Appendix B.

Short-term bulk Sobek NP ranged from 40 to $219 \mathrm{~kg} / \mathrm{t}$ in the 59 Schaft Creek samples, with a mean of 97 and a median of $92 \mathrm{~kg} / \mathrm{t}$ (Figure 4-7 and Appendix B). These are relatively high values. They explain why no acidic paste pH values were detected (Section 4.1.1), and suggest there could be a long lag time (years to decades) before these samples might become acidic. The two external duplicates and one internal duplicate showed good QA/QC for Sobek NP, with RPD values less than $10 \%$.


Figure 4-5. Calculated Pyrite-Bound Sulphide vs. Copper-Bound Sulphide as Chalcopyrite and $\mathrm{CuS}_{2}$ in the 59 Schaft Creek Rock Samples.


Figure 4-6. Pyrite-Calculated Acid Potential (PAP) vs. Sulphide-Based Acid Potential (SAP) in the 59 Schaft Creek Rock Samples.


Figure 4-7. Paste pH vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.


Figure 4-8. Inorganic-Carbon-Based Neutralization Potential vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

Some amount of measured NP is typically "unavailable" for neutralization, often between $5-15 \mathrm{~kg} / \mathrm{t}$ although smaller and larger values have been documented (Morin and Hutt, 1997 and 2001). This can sometimes be seen in scatterplots of NP with paste pH after sufficient time has passed for net acidity to develop. The trends then typically show paste pH generally, but not consistently, decreasing as NP decreases, until acidic pH values are detected.

However, the lack of any acidic paste pH in the 59 samples means that Unavailable NP cannot be estimated at this time. Thus, the common default value of $10 \mathrm{~kg} / \mathrm{t}$ will be used and will be subtracted from all measured values to obtain Available NP (Appendix B and Figure 4-7).

The comparison of total carbon with inorganic carbon showed that both were about the same in nearly all samples (Appendix B). Only four samples had noticeably higher total carbon, but inorganic carbon was still more than half of the total carbon in three of these four samples. In the remaining sample (14816, Appendix B), inorganic carbon was only around $17 \%$ of total carbon. This was probably an analytical error, with total carbon too high or inorganic carbon too low. As explained in the next paragraph, inorganic carbon was probably too low in this sample.

A scatterplot of Sobek NP with Inorganic Carbon, converted to the same units (Inorganic CaNP as kg/t), showed that Sobek NP was typically greater than Inorganic CaNP (Figure 4-8). NP was often greater by a factor of 1.5 or more, except above NP values above $100 \mathrm{~kg} / \mathrm{t}$ when the two values converged. Such exceedances of NP above Inorganic CaNP are not common. Nevertheless, this appears valid for Schaft Creek rock based on (a) the consistency of the Schaft Creek results (Figure 4-8) and (b) the mineralogy showing abundant non-carbonate, aluminosilicate minerals (Chapter 2) that can provide neutralization. Based on the trend in Figure 4-8, Inorganic CaNP in anomalous Sample 14816 is likely too low.

Because the type of carbonate (calcite, dolomite, siderite, etc.) was not determined in previous studies (Chapter 2), scatterplots with Inorganic CaNP can sometimes reveal the carbonate composition, if elements like calcium and magnesium mostly occur only with carbonate. For the comparison, calcium was converted to "Ca CaNP" with similar units as Inorganic CaNP. This showed that some samples contained excess carbonate, many contained excess calcium, and some contained both in calcite-equivalent amounts (Figure 4-9). The excess calcium was consistent with calcium-bearing aluminosilicate minerals in Schaft Creek rock (Chapter 2).

A comparison of "Ca+Mg CaNP" to Inorganic CaNP showed that nearly every sample contained more $\mathrm{Ca}+\mathrm{Mg}$ than carbonate (Figure 4-10). This meant that dolomite could not account for all the $\mathrm{Ca}+\mathrm{Mg}$, which was consistent with both calcium-bearing and magnesium-bearing aluminosilicate minerals in Schaft Creek rock (Chapter 2).

Sobek NP showed a better correlation with Ca CaNP (Figure 4-11) than with Inorganic CaNP (Figure 4-9), although the correlation was still poor for both. This suggests calcium-bearing minerals, both carbonate and aluminosilicate, can account for the Sobek NP in several samples, but not all samples. Ca +Mg CaNP displayed an even poorer correlation with Sobek NP (Figure 4-12). Thus, rapid assay-based analyses like calcium and magnesium cannot substitute for the more intensive Sobek NP in Schaft Creek rock.


Figure 4-9. Calcium-Based Neutralization Potential vs. Inorganic-CarbonBased Neutralization Potential in the 59 Schaft Creek Rock Samples.


Figure 4-10. Calcium-Magnesium-Based Neutralization Potential vs. Inorganic-Carbon-Based Neutralization Potential in the 59 Schaft Creek Rock Samples.


Figure 4-11. Calcium-Based Neutralization Potential vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.


Figure 4-12. Calcium-Magnesium-Based Neutralization Potential vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

In summary, Sobek (EPA 600) Neutralization Potential (NP) ranged from 40 to $219 \mathrm{~kg} / \mathrm{t}$ in the 59 Schaft Creek samples, with a mean of 97 and a median of $92 \mathrm{~kg} / \mathrm{t}$. These are relatively high values. They explain why no acidic paste pH values were detected, and suggest there could be a long lag time (years to decades) before these samples might become acidic. A certain amount of measured NP is typically "unavailable" for neutralization, and thus should be subtracted from measured values. The lack of acidic paste pH values precluded an initial estimate of Unavailable Neutralization Potential, so the common value of $10 \mathrm{~kg} / \mathrm{t}$ is used here. NP was typically greater than inorganic carbonate in many samples, meaning NP also reflected the presence of non-carbonate aluminosilicate minerals. These minerals have been documented in Schaft Creek rock. Also, NP did not correlate well with solid-phase calcium or magnesium levels, but some samples showed that calcium-bearing minerals could account for their NP levels.

### 4.1.4 Net Balances of Acid-Generating and Acid-Neutralizing Capacities

As explained in Section 4.1.2, the acid-generating capacities of the Schaft Creek samples of rock could be calculated from total sulphur to obtain Total-Sulphur-Based Acid Potentials (TAP), or sulphide plus \%S(del) to obtain Sulphide-Based Acid Potentials (SAP). Because total sulphur was mostly composed of sulphide, TAP and SAP were generally interchangeable. SAP is used here for net balances, because a few samples had significant amounts of leachable sulphate which was not acid generating. As explained in Section 4.1.2, SAP is considered the maximum "worst-case" acid potential for each sample, whereas the Pyrite-Calculated Acid Potential (PAP) is considered the "best-case" minimum.

Neutralization Potentials (NP) were discussed in Section 4.1.3. The current estimate of 10 $\mathrm{kg} / \mathrm{t}$ was considered unavailable and was subtracted from measured values.

Net balances of these two potentials were calculated to predict whether a sample would be net acid generating, perhaps after a long near-neutral "lag time", or net acid neutralizing indefinitely. Net balances can be calculated using division (Net Potential Ratio, NPR = NP / AP) or subtraction (Net Neutralization Potential, NNP = NP - AP).

Provincially, NPR is preferred and used here. "Adjusted" Sulphide-Based NPR values were obtained by first subtracting $10 \mathrm{~kg} / \mathrm{t}$ of unavailable NP from measured NP:

Adj SNPR $=[\mathrm{NP}-10] /[\%$ S(sulphide + positive delS values) * 31.25]
Similarly, Adjusted Pyrite-Calculated NPR values were calculated by:
Adj PNPR = [NP - 10] / [PAP]
Provincial non-site-specific ABA screening criteria are: NPR $<1$ is net acid generating, perhaps after some lag time; $1 \leq$ NPR $\leq 2$ is uncertain until further testing; and NPR $>2$ is net acid neutralizing. The implications of using the alternative criterion of 1.0 are discussed below and in Chapter 5.

It is important to note that all discussions of net balances in this report are "unweighted". This means that they were not adjusted to tonnages in the Schaft Creek Deposit. Three-dimensional
geostatistical modelling of geology and ML-ARD parameters should be conducted (Chapter 5; see also Section 4.1.5), to address issues such as (1) the total tonnages of net-acid-generating rock, (2) year-by-year production of net-acid-generating rock, and (3) portions of rock units that are net acid generating.

Worst-case Adjusted SNPR values ranged from 0.86 (net acid generating) to 114 (net neutralizing). Only one sample was less than 1.0 (tourmaline breccia, TOBR), and eight samples (several rock units) were between 1.0 and 2.0 (Figures 4-13 and 4-14, and Appendix B). Only samples with sulphide below $0.6 \%$ or Sobek NP above $125 \mathrm{~kg} / \mathrm{t}$ were consistently net neutralizing.

In contrast, best-case Adjusted PNPR values ranged from 1.03 (uncertain) to the default value of 200 which means that PAP was less than $0.01 \%$ S (Figures $4-15$ and $4-16$, and Appendix B). No values were less than 1.0, and only three samples from three rock units were less than 2.0. Many samples had the default value of 200. As with Adj SNPR, only samples with sulphide below $0.6 \%$ S or Sobek NP above $125 \mathrm{~kg} / \mathrm{t}$ were consistently net neutralizing.

Overall, only $0-2 \%$ of the 59 samples were net acid generating and $5-14 \%$ were uncertain (Table 4-1). Therefore, most samples were net neutralizing. Although the numbers of samples from most rock units were limited, the major rock units ( $>5 \%$ of 2005 footage, Table 3-1) with some uncertain samples were PPAU and PPFQ. The minor units with uncertain or net-acid-generating percentages were ANDS, TOBR, BRIV, and DIOR.

In summary, best-case and worst-case net balances of acid-generating and acid-neutralizing capacities were calculated for each of the 59 Schaft Creek samples. Overall, only $0-2 \%$ of the samples were net acid generating and $5-14 \%$ were uncertain based on generic criterion. Thus, most samples were net neutralizing. PPAU and PPFQ were the major rock units with uncertain samples, while net-acid-generating or uncertain samples were found in the minor rock units of ANDS, TOBR, BRIV, and DIOR.

### 4.1.5 Spatial Distribution of Net Balances

As explained in Section 4.1.4, net balances of acid-generating and acid-neutralizing capacities in the 59 samples of Schaft Creek core showed that most samples were net acid neutralizing. Only $0-2 \%$ of samples were net acid generating and $5-14 \%$ were uncertain.

An important aspect of these balances is whether there are any major spatial distributions through the Schaft Creek Deposit. For example, if all net-acid-generating and uncertain samples were located in one area, this area could be targetted for special mining and waste management.

Spatial distributions are best determined by geostatistical modelling combined with the Schaft Creek geologic model (Chapter 5). However, as a general indication here, one general eastwest and one general north-south vertical cross-section were plotted, with drillholes moved laterally onto the plane of the section.


Figure 4-13. Worst-Case Adjusted Sulphide-Based Net Potential Ratio vs. Sulphide in the 59 Schaft Creek Rock Samples.


Figure 4-14. Worst-Case Adjusted Sulphide-Based Net Potential Ratio vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.


Figure 4-15. Best-Case Adjusted Pyrite-Calculated Net Potential Ratio vs. Sulphide in the 59 Schaft Creek Rock Samples.


Figure 4-16. Best-Case Adjusted Pyrite-Calculated Net Potential Ratio vs. Sobek Neutralization Potential in the 59 Schaft Creek Rock Samples.

| Table 4-1. Summary of Net-Acid-Generating, Uncertain, and Net-Neutralizing Percentages of Samples from 2005 Drill Core |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Best-case and worst-case percentages ${ }^{2}$ of . . |  |  |
| Rock-Unit Code | ARD Samples ${ }^{1}$ | Net acid generating | Uncertain | Net neutralizing |
| PPAU | 16 | 0\% | 0-12.5\% | 87.5-100\% |
| ANPL (and ANLP) | 5 | 0\% | 0\% | 100\% |
| ANPF | 11 | 0\% | 0\% | 100\% |
| PPFQ | 5 | 0\% | 20-40\% | 60-80\% |
| ANDS | 4 | 0\% | 25-25\% | 75-75\% |
| BRVL | 2 | 0\% | 0\% | 100\% |
| TOBR | 4 | 0-25\% | 0-25\% | 75-75\% |
| FAUL and SHER | 3 | 0\% | 0\% | 100\% |
| PPPL | 2 | 0\% | 0\% | 100\% |
| ANTF | 2 | 0\% | 0\% | 100\% |
| BRIV | 1 | 0\% | 0-100\% | 0-100\% |
| D/BS | 1 | 0\% | 0\% | 100\% |
| DIOR | 2 | 0\% | 0-100\% | 0-100\% |
| BRXX | 0 |  |  |  |
| PNBX | 0 |  |  |  |
| VN | 0 |  |  |  |
| ANNX | 1 | 0\% | 0\% | 100\% |
|  | 59 | 0-1.7\% | 5.1-13.6\% | 84.7-94.9\% |
| ${ }^{1}$ Total includes two duplicates: 14578B from Hole 246 of PPAU, and 14685B from Hole 245 of DIOR. |  |  |  |  |
| ${ }^{2}$ Net-acid-generating samples had NPR values less than 1.0, uncertain samples had $1.0<$ NPR $<2.0$, and net-neutralizing samples > 2.0; best case is defined by the Adjusted PyriteCalculated Net Potential Ratio (Adj PNPR) and the worst case is defined by the Adjusted Sulphide-Based Net Potential Ratio (Adj SNPR). |  |  |  |  |

Based on the worst-case net balance (Adjusted SNPR, Section 4.1.4), the general east-west cross-section showed the center area was net-neutralizing (Figure 4-17), while net-acid-generating and uncertain samples were found on the periphery. The general north-south cross-section showed uncertain samples were found in three adjacent holes (Figure 4-18). Based on this limited information, the net-acid-generating and uncertain samples may be spatially restricted in the Schaft Creek Deposit, but additional samples and geostatistical modelling are needed to confirm this.

### 4.2 Total-Element Analyses

Total-element levels in the 59 Schaft Creek samples (Section 3.1) were measured by ICP-MS analysis after strong four-acid digestion and by x-ray-fluorescence whole-rock analysis (Section 3.2). The results are compiled in Appendix B. There was generally good agreement for elements detected by both methods (Appendix B), except chromium whose whole-rock levels were notably higher due to the higher detection limit.

Overall, the dominant elements in the Schaft Creek samples were silicon and aluminum (Appendix B), reflecting the dominance of aluminosilicate minerals (Chapter 2). Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were relatively abundant. LOI typically reflects the loss from the samples of some or all sulphur, carbon, and tightly bound or crystalline water.

To identify the metals and other elements that occurred at relatively high levels in the rock, each element was compared with average crustal abundances, as recommended in provincial MLARD documents (Price, 1998). Any level at least three times greater than the average maximum crustal abundance was highlighted with a box in Appendix B. This showed that the Schaft Creek samples were:

- frequently elevated in silver, bismuth, copper, molybdenum, and selenium; and, - occasionally elevated in sulphur, antimony, and tungsten.

Elevated solid-phase levels of elements do not necessarily mean they will leach into water at high concentrations. In fact, they may be elevated because they did not leach. Additional testwork is needed to evaluate metal leaching in detail (Chapter 5).

Solid-phase correlations of elements can sometimes reveal mineralogical associations. For example, elements correlating with sulphide presumably occur within the sulphide minerals, which at the Schaft Creek Project are typically pyrite and chalcopyrite (Chapter 2). Correlations with Sobek Neutralization Potential (NP, Section 4.1.3) indicate those elements may be concentrated in certain carbonate and aluminosilicate minerals, which can dissolve even in the absence of sulphide oxidation.

The only element that showed some correlation with sulphide was copper. This was discussed in Section 4.1.2. NP showed some correlation with calcium, as discussed in Section 4.1.3, and perhaps minor negative correlations with arsenic and lead. The few samples of tourmaline breccia (TOBR), and a few samples of other units, sometimes stood out as distinct groupings of generally higher or lower levels of elements like gallium, phosphorus, thallium, tungsten, and uranium.


Figure 4-17. General East-West Vertical Cross-Section through the Schaft Creek Deposit, Showing Worst-Case Adjusted Sulphide-Based Net Potential Ratio (0-1 = net acid generating; 1-2 = uncertain; >2 = net acid neutralizing).


Figure 4-18. General North-South Vertical Cross-Section through the Schaft Creek Deposit, Showing Worst-Case
Adjusted Sulphide-Based Net Potential Ratio (0-1 = net acid generating; 1-2 = uncertain; >2 = net acid neutralizing).

In summary, the 59 samples of Schaft Creek core were predominantly composed of silicon and aluminum, reflecting the abundant aluminosilicate minerals. Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were also relatively abundant. Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so additional testwork is needed on metal leaching. Only copper showed some correlation with sulphide, reflecting the copper-bound sulphide discussed under Acid-Base Accounting. For Sobek Neutralization Potential, calcium showed some correlation, which was also discussed under Acid-Base Accounting. Samples of some rock units, particularly tourmaline breccia (TOBR), stood out as a distinct group for some elements like gallium, phosphorus, thallium, tungsten, and uranium.

## 5. CONCLUSION AND RECOMMENDATIONS

This report contains the first phase of ML-ARD studies for the Schaft Creek Project. Previous relevant information was compiled. Also, 59 samples of core rejects, from 11 holes drilled in 2005, were collected from cold storage. This set included two duplicates for QA/QC checks. All 59 samples were analyzed for expanded Sobek (EPA 600) acid-base accounting, and for totalelement contents using ICP-MS after four-acid digestion and using x-ray fluorescence whole rock.

## Previous Information

The compilation of existing information relevant to ML-ARD led to the following important observations.

- The Schaft Creek copper-gold-molybdenum deposit is widely acknowledged as being a porphyry copper deposit. It contains three mineral zones: the Liard, West Breccia, and Paramount Zones.
- During an examination of existing core, "It has been noted that the core from previous drilling programs, which is stored on site, exhibits a remarkable degree of preservation with limited visible weathering." Thus, the oxidation rate of Schaft Creek rock may be relatively slow.
- Based on 16 acid-base accounts from a previous, metallurgical study, all 16 samples were net acid neutralizing, with sulphide between 0.1 and $0.9 \%$, and Neutralization Potentials from 53 to $114 \mathrm{~kg} / \mathrm{t}$. Flotation recovery of sulphide reduced the sulphide levels in the synthetic tailings.
- Detailed mineralogy was examined in 18 thin sections, representing feldspar quartz porphyry (rock code PPFQ), tourmaline breccia, pneumatolytic breccia, and volcanics. Even one rock unit (PPFQ) was not entirely intrusive. Some PPFQ samples were porphyritic volcanics of felsic and intermediate composition (dacitic - andesitic), and one sample was a fine grained, feldspathic intrusive rock classified as either syenite or anorthosite, depending on the composition of feldspar. Groundmass in these samples was generally around one-half of the total, with the groundmass consisting of more than $90 \%$ feldspar, and accessory amounts of quartz, chlorite, sericite, carbonate, opaques. Sulphide minerals were mostly disseminated and as veinlets and clusters, and mostly pyrite and chalcopyrite with less common molybdenite and bornite. Carbonate minerals, mostly reported as veins, patches, and groundmass, were not individually identified and were sometimes seen as feldspar replacement/alteration.


## Results of Acid-Base Accounting (ABA)

Paste pH in the 59 core samples for Schaft Creek ranged from 7.6 to 8.6. Thus, no samples were acidic at the time of analysis.

Total sulphur in the 59 Schaft Creek rock samples ranged from 0.02 to $1.91 \%$ S, with a mean of $0.45 \%$ S and a median of $0.26 \%$ S. In most samples, total sulphur and sulphide were similar, and thus the two parameters were typically interchangeable. Because a few samples did contain elevated leachable sulphate, sulphide is a better indicator of acid potential than total sulphur for Schaft Creek rock. However, in many samples, most sulphide was copper-bound sulphide (chalcopyrite) which may have less capacity to generate acidity. Therefore, each sample has a maximum "worst-case" Sulphide-Based Acid Potential (SAP) and a minimum "best-case" Pyrite-Calculated Acid Potential (PAP).

Sobek (EPA 600) Neutralization Potential (NP) ranged from 40 to $219 \mathrm{~kg} / \mathrm{t}$ in the 59 Schaft Creek samples, with a mean of 97 and a median of $92 \mathrm{~kg} / \mathrm{t}$. These relatively high values explain why no acidic paste pH values were detected, and suggest there could be a long lag time (years to decades) before these samples might become acidic. The lack of acidic paste pH values precluded an initial estimate of Unavailable Neutralization Potential, so the common value of $10 \mathrm{~kg} / \mathrm{t}$ is used here.

NP was typically greater than inorganic carbonate in many samples, meaning NP also reflected the presence of non-carbonate aluminosilicate minerals. These minerals have been documented in Schaft Creek rock. Also, NP did not correlate well with solid-phase calcium or magnesium levels, but some samples showed that calcium-bearing minerals could account for their NP levels.

Best-case and worst-case net balances of acid-generating and acid-neutralizing capacities were calculated for each of the 59 Schaft Creek samples. Overall, only $0-2 \%$ of the samples were net acid generating and $5-14 \%$ were "uncertain" based on generic criterion. Thus, most samples were net neutralizing. PPAU and PPFQ were the major rock units with uncertain samples, while net-acid-generating or uncertain samples were found in the minor rock units of ANDS, TOBR, BRIV, and DIOR.

To generally assess the spatial distribution of net balances, a general east-west cross-section showed the center area was net-neutralizing, while net-acid-generating and uncertain samples were found on the periphery. The general north-south cross-section showed uncertain samples were found in three adjacent holes. Based on this limited information, the net-acid-generating and uncertain samples may be spatially restricted in the Schaft Creek Deposit, but additional samples and geostatistical modelling are needed to confirm this.

## Results of Total-Element Analyses

The 59 samples of Schaft Creek core were predominantly composed of silicon and aluminum, reflecting the abundant aluminosilicate minerals. Calcium, iron, potassium, magnesium, sodium, and Loss on Ignition (LOI) were also relatively abundant.

Compared to general crustal abundances, the 59 samples were frequently elevated in silver, bismuth, copper, molybdenum, and selenium, and occasionally elevated in sulphur, antimony, and tungsten. However, solid-phase levels do not typically reflect leaching rates into water, so
additional testwork is needed on metal leaching.
Only copper showed some correlation with sulphide, reflecting the copper-bound sulphide discussed under Acid-Base Accounting. For Sobek Neutralization Potential, calcium showed some correlation. Samples of some rock units, particularly tourmaline breccia (TOBR), stood out as a distinct group for some elements like gallium, phosphorus, thallium, tungsten, and uranium.

## Recommendations for Future ML-ARD Work

A phased approach, with each focussing on resolving uncertainties raised in previous ones, is recommended in the provincial ML-ARD Prediction Manual. Thus, based on the preceding information, we offer the following recommendations for the next phase of ML-ARD studies at the Schaft Creek Project.

- Overburden should be analyzed for ML-ARD potential. Up to several tens of meters of overburden have been reported in drillholes. This overburden in the pit area would be disturbed and oxidized during mining, and might be used for construction or reclamation during and after operation.
- Unavailable Neutralization Potential (UNP) could not be reliably estimated from available data (Section 4.1.3), but affects net balances. Therefore, UNP should be determined better for Schaft Creek. This would likely require humidity cells (see below).
- Most samples with NPR < 2 were between 1.0 and 2.0, meaning their ARD potential is "uncertain" at this time (Section 4.1.5). This uncertain range should be resolved for proper planning of waste management and water management. Humidity cells would help with this (see next recommendation).
- Six laboratory-based kinetic tests, known as humidity cells, should be conducted for at least 40 weeks on $1-\mathrm{kg}$ samples of Schaft Creek rock. These would provide bulk rates of acid generation, neutralization, and metal leaching, and would help in resolving UNP and "uncertain" samples (see above). Previous information on weathered core suggested reaction rates in Schaft Creek rock were low.
- Four on-site leach tests, each containing up to approximately one tonne of disturbed rock or broken core, should be set up at Schaft Creek and periodically sampled as part of routine on-site water-quality monitoring. These would provide on-site drainage-chemistry data and are important for upscaling the smaller-scale humidity cells.
- At this time, the net-acid-generating and "uncertain" samples may be clustered in portions of the deposit, which would focus waste management and any special handling onto specific zones. To examine this clustering further, additional core samples, including 2006 holes, should be collected from across the deposit and submitted for expanded acid-base accounting and totalelement contents. The results would be used in geostatistical modelling (see next recommendation).
- Three-dimensional geostatistical modelling should be carried out to calculate total tonnages and year-by-year tonnages of net-acid-generating, currently "uncertain", and net-neutralizing rock. This is important for identifying the most cost-effective options for waste management and water management.


## 6. REFERENCES

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APPENDIX A. Notes on the Collection of Phase 1 ML/ARD Samples by MDAG, February 2007

# Schaft Creek Project Trip Report for Static-Test Sampling 

K. Morin, February 9, 2007

On February 3 (Saturday), staff at Bandstra Transportation Systems opened Copper Fox’ unheated storage locker. They sorted up to 20 skids to find the 63 buckets containing the initial list of samples for static testing (acid-base accounting and total-element analyses). This saved several hours of Rescan/MDAG time. The selected buckets were consolidated onto two skids, and brought inside to warm up so that saturated samples could be sampled. Six of the 63 sample buckets could not be found and were thus deleted from the sampling list. This left 57 samples to be collected.

On February 7, Kevin Morin flew to Smithers on the early morning flight. At Bandstra, he collected the 57 samples, plus two additional backup samples (Table 1). This involved prying open each bucket, noting the general colour and the dryness of the rejects (gravel, sand, and silt), then removing a few hundred grams from the top of the rejects. To minimize cross-contamination of metals, each sample was removed with a fibreglass hand shovel, after cleaning with disposable soapy wipes and clean paper towels. The two backup samples were collected from the bottom, rather than the top, of the rejects, to check for any significant geochemical variability within each reject bucket.

The 59 samples were shipped in the late afternoon of February 7, by Greyhound Courier, to ALS Chemex Labs in North Vancouver.

Project: Schaft Creek Projec
Client: Copper Fox Metals Inc
Data: Sample Information
Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7 ' 07 by Kevin Morin, MDAG.

| Sample No. | Hole Id | Lithology From (m) | To (m) | Rock Code | Mineralization Style | $\begin{gathered} \text { Ch } \\ \text { Chlorite } \end{gathered}$ | $\begin{gathered} \text { Ep } \\ \text { Epidote } \end{gathered}$ | $\begin{gathered} \mathrm{Bt} \\ \text { Biotite } \end{gathered}$ | Alterati Se Sericite |  | Si Silicic | Hm Hematite | Cb | Tm Tourmaline |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14545 | 05CF246 | 12.1 | 15.2 | ANPF | Py, Cp dis | W-M |  |  |  |  |  | W |  |  |  |
| 14565 | 05CF246 | 63.6 | 66.7 | ANPF | Cp cb-qtz-ch stkwk | w |  |  |  | W |  | W |  |  |  |
| 14571 | 05CF246 | 81.8 | 84.8 | PPPL | Py, Cp dis, Mb cb-qtz-ch vn | W |  |  |  | W |  | X |  |  |  |
| 14578 | 05CF246 | 103.0 | 106.1 | PPAU | Py dis, Cp ch stckwk | W-M |  |  |  | W-M |  | X |  |  |  |
| 14578B | 05CF246 | 103.0 | 106.1 | PPAU |  |  |  |  |  |  |  |  |  |  |  |
| 14598 | 05CF246 | 154.5 | 157.6 | PPAU | Cp,Py dis | M |  |  |  |  |  |  |  |  | 5 |
| 14689 | 05CF244 | 9.1 | 12.1 | PPFQ | Py, Cp, dis, cb-qtz vn, frct | W |  |  | w | S |  | X |  |  |  |
| 14695 | 05CF244 | 27.3 | 30.3 | PPAU | Py, Cp, dis | M-S |  |  |  | W |  | W |  |  | T |
| 14742 | 05CF244 | 160.6 | 163.6 | ANLP | Cp dis, Cp,Bn qtz-cb vn, Mb frct | W |  |  |  | W |  |  | W |  | 1 |
| 14998 | 05CF248 | 36.4 | 39.4 | ANPF | STKWK | W |  |  |  |  |  |  |  |  |  |
| 15862 | 05CF248 | 78.8 | 81.8 | ANPF | STKWK, MB-Frct | W | W |  |  | W |  |  |  |  |  |
| 15870 | 05CF248 | 103.0 | 106.1 | ANLP | STKWK | W |  |  |  | M |  | w |  |  |  |
| 15879 | 05CF248 | 130.3 | 133.3 | BRVL | STKWK | W | W |  |  | W |  | W |  |  |  |
| 15887 | 05CF248 | 145.5 | 148.5 | ANTF | STKWK, Dis | w | W |  |  |  | w |  | w |  |  |
| 15891 | 05CF248 | 157.6 | 160.6 | ANPF | STKWK | W |  |  |  | W |  | W |  |  |  |
| 15908 | 05CF248 | 209.1 | 212.1 | PPFQ | STKWK, MB-Frct, Dis, Flt | W |  |  |  |  |  |  |  |  |  |
| 15911 | 05CF248 | 218.2 | 221.2 | ANDS | STKWK, Dis | W |  |  |  | W |  |  |  |  |  |
| 14130 | 05CF236 | 18.2 | 21.2 | ANPF | Cu diss \& qtz veins |  |  |  |  | S | w |  |  |  |  |
| 14144 | 05CF236 | 60.6 | 63.6 | ANPF | Cu diss \& veins | M |  |  |  | M-S | W | M |  |  |  |
| 14148 | 05CF236 | 72.7 | 75.8 | FAUL | Cudiss | S |  |  |  | S |  | W |  |  |  |
| 14156 | 05CF236 | 87.9 | 90.9 | FAUL | Mb fracture |  |  |  |  | W |  |  |  |  |  |
| 14162 | 05CF236 | 106.1 | 109.1 | D/BS |  |  |  |  |  |  |  |  |  |  | W |
| 14169 | 05CF236 | 127.3 | 130.3 | PPFQ | $\mathrm{Cu}, \mathrm{Mb}$ qtz veins \& diss |  |  |  |  | M-S |  |  |  |  |  |
| 14018 | 05CF234 | 18.2 | 21.2 | PPFQ | Disseminated + Vein | W | w |  | W | W |  |  |  |  |  |
| 14021 | 05CF234 | 27.3 | 30.3 | TOBR | Hydro Bx Matrix (vein) + diss | M | W |  | M | M | M |  |  | X |  |
| 14036 | 05CF234 | 63.6 | 66.7 | TOBR | Stockwork + disseminated | M |  |  | S | M | M |  |  | X |  |
| 14043 | 05CF234 | 84.8 | 87.9 | TOBR | Stockwork + disseminated | W | W |  | M | M | W |  |  | X |  |
| 14060 | 05CF234 | 136.4 | 139.4 | BRIV | Disseminated in matrix | M | M |  | M | M? |  | M? |  |  |  |
| 14067 | 05CF234 | 157.6 | 160.6 | ANPF | Disseminated, vein | S | W |  | S | W | w |  |  |  |  |
| 14076 | 05CF235 | 18.2 | 21.2 | ANDS | STKWK, Dis | W |  |  |  |  |  |  |  |  |  |
| 14083 | 05CF235 | 39.4 | 42.4 | ANDS | STKWK | W | w |  |  |  |  |  |  |  |  |
| 14099 | 05CF235 | 87.9 | 90.9 | PPFQ | Dis | W |  |  |  |  |  |  |  |  |  |
| 14103 | 05CF235 | 100.0 | 103.0 | TOBR | Dis | w | w |  |  | w |  |  |  | M |  |
| 14232 | 05CF239 | 27.3 | 30.3 | PPAU | dis, stkwk, bx vns, Mb frct |  |  |  |  | W |  |  |  |  |  |
| 14250 | 05CF239 | 72.7 | 75.8 | PPAU | stkwk | W |  |  |  | W |  | w |  |  |  |
| 14260 | 05CF239 | 103.0 | 106.1 | PPAU | stkwk, $\mathrm{Cp}, \mathrm{Bn}$ in vns | W |  |  |  | W |  | W |  |  |  |
| 14276 | 05CF239 | 142.4 | 145.5 | ANPF | stkwk, dis, Cp,Mb vns, Mb frct | W | W |  |  |  |  |  |  |  |  |
| 14295 | 05CF239 | 200.0 | 203.0 | ANPF | stkwk, Py vns | W | W |  |  | W |  | w |  |  |  |
| 14301 | 05CF240 | 9.1 | 12.1 | ANNX | STKWK, Mb Frct |  |  |  |  | S |  |  |  |  |  |
| 14323 | 05CF240 | 66.7 | 69.7 | PPAU | STKWK, Cp-V | w |  |  |  | W |  |  |  |  |  |
| 14332 | 05CF240 | 93.9 | 97.0 | PPAU | STKWK, Mb-Frct | W |  |  |  | W |  | w |  |  |  |
| 14345 | 05CF240 | 133.3 | 136.4 | ANPF | STKWK, Dis | W |  |  |  | W |  |  |  |  |  |
| 14348 | 05CF240 | 142.4 | 145.5 | PPAU | STKWK, Dis, Mb-Frct | W |  |  |  | W |  |  |  | W |  |
| 14666 | 05CF245 | 51.5 | 54.5 | BRVL | STKWK, Dis, MB-Frct | w | W |  |  | W |  |  |  |  |  |
| 14685 | 05CF245 | 100.0 | 103.0 | DIOR | STKWK, Dis, MB-Frct | W |  |  |  | M |  |  |  |  |  |
| 14685B | 05CF245 | 100.0 | 103.0 | DIOR |  |  |  |  |  |  |  |  |  |  |  |
| 14797 | 05CF243 | 9.1 | 12.1 | PPAU | STKWK, Dis, MB-Frct | w |  |  |  | W |  |  |  |  |  |
| 14808 | 05CF243 | 42.4 | 45.5 | FAUL | STKWK, MB-Frct, SHEAR | w |  |  |  | S |  |  |  |  |  |
| 14816 | 05CF243 | 66.7 | 69.7 | PPAU | STKWK, PY-Vns | W |  |  |  | M |  | W |  |  |  |
| 14828 | 05CF243 | 103.0 | 106.1 | PPAU | STKWK, Dis, MB-Frct | w |  |  |  | W |  |  |  |  |  |
| 14844 | 05CF243 | 142.4 | 145.5 | ANDS | STKWK, CP-Vn, Dis | W |  |  |  |  |  |  |  |  |  |
| 14860 | 05CF243 | 190.9 | 193.9 | PPAU | STKWK, MB-Frct, CP-Frct | w |  |  |  | w |  |  |  |  | W |
| 14871 | 05CF243 | 224.2 | 227.3 | ANLP | STKWK, CP-Vn,Frct, Dis, SHR, | w | w |  |  | W |  | w |  |  |  |

Project: Schaft Creek Project
Client: Copper Fox Metals Inc
Data: Sample Information
Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7 ' 07 by Kevin Morin, MDAG.

| Sample No. | Hole Id | Lithology From (m) | To (m) | Rock Code | Mineralization Style | Ch Chlorite | $\begin{gathered} \text { Ep } \\ \text { Epidote } \end{gathered}$ | $\begin{gathered} \mathrm{Bt} \\ \text { Biotite } \end{gathered}$ | Alterati Se Sericite | Minerals K K-spar | $\underset{\text { Silicic }}{\mathrm{Si}}$ | Hm <br> Hematite | Cb | Tm Tourmaline |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14887 | 05CF243 | 263.6 | 266.7 | ANTF | STKWK, CP-Vn, Dis | W | W |  |  |  |  | W |  |  |  |
| 14893 | 05CF247 | 12.1 | 15.2 | PPAU | Mal frct-1\%, Cp dis | w |  |  |  |  |  |  |  |  | 5 |
| 14899 | 05CF247 | 30.3 | 33.3 | PPAU |  | X |  |  |  |  |  | X |  |  |  |
| 14908 | 05CF247 | 57.6 | 60.6 | ANLP | Cp,Bn qtz-cb stkwk, Cp dis | W |  |  |  | W |  |  |  |  |  |
| 14917 | 05CF247 | 75.8 | 78.8 | PPPL | Bn dis, qtz-cb vn | X |  | x |  | W-M |  |  |  |  |  |
| 14925 | 05CF247 | 100.0 | 103.0 | ANLP | Cp qtz-cb vn, dis | W | x |  |  | X |  | w |  |  | 3 |


| Rock Code Legend: |  | Mineral Legend: |  | Legend: |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ANDS | Andesite | Ch | Chlorite | T | Trace |
| ANNX | Altered Andesite | Ep | Epidote | W | weak |
| ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | Bt | Biotite | M | moderate |
| ANPL/ANLP | Andesitic Lapilli Tuff | Se | Sericite | S | strong |
| ANTF | Andesitic Tuff | K | K-spar |  |  |
| BRIV | Intrusive Breccia or Felsic Igneous Breccia | Si | Silicic |  |  |
| BRVL | Volcanic Breccia | Hm | Hematite |  |  |
| BRXX | Diorite Breccia | Mt | Magnetite |  |  |
| D/BS | Diabase/Basic dyke | Tm | Tourmaline |  |  |
| DIOR | Diorite | Cp | Chalcopyrite |  |  |
| FAUL | Faults | Bn | Bornite |  |  |
| PNBX | Pneumatolytic Breccia | Py | Pyrite |  |  |
| PPAU | Plagioclase-Augite-phyric Andesite | Mb | Molybdenite |  |  |
| PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | Oth | See description |  |  |
| PPPPL | Plagioclase or Feldspar Porphyry | X | mineral present |  |  |

## Data: Sample Information

Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7'07 by Kevin Morin, MDAG.

| Sample No. | Sulphides \% |  |  |  |  |  | Sampling Notes | Assay Data |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cp Chalcopyrite | Bn <br> Bornite |  | Mb <br> Molybdenite | Other | Total |  | Cu <br> (\%) | Mo (\%) | Au <br> (g/t) | $\begin{gathered} \mathrm{Ag} \\ (\mathrm{~g} / \mathrm{t}) \end{gathered}$ |
| 14545 | T |  | T |  |  | T | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.113 | 0.001 | 0.02 | 0.4 |
| 14565 | T |  |  |  |  | T | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.289 | 0.002 | 0.14 | 0.6 |
| 14571 | 2.0 |  | 1.0 | 0.5 |  | 3.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.593 | 0.011 | 0.13 | 1.8 |
| 14578 | T |  | 1.0 |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines (see 14578B) | 0.293 | 0.002 | 0.04 | 0.7 |
| 14578B |  |  |  |  |  |  | Subsample collected from bottom of rejects stored in white plastic bucket; dry, light grey gravel and fines (see 14578) |  |  |  |  |
| 14598 | T |  | T |  |  | T | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.075 | 0.005 | 0.02 | 0.3 |
| 14689 | 0.5 |  | 1.0 | 0.5 |  | 2.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.213 | 0.008 | 0.07 | 0.4 |
| 14695 | T |  | 0.5 |  |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.182 | 0.059 | 0.13 | 0.7 |
| 14742 | T |  |  | 0.5 |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.223 | 0.071 | 0.17 | 1.0 |
| 14998 | T | T | 0.5 | T |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.169 | 0.007 | 0.14 | 0.5 |
| 15862 | T | T |  | 0.5 |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; moist, dark grey gravel and fines | 0.116 | 0.008 | 0.14 | 0.6 |
| 15870 | 0.5 | T | T | 0.5 |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; saturated, medium grey gravel and fines | 0.157 | 0.002 | 0.09 | 0.8 |
| 15879 | 0.5 | T |  | T |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.224 | 0.003 | 0.15 | 1.5 |
| 15887 | 1.0 | T |  | 0.5 |  | 1.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.285 | 0.008 | 0.28 | 1.8 |
| 15891 | T | 0.5 |  | 0.5 |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.234 | 0.011 | 0.21 | 1.5 |
| 15908 | 0.5 | 0.5 |  | 0.5 |  | 1.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.421 | 0.032 | 0.38 | 2.4 |
| 15911 | 0.5 | 0.5 |  | 0.5 |  | 1.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.179 | 0.017 | 0.15 | 1.0 |
| 14130 | T | -1 |  |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines | 0.555 | 0.008 | 0.39 | 3.3 |
| 14144 | T | $\sim 1$ |  |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines | 0.290 | 0.008 | 0.20 | 2.2 |
| 14148 |  | T |  |  |  | T | Subsample collected from top of rejects stored in white plastic bucket; saturated, medium grey gravel and fines | 0.275 | 0.020 | 0.17 | 1.2 |
| 14156 |  | T |  | 1.0 |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines | 0.204 | 0.005 | 0.07 | 1.0 |
| 14162 |  |  |  |  |  |  | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.115 | 0.051 | 0.09 | <0.5 |
| 14169 | 1.0 | 1.0 |  | <1 |  | <2 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.386 | 0.016 | 0.18 | 3.0 |
| 14018 |  |  | 1.0 |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines | 0.147 | 0.007 | 0.06 | <0.5 |
| 14021 | 2.0 |  | T |  |  | 2.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.173 | 0.036 | 0.03 | <0.5 |
| 14036 | 4.0 |  |  |  |  | 4.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines | 0.189 | 0.061 | 0.04 | 5.8 |
| 14043 | 0.0 |  |  |  |  | 2.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines | 0.153 | 0.034 | 0.15 | 2.0 |
| 14060 | T-1 |  |  |  |  | T-1 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.280 | 0.032 | 0.04 | <0.5 |
| 14067 | 1.0 |  |  |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; saturated, dark grey gravel and fines | 0.247 | 0.014 | 0.03 | <0.5 |
| 14076 | T |  | T |  |  | T | Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey-green gravel and fines | 0.173 | 0.005 | 0.16 | <0.5 |
| 14083 | T |  | 1.0 |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines | 0.130 | 0.001 | 0.01 | <0.5 |
| 14099 | 0.5 |  | 1.0 |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines | 0.157 | 0.002 | 0.02 | 1.1 |
| 14103 | 1.0 |  | T |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines | 0.266 | 0.022 | 0.02 | 1.0 |
| 14232 | 0.5 | 1.0 | 0.5 | 0.5 |  | 2.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines; low weight remaining | 0.325 | 0.011 | 0.21 | 1.8 |
| 14250 | 0.5 | 1.0 | 0.5 | 0.5 |  | 2.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.300 | 0.038 | 0.33 | 2.0 |
| 14260 | 1.0 | 0.5 | 0.5 | T |  | 2.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, dark grey gravel and fines | 0.505 | 0.016 | 0.9 | 3.1 |
| 14276 | 2.0 | T | 0.5 | 1.0 |  | 3.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines; low weight remaining | 0.136 | 0.003 | <0.01 | 1.0 |
| 14295 | 0.5 | T | 0.5 | T |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.250 | 0.001 | 0.07 | 0.5 |
| 14301 | T |  | T | 0.5 |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, grey and pink (granite?) gravel and fines | 0.241 | 0.023 | 0.09 | 0.6 |
| 14323 | 0.5 | 0.5 | T | T |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.200 | 0.005 | 0.18 | 1.6 |
| 14332 | 0.5 | 0.5 | T | 1.0 |  | 2.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.336 | 0.010 | 0.16 | 1.5 |
| 14345 | 2.0 | 0.5 | 0.5 | 0.5 |  | 3.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.559 | 0.020 | 0.19 | 2.4 |
| 14348 | 1.0 | 0.5 | 0.5 | 0.5 |  | 2.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.461 | 0.013 | 0.13 | 1.4 |
| 14666 | 0.5 |  | 1.0 | T |  | 1.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.163 | 0.002 | 0.07 | 0.3 |
| 14685 | 0.5 |  | 2.0 | T |  | 2.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines (see 14685B) | 0.455 | 0.013 | 0.18 | 0.6 |
| 14685B |  |  |  |  |  |  | Subsample collected from bottom of rejects stored in white plastic bucket; dry, medium grey gravel and fines (see 14685) |  |  |  |  |
| 14797 | 0.5 | 0.5 |  | 0.5 |  | 1.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.184 | 0.034 | 0.10 | 1.0 |
| 14808 | 0.5 | 0.5 |  | 2.0 |  | 3.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.257 | 0.040 | 0.28 | 1.7 |
| 14816 | T | 0.5 | 1.0 | T |  | 1.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, light grey gravel and fines | 0.387 | 0.008 | 0.57 | 2.3 |
| 14828 | 0.5 | 2.0 |  | 0.5 |  | 3.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.317 | 0.019 | 0.74 | 2.3 |
| 14844 | 1.0 | 0.5 | 0.5 | T |  | 2.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.249 | 0.010 | 0.16 | 1.0 |
| 14860 | 1.0 | 0.5 |  | 0.5 |  | 2.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.373 | 0.035 | 0.25 | 2.5 |
| 14871 | 2.0 | 0.5 |  | T |  | 2.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.365 | 0.034 | 0.10 | 0.7 |

Project:
Client:
Data:
Samper Fox Metals Inc
Comments: Samples collected for ABA, trace metal, and whole rock analysis On Feb 7'07 by Kevin Morin, MDAG

| Sample No. | Sulphides \% |  |  |  |  |  | Sampling Notes | Assay Data |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cp Chalcopyrite | Bn Bornite | Py Pyrite | Mb <br> Molybdenite | Other | Total |  | Cu <br> (\%) | Mo <br> (\%) | $\begin{gathered} \mathrm{Au} \\ (\mathrm{~g} / \mathrm{t}) \end{gathered}$ | $\begin{gathered} \mathrm{Ag} \\ (\mathrm{~g} / \mathrm{t}) \end{gathered}$ |
| 14887 | 0.5 |  | 0.5 |  |  | 1.0 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.196 | 0.00 | 0.07 | 0.7 |
| 14893 |  |  |  |  |  |  | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.164 | 0.008 | 0.12 | 0.9 |
| 14899 |  |  |  |  |  |  | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.032 | 0.002 | 0.03 | 0.7 |
| 14908 | 1.5 | T |  |  |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.113 | 0.005 | 0.08 | 0.7 |
| 14917 |  | 0.5 |  |  |  | 0.5 | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.361 | 0.001 | 0.31 | 2.5 |
| 14925 | T |  |  |  |  | T | Subsample collected from top of rejects stored in white plastic bucket; dry, medium grey gravel and fines | 0.182 | 0.001 | 0.11 | 1.0 |


| Mineral | Legend: | Legend: |  |
| :--- | :--- | :--- | :--- |
| Ch | Chlorite | T | Trace |
| Ep | Epidote | W | weak |
| Bt | Biotite | M | moderate |
| Se | Sericite | S | strong |
| K | K-spar |  |  |
| Si | Silicic |  |  |
| Hm | Hematite |  |  |
| Mt | Magnetite |  |  |
| Tm | Tourmaline |  |  |
| Cp | Chalcopyrite |  |  |
| Bn | Bornite |  |  |
| Py | Pyrite |  |  |
| Mb | Molybdenite |  |  |
| Oth | See description |  |  |
| X | mineral present |  |  |

# APPENDIX B. Compiled Acid-Base Accounting and Total-Element Analyses for Rock at the Schaft Creek Project 

Project:
Data:
Comments:

Schaft Creek
Copper Fox Metals Inc.
Sample Information
Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Sample |  | Lithology |  |  | Centre of |  | Rock | Rock Code |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Id. | Hole Id | From <br> (m) | $\begin{aligned} & \text { To } \\ & \text { (m) } \end{aligned}$ | Interval <br> (m) | Interval <br> (m) | Zone | Code | Description | Mineralization Style |
| 14018 | 05CF234 | 18.2 | 21.2 | 3.03 | 19.70 | West Breccia | PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | Disseminated + Vein |
| 14021 | 05CF234 | 27.3 | 30.3 | 3.03 | 28.79 | West Breccia | TOBR | Tourmaline Breccia | Hydro Bx Matrix (vein) + diss |
| 14036 | 05CF234 | 63.6 | 66.7 | 3.03 | 65.15 | West Breccia | TOBR | Tourmaline Breccia | Stockwork + disseminated |
| 14043 | 05CF234 | 84.8 | 87.9 | 3.03 | 86.36 | West Breccia | TOBR | Tourmaline Breccia | Stockwork + disseminated |
| 14060 | 05CF234 | 136.4 | 139.4 | 3.03 | 137.88 | West Breccia | BRIV | Intrusive Breccia or Felsic Igneous Breccia | Disseminated in matrix |
| 14067 | 05CF234 | 157.6 | 160.6 | 3.03 | 159.09 | West Breccia | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | Disseminated, vein |
| 14076 | 05CF235 | 18.2 | 21.2 | 3.03 | 19.70 | West Breccia | ANDS | Andesite | STKWK, Dis |
| 14083 | 05CF235 | 39.4 | 42.4 | 3.03 | 40.91 | West Breccia | ANDS | Andesite | STKWK |
| 14099 | 05CF235 | 87.9 | 90.9 | 3.03 | 89.39 | West Breccia | PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | Dis |
| 14103 | 05CF235 | 100.0 | 103.0 | 3.03 | 101.52 | West Breccia | TOBR | Tourmaline Breccia | Dis |
| 14130 | 05CF236 | 18.2 | 21.2 | 3.03 | 19.70 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | Cu diss \& qtz veins |
| 14144 | 05CF236 | 60.6 | 63.6 | 3.03 | 62.12 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | Cu diss \& veins |
| 14148 | 05CF236 | 72.7 | 75.8 | 3.03 | 74.24 | Liard Main | FAUL | Faults | Cudiss |
| 14156 | 05CF236 | 87.9 | 90.9 | 3.03 | 89.39 | Liard Main | FAUL | Faults | Mb fracture |
| 14162 | 05CF236 | 106.1 | 109.1 | 3.03 | 107.58 | Liard Main | D/BS | Diabase/Basic dyke |  |
| 14169 | 05CF236 | 127.3 | 130.3 | 3.03 | 128.79 | Liard Main | PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | $\mathrm{Cu}, \mathrm{Mb}$ qtz veins \& diss |
| 14232 | 05CF239 | 27.3 | 30.3 | 3.03 | 28.79 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | dis, stkwk, bx vns, Mb frct |
| 14250 | 05CF239 | 72.7 | 75.8 | 3.03 | 74.24 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | stkwk |
| 14260 | 05CF239 | 103.0 | 106.1 | 3.03 | 104.55 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | stkwk, $\mathrm{Cp}, \mathrm{Bn}$ in vns |
| 14276 | 05CF239 | 142.4 | 145.5 | 3.03 | 143.94 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | stkwk, dis, Cp,Mb vns, Mb frct |
| 14295 | 05CF239 | 200.0 | 203.0 | 3.03 | 201.52 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | stkwk, Py vns |
| 14301 | 05CF240 | 9.1 | 12.1 | 3.03 | 10.61 | Liard Main | ANNX | Altered Andesite | STKWK, Mb Frct |
| 14323 | 05CF240 | 66.7 | 69.7 | 3.03 | 68.18 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | STKWK, Cp-V |
| 14332 | 05CF240 | 93.9 | 97.0 | 3.03 | 95.45 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | STKWK, Mb-Frct |
| 14345 | 05CF240 | 133.3 | 136.4 | 3.03 | 134.85 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | STKWK, Dis |
| 14348 | 05CF240 | 142.4 | 145.5 | 3.03 | 143.94 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | STKWK, Dis, Mb-Frct |
| 14797 | 05CF243 | 9.1 | 12.1 | 3.03 | 10.61 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | STKWK, Dis, MB-Frct |
| 14808 | 05CF243 | 42.4 | 45.5 | 3.03 | 43.94 | Liard Main | FAUL | Faults | STKWK, MB-Frct, SHEAR |
| 14816 | 05CF243 | 66.7 | 69.7 | 3.03 | 68.18 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | STKWK, PY-Vns |
| 14828 | 05CF243 | 103.0 | 106.1 | 3.03 | 104.55 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | STKWK, Dis, MB-Frct |
| 14844 | 05CF243 | 142.4 | 145.5 | 3.03 | 143.94 | Liard Main | ANDS | Andesite | STKWK, CP-Vn, Dis |
| 14680 | 05CF243 | 190.9 | 193.9 | 3.03 | 192.42 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | STKWK, MB-Frct, CP-Frct |
| 14871 | 05CF243 | 224.2 | 227.3 | 3.03 | 225.76 | Liard Main | ANLP | Andesitic LapilliTuff | STKWK, CP-Vn,Frct, Dis, SHR, |
| 14887 | 05CF243 | 263.6 | 266.7 | 3.03 | 265.15 | Liard Main | ANTF | Andesitic Tuff | STKWK, CP-Vn, Dis |
| 14689 | 05CF244 | 9.1 | 12.1 | 3.03 | 10.61 | Liard Main | PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | Py, Cp, dis, cb-qtz vn, frct |
| 14695 | 05CF244 | 27.3 | 30.3 | 3.03 | 28.79 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | Py, Cp, dis |
| 14742 | 05CF244 | 160.6 | 163.6 | 3.03 | 162.12 | Liard Main | ANLP | Andesitic LapilliTuff | Cp dis, $\mathrm{Cp}, \mathrm{Bn}$ qtz-cb vn, Mb frct |
| 14666 | 05CF245 | 51.5 | 54.5 | 3.03 | 53.03 | Liard Main | BRVL | Volcanic Breccia | STKWK, Dis, MB-Frct |
| 14685 | 05CF245 | 100.0 | 103.0 | 3.03 | 101.52 | Liard Main | DIOR | Diorite | STKWK, Dis, MB-Frct |
| 14685B | 05CF245 | 100.0 | 103.0 | 3.03 | 101.52 | Liard Main | DIOR | Diorite |  |
| 14545 | 05CF246 | 12.1 | 15.2 | 3.03 | 13.64 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | Py, Cp dis |
| 14565 | 05CF246 | 63.6 | 66.7 | 3.03 | 65.15 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | Cp cb-qtz-ch stkwk |
| 14571 | 05CF246 | 81.8 | 84.8 | 3.03 | 83.33 | Liard Main | PPPL | Plagioclase or Feldspar Porphyry | Py, Cp dis, Mb cb-qtz-ch vn |
| 14578 | 05CF246 | 103.0 | 106.1 | 3.03 | 104.55 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | Py dis, Cp ch stckwk |
| 14578B | 05CF246 | 103.0 | 106.1 | 3.03 | 104.55 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite |  |
| 14598 | 05CF246 | 154.5 | 157.6 | 3.03 | 156.06 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | Cp,Py dis |
| 14893 | 05CF247 | 12.1 | 15.2 | 3.03 | 13.64 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite | Mal frct-1\%, Cp dis |
| 14899 | 05CF247 | 30.3 | 33.3 | 3.03 | 31.82 | Liard Main | PPAU | Plagioclase-Augite-phyric Andesite |  |
| 14908 | 05CF247 | 57.6 | 60.6 | 3.03 | 59.09 | Liard Main | ANLP | Andesitic LapilliTuff | Cp,Bn qtz-cb stkwk, Cp dis |
| 14917 | 05CF247 | 75.8 | 78.8 | 3.03 | 77.27 | Liard Main | PPPL | Plagioclase or Feldspar Porphyry | Bn dis, qtz-cb vn |
| 14925 | 05CF247 | 100.0 | 103.0 | 3.03 | 101.52 | Liard Main | ANLP | Andesitic LapilliTuff | Cp qtz-cb vn, dis |
| 14998 | 05CF248 | 36.4 | 39.4 | 3.03 | 37.88 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | STKWK |
| 15862 | 05CF248 | 78.8 | 81.8 | 3.03 | 80.30 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | STKWK, MB-Frct |
| 15870 | 05CF248 | 103.0 | 106.1 | 3.03 | 104.55 | Liard Main | ANLP | Andesitic LapilliTuff | STKWK |
| 15879 | 05CF248 | 130.3 | 133.3 | 3.03 | 131.82 | Liard Main | BRVL | Volcanic Breccia | STKWK |
| 15887 | 05CF248 | 145.5 | 148.5 | 3.03 | 146.97 | Liard Main | ANTF | Andesitic Tuff | STKWK, Dis |
| 15891 | 05CF248 | 157.6 | 160.6 | 3.03 | 159.09 | Liard Main | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite | STKWK |
| 15908 | 05CF248 | 209.1 | 212.1 | 3.03 | 210.61 | Liard Main | PPFQ | Quartz-Feldspar or Feldspar-Quartz Porphyry | STKWK, MB-Frct, Dis, Flt |

## Project:

Client:
Data:
Comments:
Schat Creek
Copper Fox Metals Inc.
Sample information
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Sample <br> Id. | Hole Id | Lithology From (m) | To <br> (m) | Interval <br> (m) | Centre o Interval <br> (m) | Zone | Rock Code | Rock Code Description | Mineralization Style |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15911 | 05CF248 | 218.2 | 221.2 | 3.03 | 219.70 | Liard Main | ANDS | Andesite | STKWK, Dis |
|  |  |  |  |  |  |  | Rock Code Legend: |  |  |
|  |  |  |  |  |  |  | ANDS | Andesite |  |
|  |  |  |  |  |  |  | ANNX | Altered Andesite |  |
|  |  |  |  |  |  |  | ANPF | Plagioclase-phyric or Feldspar-phyric Andesite |  |
|  |  |  |  |  |  |  | ANPL/ANLP | Andesitic Lapilli Tuff |  |
|  |  |  |  |  |  |  | ANTF | Andesitic Tuff |  |
|  |  |  |  |  |  |  | BRIV | Intrusive Breccia or Felsic Igneous Breccia |  |
|  |  |  |  |  |  |  | BRVL | Volcanic Breccia |  |
|  |  |  |  |  |  |  | BRXX | Diorite Breccia |  |
|  |  |  |  |  |  |  | D/BS | Diabase/Basic dyke |  |
|  |  |  |  |  |  |  | DIOR | Diorite |  |
|  |  |  |  |  |  |  | FAUL | Faults |  |
|  |  |  |  |  |  |  | PNBX | Pneumatolytic Breccia |  |
|  |  |  |  |  |  |  | PPAU | Plagioclase-Augite-phyric Andesite |  |
|  |  |  |  |  |  |  | PPFPQ | Quartz-Feldspar or Feldspar-Quartz Porphyry |  |
|  |  |  |  |  |  |  | PPPL | Plagioclase or Feldspar Porphyry |  |
|  |  |  |  |  |  |  | SHER | Shear Zone / Faults |  |
|  |  |  |  |  |  |  | TOBR | Tourmaline Breccia |  |
|  |  |  |  |  |  |  | VN |  |  |

Project:
Data:
Comments:

| Sample Id. | Alteration Minerals |  |  |  |  |  |  |  |  |  | $\begin{gathered} \text { Cp } \\ \text { Chalcopyrite } \end{gathered}$ | $\begin{gathered} \mathrm{Bn} \\ \text { Bornite } \end{gathered}$ | Sulphides \% |  | Other | Total | Assay Data |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ch Chlorite | $\begin{gathered} \text { Ep } \\ \text { Epidote } \end{gathered}$ | $\begin{gathered} \mathrm{Bt} \\ \text { Biotite } \end{gathered}$ | Se <br> Sericite | $\underset{\text { K-spar }}{\text { K }}$ | Si <br> Silicic | $\begin{gathered} \mathrm{Hm} \\ \text { Hematite } \end{gathered}$ | Cb |  |  | Py Pyrite |  | Mb Molybdenite | Cu <br> (\%) |  |  | Mo <br> (\%) | $\begin{gathered} \mathrm{Au} \\ (\mathrm{~g} / \mathrm{t}) \end{gathered}$ | Ag <br> (g/t) |
| 14018 | w | w |  | w | w |  |  |  |  |  |  |  |  | 1.0 |  |  | 1.0 | 0.147 | 0.007 | 0.06 | <0.5 |
| 14021 | M | w |  | M | M | M |  |  | x |  | 2.0 |  | T |  |  | 2.0 | 0.173 | 0.036 | 0.03 | <0.5 |
| 14036 | M |  |  | S | M | M |  |  | X |  | 4.0 |  |  |  |  | 4.0 | 0.189 | 0.061 | 0.04 | 5.8 |
| 14043 | W | w |  | M | M | W |  |  | X |  | 0.0 |  |  |  |  | 2.0 | 0.153 | 0.034 | 0.15 | 2.0 |
| 14060 | M | M |  | M | M? |  | M? |  |  |  | T-1 |  |  |  |  | T-1 | 0.280 | 0.032 | 0.04 | <0.5 |
| 14067 | S | w |  | S | w | w |  |  |  |  | 1.0 |  |  |  |  | 1.0 | 0.247 | 0.014 | 0.03 | <0.5 |
| 14076 | w |  |  |  |  |  |  |  |  |  | T |  | T |  |  | T | 0.173 | 0.005 | 0.16 | <0.5 |
| 14083 | w | w |  |  |  |  |  |  |  |  | T |  | 1.0 |  |  | 1.0 | 0.130 | 0.001 | 0.01 | <0.5 |
| 14099 | w |  |  |  |  |  |  |  |  |  | 0.5 |  | 1.0 |  |  | 1.0 | 0.157 | 0.002 | 0.02 | 1.1 |
| 14103 | w | w |  |  | w |  |  |  | M |  | 1.0 |  | T |  |  | 1.0 | 0.266 | 0.022 | 0.02 | 1.0 |
| 14130 |  |  |  |  | S | w |  |  |  |  | T | $\sim 1$ |  |  |  | 1.0 | 0.555 | 0.008 | 0.39 | 3.3 |
| 14144 | M |  |  |  | M-S | w | M |  |  |  | T | $\sim 1$ |  |  |  | 1.0 | 0.290 | 0.008 | 0.20 | 2.2 |
| 14148 | S |  |  |  | S |  | w |  |  |  |  | T |  |  |  | T | 0.275 | 0.020 | 0.17 | 1.2 |
| 14156 |  |  |  |  | w |  |  |  |  |  |  | T |  | 1.0 |  | 1.0 | 0.204 | 0.005 | 0.07 | 1.0 |
| 14162 |  |  |  |  |  |  |  |  |  | w |  |  |  |  |  |  | 0.115 | 0.051 | 0.09 | <0.5 |
| 14169 |  |  |  |  | M-S |  |  |  |  |  | 1.0 | 1.0 |  | <1 |  | <2 | 0.386 | 0.016 | 0.18 | 3.0 |
| 14232 |  |  |  |  | w |  |  |  |  |  | 0.5 | 1.0 | 0.5 | 0.5 |  | 2.5 | 0.325 | 0.011 | 0.21 | 1.8 |
| 14250 | w |  |  |  | w |  | w |  |  |  | 0.5 | 1.0 | 0.5 | 0.5 |  | 2.5 | 0.300 | 0.038 | 0.33 | 2.0 |
| 14260 | w |  |  |  | w |  | w |  |  |  | 1.0 | 0.5 | 0.5 | T |  | 2.0 | 0.505 | 0.016 | 0.9 | 3.1 |
| 14276 | w | w |  |  |  |  |  |  |  |  | 2.0 | T | 0.5 | 1.0 |  | 3.5 | 0.136 | 0.003 | <0.01 | 1.0 |
| 14295 | w | w |  |  | w |  | w |  |  |  | 0.5 | T | 0.5 | T |  | 1.0 | 0.250 | 0.001 | 0.07 | 0.5 |
| 14301 |  |  |  |  | S |  |  |  |  |  | T |  | T | 0.5 |  | 0.5 | 0.241 | 0.023 | 0.09 | 0.6 |
| 14323 | w |  |  |  | w |  |  |  |  |  | 0.5 | 0.5 | T | T |  | 1.0 | 0.200 | 0.005 | 0.18 | 1.6 |
| 14332 | w |  |  |  | w |  | w |  |  |  | 0.5 | 0.5 | T | 1.0 |  | 2.0 | 0.336 | 0.010 | 0.16 | 1.5 |
| 14345 | w |  |  |  | w |  |  |  |  |  | 2.0 | 0.5 | 0.5 | 0.5 |  | 3.5 | 0.559 | 0.020 | 0.19 | 2.4 |
| 14348 | w |  |  |  | w |  |  |  | w |  | 1.0 | 0.5 | 0.5 | 0.5 |  | 2.5 | 0.461 | 0.013 | 0.13 | 1.4 |
| 14797 | w |  |  |  | w |  |  |  |  |  | 0.5 | 0.5 |  | 0.5 |  | 1.5 | 0.184 | 0.034 | 0.10 | 1.0 |
| 14808 | w |  |  |  | S |  |  |  |  |  | 0.5 | 0.5 |  | 2.0 |  | 3.0 | 0.257 | 0.040 | 0.28 | 1.7 |
| 14816 | w |  |  |  | M |  | w |  |  |  | T | 0.5 | 1.0 | T |  | 1.5 | 0.387 | 0.008 | 0.57 | 2.3 |
| 14828 | w |  |  |  | w |  |  |  |  |  | 0.5 | 2.0 |  | 0.5 |  | 3.0 | 0.317 | 0.019 | 0.74 | 2.3 |
| 14844 | w |  |  |  |  |  |  |  |  |  | 1.0 | 0.5 | 0.5 | T |  | 2.0 | 0.249 | 0.010 | 0.16 | 1.0 |
| 14680 | w |  |  |  | w |  |  |  |  | w | 1.0 | 0.5 |  | 0.5 |  | 2.0 | 0.373 | 0.035 | 0.25 | 2.5 |
| 14871 | W | w |  |  | w |  | w |  |  |  | 2.0 | 0.5 |  | T |  | 2.5 | 0.365 | 0.034 | 0.10 | 0.7 |
| 14887 | w | w |  |  |  |  | w |  |  |  | 0.5 |  | 0.5 |  |  | 1.0 | 0.196 | 0.00 | 0.07 | 0.7 |
| 14689 | w |  |  | w | S |  | x |  |  |  | 0.5 |  | 1.0 | 0.5 |  | 2.0 | 0.213 | 0.008 | 0.07 | 0.4 |
| 14695 | M-S |  |  |  | w |  | w |  |  | T | T |  | 0.5 |  |  | 0.5 | 0.182 | 0.059 | 0.13 | 0.7 |
| 14742 | w |  |  |  | w |  |  | w |  | 1 | T |  |  | 0.5 |  | 0.5 | 0.223 | 0.071 | 0.17 | 1.0 |
| 14666 | w | w |  |  | w |  |  |  |  |  | 0.5 |  | 1.0 | T |  | 1.5 | 0.163 | 0.002 | 0.07 | 0.3 |
| 14685 | w |  |  |  | M |  |  |  |  |  | 0.5 |  | 2.0 | T |  | 2.5 | 0.455 | 0.013 | 0.18 | 0.6 |
| 14685B |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14545 | W-M |  |  |  |  |  | w |  |  |  | T |  | T |  |  | T | 0.113 | 0.001 | 0.02 | 0.4 |
| 14565 | w |  |  |  | w |  | w |  |  |  | T |  |  |  |  | T | 0.289 | 0.002 | 0.14 | 0.6 |
| 14571 | w |  |  |  | w |  | X |  |  |  | 2.0 |  | 1.0 | 0.5 |  | 3.5 | 0.593 | 0.011 | 0.13 | 1.8 |
| 14578 | W-M |  |  |  | W-M |  | X |  |  |  | T |  | 1.0 |  |  | 1.0 | 0.293 | 0.002 | 0.04 | 0.7 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14598 | M |  |  |  |  |  |  |  |  | 5 | T |  | T |  |  | T | 0.075 | 0.005 | 0.02 | 0.3 |
| 14893 | w |  |  |  |  |  |  |  |  | 5 |  |  |  |  |  |  | 0.164 | 0.008 | 0.12 | 0.9 |
| 14899 | x |  |  |  |  |  | x |  |  |  |  |  |  |  |  |  | 0.032 | 0.002 | 0.03 | 0.7 |
| 14908 | w |  |  |  | w |  |  |  |  |  | 1.5 | T |  |  |  | 0.5 | 0.113 | 0.005 | 0.08 | 0.7 |
| 14917 | x |  | x |  | W-M |  |  |  |  |  |  | 0.5 |  |  |  | 0.5 | 0.361 | 0.001 | 0.31 | 2.5 |
| 14925 | w | x |  |  | x |  | w |  |  | 3 | T |  |  |  |  | T | 0.182 | 0.001 | 0.11 | 1.0 |
| 14998 | w |  |  |  |  |  |  |  |  |  | T | T | 0.5 | T |  | 0.5 | 0.169 | 0.007 | 0.14 | 0.5 |
| 15862 | w | w |  |  | w |  |  |  |  |  | T | T |  | 0.5 |  | 0.5 | 0.116 | 0.008 | 0.14 | 0.6 |
| 15870 | w |  |  |  | M |  | w |  |  |  | 0.5 | T | T | 0.5 |  | 1.0 | 0.157 | 0.002 | 0.09 | 0.8 |
| 15879 | w | w |  |  | w |  | w |  |  |  | 0.5 | T |  | T |  | 0.5 | 0.224 | 0.003 | 0.15 | 1.5 |
| 15887 | w | w |  |  |  | w |  | w |  |  | 1.0 | T |  | 0.5 |  | 1.5 | 0.285 | 0.008 | 0.28 | 1.8 |
| 15891 | w |  |  |  | w |  | w |  |  |  | T | 0.5 |  | 0.5 |  | 1.0 | 0.234 | 0.011 | 0.21 | 1.5 |
| 15908 | w |  |  |  |  |  |  |  |  |  | 0.5 | 0.5 |  | 0.5 |  | 1.5 | 0.421 | 0.032 | 0.38 | 2.4 |

Project:
lient:
Data:
Comments

Sample
Id.

15911
chatt Creek
Copper Fox Metals Inc.
Sample Information
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Alteration Minerals |  |  |  |  |  |  |  |  | Sulphides \% |  |  |  |  |  | Assay Data |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ch Ep <br> Chlorite  | Bt Biotite | Se <br> Sericite | $\begin{gathered} \text { K-spar } \end{gathered}$ | $\underset{\text { Silicic }}{\mathrm{Si}}$ |  | Cb | Tm Tourmaline | Mt <br> Magnetite | Cp <br> Chalcopyrite | $B n$ Bornite | Py Pyrite | Mb Molybdenite | Other | Total | Cu <br> (\%) | Mo (\%) | $\begin{gathered} \mathrm{Au} \\ (\mathrm{~g} / \mathrm{t}) \end{gathered}$ | Ag <br> (g/t) |
| w |  |  | w |  |  |  |  |  | 0.5 | 0.5 |  | 0.5 |  | 1.5 | 0.179 | 0.017 | 0.15 | 1.0 |
| Mineral Legend: |  |  |  |  |  |  |  |  | Mineral Lege | nd: |  |  |  |  |  |  |  | Legend: |
| Ch | Chlorite |  |  |  | T | Trace |  |  | Ch | Chlorite |  |  |  |  |  |  |  | T |
| Ep | Epidote |  |  |  | W | weak |  |  | Ep | Epidote |  |  |  |  |  |  |  | w |
| Bt | Biotite |  |  |  | M | moderate |  |  | Bt | Biotite |  |  |  |  |  |  |  | M |
| Se | Sericite |  |  |  | S | strong |  |  | Se | Sericite |  |  |  |  |  |  |  | S |
| K | K-spar |  |  |  |  |  |  |  | K | K-spar |  |  |  |  |  |  |  |  |
| Si | Silicic |  |  |  |  |  |  |  | Si | Silicic |  |  |  |  |  |  |  |  |
| Hm | Hematite |  |  |  |  |  |  |  | Hm | Hematite |  |  |  |  |  |  |  |  |
| Mt | Magnetite |  |  |  |  |  |  |  | Mt | Magnetite |  |  |  |  |  |  |  |  |
| Tm | Tourmaline |  |  |  |  |  |  |  | Tm | Tourmaline |  |  |  |  |  |  |  |  |
| Cp | Chalcopyrit |  |  |  |  |  |  |  | Cp | Chalcopyrit |  |  |  |  |  |  |  |  |
| Bn | Bornite |  |  |  |  |  |  |  | Bn | Bornite |  |  |  |  |  |  |  |  |
| Py | Pyrite |  |  |  |  |  |  |  | Py | Pyrite |  |  |  |  |  |  |  |  |
| Mb | Molybdenit |  |  |  |  |  |  |  | Mb | Molybdenit |  |  |  |  |  |  |  |  |
| Oth | See descri |  |  |  |  |  |  |  | Oth | See descri |  |  |  |  |  |  |  |  |
| x | mineral pre | sent |  |  |  |  |  |  | x | mineral pre |  |  |  |  |  |  |  |  |

Sample


 replacement of hornblende. -From 18.6-19.8 m: fairly wide vein ( $\sim 1 \mathrm{~cm}$ ) hosting notable pyrite and possible chalcopyrite.
Tourmaline Breccia. Unit is primarily porphyritic quartz-feldspar with primarily medium-grained plagioclase phenocrysts. "Wall-rock" is identical to the unit described above, and this unit is really the same lithology having undergone intense





 restricted almost exclusively to the hydrothermal veins.

 entire hole reflecting the variable degree of fracturing as a result of a violent fluid event. Photo 14 taken of box 39 showing typical stockwork texture ( $82.0-84.1 \mathrm{~m}$ ).

 igneous breccia unit. (sample 05-JES-228 was also collected from this interval).


 possibly were filling fractures. These minor veins are typically $<2 \mathrm{~mm}$ wide.
Fine grained andesite. Weak brecciation and veining: epidote-carb-quartz, accessory pyrite, in part vuggy. Strong fracturing, low angle CA. Core rubbly. 1-2\% pyrite, disseminated, associated with fractures.
Andesite. Fine grained,similar to 15.8 m . Strongly fractured, moderately veined (epidote-carb-quartz). Locally developed as breccia.

 to $1 \%$ each pyrite, chalcopyrite.

 clasts.

 section.
 gouge and breccia along 30 cm length with a 20 cm section at 61.9 m of a low angle hematized vein breccia.

 rich zones.
Fault Zone - Tectonic Deformation and Alteration Zone. 87.2-96.0 m relict protolith of possible feldspar porphyry displaying variable K-alteration.

 quartz veins with $10 \%$ bornite along 10 cm length.

 painted along fracture planes trace chalcopyrite. Typically the fractures are at a low-medium angle and average 1 per meter
 spacing: Quartz veins, carbonate veins, talc(?)-chlorite veins. Total sulphides $2 \%: 0.5 \%$ each, bornite, chalcopyrite, pyrite in veins and adjacent to veins. Very fine chalcopyrite commonly replacing augite crystals.
 strongly variable, generally low abundance.
 strongly variable, generally low abundance. $96.0-106.7 \mathrm{~m}$ Alternating weak chlorite alteration and weak potassic alteration. Weak quartz-carbonate stockwork, $\sim 0.5 \%$ each chalcopyrite, bornite, pyrite, trace molybdenite,


 chlorite alteration. Low vein density. Rare 1 mm massive chalcopyrite veins and molybdenite coated slickensides, fractures.

Sample



 sulphides: 0.5-1\% of each chalcopyrite, pyrite, in veins, halos.
 appears to overprint the K-alteration, and may in part be epidote and serictic alteration. Areas of intense K-alteration completely obliterate protolith and are usually associated with stockwork arrray of mm-cm carbonate-quartz veins containing disseminated molybdenite and bornite. 10.8-12.8 m medium grey-green, fine grained with mm carbonate amygdules and mm low angle carbonate veinng. Possibly a late mafic dyke.
 weak pervasive chloritization. Low to medium angle carbonate-chlorite fractures averaging $6 / \mathrm{meter}$.
 weak pervasive chloritization. Low to medium angle carbonate-chlorite fractures averaging $6 /$ meter.

 carrying up to $7 \%$, and forming a stockwork array with diffuse boundaries and does not appear to be vein associated. More of a late mineralization phase which may also be contributing to painted molybdenite on fracture planes Augite-Phyric Andesite. Fractured containing carbonate-chlorite filling and K -alteration envelopes on a mm-cm scale. Upper contact is fault controlled at high angle.
 Moderate pervasive chloritization along meter lengths, accompanied by intense chlorite hairline chlorite veinlets forming a crackle breccia. Overall $5 \%$ magnetite

 cm sections of fault gouge. $\mathrm{Mm}-\mathrm{cm}$ medium to high angle quartz-carbonate -chlorite veins some heavily mineralized with bornite.
 96.9-104.8 m; mm randomly oriented quartz-carbonate veins forming a weak stockwork array

Andesite. Grey, fine grain, masive, Incipient crackle brecciation developed by hairline to 3 mm randomly oriented carbonate veinlets. Rare 5 mm quartz-carbonate veins with bornite. Rare molybdenite painted fractures.
Augite-Feldspar-Phyric Andesite. Grey-green, massive with weak patchy K-alteration, rare mm epidote and darker blotchy areas of high magnetite. Mm randomly oriented quartz-carbonate veins with molybdenite and bornite, about $2 /$ meter

 sharp high angle contacts
Andesitic Tuff. Massive fine grain rock displaying weak low angle bedding and intercalated lithic tuff horizons. Weak epidote forming cm patches.
Feldspar-porphyry. Massive, competent. Pink colour, potassic alteration. Rock made up of very fine grained felsic groundmass and ~20\% white feldspar phenocrysts and $1-2 \%$ yellowish, boxy, altered phenocrysts showing relict cleavage
 veins, chlorite veins, pink carbonate-hematite veins. Accessory chalcopyrite, molybdenite in veins.

 hematite, chlorite. 29.1-29.4 m 3cm quartz-carbonate vein 45CA and 3 cm strongly molybdenite-coated vein and fault 75CA (i.e. subhorizontal).
Lapilli andesite and andesite, variously textured and altered. Unit divided into subdivisions 155.7-164.3 m ANLP Colour medium grey. Weak chloritic and potassic alteration. Low vein density, medium angle


 inclusions, up to $10 \%$ by volume.
 massive with a low vein density.


 vide pink halos. Sulphides. Trace to accessory pyrite, chalcopyrite, bornite in rare mm size patches, veins and disseminations. Rare 5 -10mm size chalcopyrite patches or discontinuous veins
 chalcopyrite as a) disseminations, mm patches; $b$ ) in thin veins

 85.3 m . Lower contact irregular: PPPL and ANPF are intertwined, fine grained andesite being broken up and intruded by medium grained plagioclase porphyry.

## Project: <br> chat Creek

lient:
Data:
Metals
Comments: Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps
 breccia of dark veins, low angle, carbonate-chlorite-veins. 102.1-102.4 m Several 1 mm high-molybdenite slickensides; at 108.5 m one 4 cm quartz vein with $2 \%$ molybdenite. Overall accessory chalcopyrite, bornite, molybdenite.

4578 medium angle. Several $1-5 \mathrm{~cm}$ carbonate-chlorite-veins and vein breccia with high sulphide abundance (several \% of coarse grained chalcopyrite, pyrite, molybdenite)
Plagioclase-phyric and augite-phyric andesite. Fine grained, massive, competent core. Fine grained, felsic, igneous grondmass hosting 20\% 0.2-2mm plagioclase phenocrysts; and 1-5\% dark, altered augite phenocrysts. Variable phenocryst

 green grey with minor medium brown grey portions. Strongly fractured, rusty, limonitic, in part with malachite coating
lagioclase-phyric and augite-phyric andesite. Fine grained, massive, competent core. Fine grained, felsic, igneous grondmass hosting 20\% 0.2-2mm plagioclase phenocrysts; and 1-5\% dark, altered augite phenocrysts. Variable phenocryst
 ANDS, fine veins. Scattered portions ( $0.3-1.5 \mathrm{~m}$ )
 Generally low vein density, but slightly higher than above: cm to dm spacing, medium angle.

 chalcopyrite. Quartz veins in part vuggy, open. Sharp contact 60CA


 sulphides abundanc: 84.7-85.0m; 87.8-88.4m; 91.1-91.4m; 99.4-100.0m; 100.6-101.8m; 110.9-112.8m; 114.3-114.9m; 117.3-118.0m; 120.7-121.9m; 127.7-128.3m; 134.1-137.1m
 $1 / 2 \mathrm{~cm}$ quartz-carbonate-chlorite veins forming dm sections of stockworks, variably mineralized with chalcopyrite, bornite and molybdenite. Occasional molybdenite painted fracture surfaces. Late mm unmineralized arbonate veins.
 stockworks. 75.4-91.4 m; high fracture and fault density at variable angles from low to high associated with carbonate-chlorite veins. Occasional molybdenite painted fracture surfaces.

 veins. Rare cm sections of highly comminuted rock forming bands at medium to high angle. Vuggy veins associated with carbonate phase. Cm sections of K-alteration, vein related.

 selvages manifest as grey tones overprinting an earlier pervasive alteration event of carbonate-sericite soaking the protolith. Fine mm scale bedding oriented at very low angle to core. Sharp high angle lower contact
 veins. 158.8 m ; very low angle carbonate-quartz vein brecciating host rock, displaying moderate K -alteration. Fault associated vein walls
Feldspar-Quartz Porphyry. Andedral to subhedral feldspar phenocrysts and anhedral quartz compacted into a massive rock with disseminated chalcopyrite.
Andesite. Green-grey. Pervasive carbonatization and chloritization, with cm sections of intense carbonatization. $10 \%$ angular to round oxide inclusions. Minor bornite and chalcopyrite associated with quartz-carbonate veins.

Project:
Client:
Comments:

Schaft Creek
Copper Fox Metals Inc.
ABA Data
pH of DI water used for paste pH read ???

| Sample <br> Id. | Paste pH | S (Total) | S (Sulphide) | S (Sulphide) | Carbonate Leach S (Sulphate) | HCI Leachable <br> S (Sulphate) | S (Sulphate) | $\mathrm{S}\left(\mathrm{BaSO}_{4}\right)$ | S (del ${ }_{\text {actual }}$ ) | S(del) | TAP | SAP | PAP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Unity | (\% Leco) | (\% Leco) | (\% Calc) | (\%) | (\%) | (\% HCl/Carb) | (\%) | (\%) | (\%) | ( kg CaCO 3 /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\left.\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}\right)$ |
| Method | OA-ELE07 | S-IR08 | S-IR07 | s-CALO6 | s-GRA06 | s-gra06a |  | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated |
| MDL | 0.1 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |  |  |  |  |  |  |  |
| 14018 | 7.6 | 0.8 | 0.69 | 0.795 | 0.02 | 0.005 | 0.005 | 0.027 | 0.078 | 0.078 | 25.0 | 24.0 | 19.7 |
| 14021 | 7.9 | 0.62 | 0.6 | 0.615 | 0.03 | 0.005 | 0.005 | 0.010 | 0.005 | 0.005 | 19.4 | 18.9 | 12.5 |
| 14036 | 7.9 | 1.47 | 1.39 | 1.465 | 0.02 | 0.005 | 0.005 | 0.013 | 0.062 | 0.062 | 45.9 | 45.4 | 37.8 |
| 14043 | 8.2 | 0.26 | 0.22 | 0.255 | 0.02 | 0.005 | 0.005 | 0.006 | 0.029 | 0.029 | 8.1 | 7.8 | 2.8 |
| 14060 | 8 | 1.31 | 0.62 | 0.6 | 0.74 | 0.71 | 0.71 | 0.008 | -0.028 | 0.000 | 40.9 | 19.4 | 10.6 |
| 14067 | 8.4 | 0.4 | 0.41 | 0.395 | 0.01 | 0.005 | 0.005 | 0.008 | -0.023 | 0.000 | 12.5 | 12.8 | 4.7 |
| 14076 | 8.2 | 0.77 | 0.76 | 0.765 | 0.01 | 0.005 | 0.005 | 0.010 | -0.005 | 0.000 | 24.1 | 23.8 | 19.1 |
| 14083 | 8.2 | 1.46 | 1.35 | 1.455 | 0.03 | 0.005 | 0.005 | 0.017 | 0.088 | 0.088 | 45.6 | 44.9 | 40.4 |
| 14099 | 8.1 | 0.34 | 0.28 | 0.335 | 0.03 | 0.005 | 0.005 | 0.021 | 0.034 | 0.034 | 10.6 | 9.8 | 5.6 |
| 14103 | 8 | 0.69 | 0.25 | 0.27 | 0.45 | 0.42 | 0.42 | 0.006 | 0.014 | 0.014 | 21.6 | 8.2 | 0.2 |
| 14130 | 8.3 | 0.29 | 0.29 | 0.285 | 0.03 | 0.005 | 0.005 | 0.013 | -0.018 | 0.000 | 9.1 | 9.1 | 0.2 |
| 14144 | 8 | 0.26 | 0.2 | 0.255 | 0.02 | 0.005 | 0.005 | 0.008 | 0.047 | 0.047 | 8.1 | 7.7 | 0.2 |
| 14148 | 7.6 | 0.14 | 0.04 | 0.135 | 0.02 | 0.005 | 0.005 | 0.015 | 0.080 | 0.080 | 4.4 | 3.8 | 0.2 |
| 14156 | 7.7 | 0.17 | 0.14 | 0.165 | 0.04 | 0.005 | 0.005 | 0.006 | 0.019 | 0.019 | 5.3 | 5.0 | 0.2 |
| 14162 | 7.9 | 0.13 | 0.12 | 0.125 | 0.02 | 0.005 | 0.005 | 0.013 | -0.008 | 0.000 | 4.1 | 3.8 | 0.2 |
| 14169 | 8.1 | 0.3 | 0.29 | 0.295 | 0.01 | 0.005 | 0.005 | 0.002 | 0.003 | 0.003 | 9.4 | 9.2 | 0.2 |
| 14232 | 8.3 | 0.15 | 0.14 | 0.145 | 0.005 | 0.005 | 0.005 | 0.004 | 0.001 | 0.001 | 4.7 | 4.4 | 0.2 |
| 14250 | 8.3 | 0.19 | 0.19 | 0.185 | 0.01 | 0.005 | 0.005 | 0.004 | -0.009 | 0.000 | 5.9 | 5.9 | 0.2 |
| 14260 | 8.4 | 0.34 | 0.34 | 0.335 | 0.01 | 0.005 | 0.005 | 0.004 | -0.009 | 0.000 | 10.6 | 10.6 | 0.2 |
| 14276 | 8.5 | 0.17 | 0.14 | 0.165 | 0.01 | 0.005 | 0.005 | 0.025 | 0.000 | 0.000 | 5.3 | 4.4 | 0.2 |
| 14295 | 8.6 | 0.44 | 0.41 | 0.435 | 0.005 | 0.005 | 0.005 | 0.002 | 0.023 | 0.023 | 13.8 | 13.5 | 6.1 |
| 14301 | 8.6 | 0.34 | 0.32 | 0.335 | 0.01 | 0.005 | 0.005 | 0.006 | 0.009 | 0.009 | 10.6 | 10.3 | 2.1 |
| 14323 | 8.6 | 0.15 | 0.13 | 0.145 | 0.005 | 0.005 | 0.005 | 0.006 | 0.009 | 0.009 | 4.7 | 4.3 | 0.2 |
| 14332 | 8.6 | 0.26 | 0.26 | 0.255 | 0.01 | 0.005 | 0.005 | 0.004 | -0.009 | 0.000 | 8.1 | 8.1 | 0.2 |
| 14345 | 8.4 | 0.52 | 0.52 | 0.515 | 0.005 | 0.005 | 0.005 | 0.004 | -0.009 | 0.000 | 16.3 | 16.3 | 0.2 |
| 14348 | 8.3 | 0.44 | 0.45 | 0.435 | 0.01 | 0.005 | 0.005 | 0.004 | -0.019 | 0.000 | 13.8 | 14.1 | 0.2 |
| 14797 | 8.1 | 0.08 | 0.05 | 0.075 | 0.005 | 0.005 | 0.005 | 0.004 | 0.021 | 0.021 | 2.5 | 2.2 | 0.2 |
| 14808 | 7.8 | 0.18 | 0.16 | 0.175 | 0.005 | 0.005 | 0.005 | 0.004 | 0.011 | 0.011 | 5.6 | 5.3 | 0.2 |
| 14816 | 7.6 | 0.46 | 0.46 | 0.45 | 0.005 | 0.01 | 0.01 | 0.004 | -0.014 | 0.000 | 14.4 | 14.4 | 1.7 |
| 14828 | 7.6 | 0.13 | 0.1 | 0.125 | 0.02 | 0.005 | 0.005 | 0.017 | 0.008 | 0.008 | 4.1 | 3.4 | 0.2 |
| 14844 | 7.7 | 0.21 | 0.2 | 0.2 | 0.005 | 0.01 | 0.01 | 0.008 | -0.008 | 0.000 | 6.6 | 6.3 | 0.2 |
| 14680 | 7.7 | 0.22 | 0.2 | 0.215 | 0.01 | 0.005 | 0.005 | 0.006 | 0.009 | 0.009 | 6.9 | 6.5 | 0.2 |
| 14871 | 7.6 | 0.37 | 0.32 | 0.365 | 0.02 | 0.005 | 0.005 | 0.002 | 0.043 | 0.043 | 11.6 | 11.3 | 0.2 |
| 14887 | 7.8 | 0.44 | 0.42 | 0.41 | 0.01 | 0.03 | 0.03 | 0.008 | -0.018 | 0.000 | 13.8 | 13.1 | 6.8 |
| 14689 | 8.2 | 0.68 | 0.69 | 0.675 | 0.01 | 0.005 | 0.005 | 0.002 | -0.017 | 0.000 | 21.3 | 21.6 | 15.0 |
| 14695 | 8.2 | 0.14 | 0.13 | 0.135 | 0.005 | 0.005 | 0.005 | 0.004 | 0.001 | 0.001 | 4.4 | 4.1 | 0.2 |
| 14742 | 8.2 | 0.19 | 0.19 | 0.185 | 0.005 | 0.005 | 0.005 | 0.004 | -0.009 | 0.000 | 5.9 | 5.9 | 0.2 |
| 14666 | 8.1 | 0.32 | 0.31 | 0.315 | 0.01 | 0.005 | 0.005 | 0.008 | -0.003 | 0.000 | 10.0 | 9.7 | 5.0 |
| 14685 | 8.1 | 1.79 | 1.8 | 1.785 | 0.01 | 0.005 | 0.005 | 0.010 | -0.025 | 0.000 | 55.9 | 56.3 | 42.3 |
| 14685B | 7.9 | 1.95 | 1.8 | 1.945 | 0.01 | 0.005 | 0.005 | 0.008 | 0.137 | 0.137 | 60.9 | 60.5 | 45.9 |
| 14545 | 7.8 | 0.19 | 0.13 | 0.185 | 0.01 | 0.005 | 0.005 | 0.021 | 0.034 | 0.034 | 5.9 | 5.1 | 1.2 |
| 14565 | 7.8 | 0.23 | 0.24 | 0.225 | 0.005 | 0.005 | 0.005 | 0.004 | -0.019 | 0.000 | 7.2 | 7.5 | 0.2 |
| 14571 | 7.8 | 1.04 | 1.03 | 1.035 | 0.02 | 0.005 | 0.005 | 0.010 | -0.005 | 0.000 | 32.5 | 32.2 | 14.7 |
| 14578 | 7.9 | 1.82 | 1.82 | 1.815 | 0.02 | 0.005 | 0.005 | 0.015 | -0.020 | 0.000 | 56.9 | 56.9 | 47.4 |
| 14578B | 7.9 | 1.93 | 1.91 | 1.925 | 0.03 | 0.005 | 0.005 | 0.019 | -0.004 | 0.000 | 60.3 | 59.7 | 49.2 |
| 14598 | 8.1 | 0.13 | 0.13 | 0.125 | 0.01 | 0.005 | 0.005 | 0.004 | -0.009 | 0.000 | 4.1 | 4.1 | 1.7 |
| 14893 | 8 | 0.11 | 0.08 | 0.07 | 0.005 | 0.04 | 0.04 | 0.010 | -0.020 | 0.000 | 3.4 | 2.5 | 0.2 |
| 14899 | 8.1 | 0.02 | 0.02 | 0.015 | 0.005 | 0.005 | 0.005 | 0.008 | -0.013 | 0.000 | 0.6 | 0.6 | 0.2 |
| 14908 | 8.1 | 0.08 | 0.07 | 0.075 | 0.005 | 0.005 | 0.005 | 0.017 | -0.012 | 0.000 | 2.5 | 2.2 | 0.2 |
| 14917 | 8.2 | 0.19 | 0.16 | 0.185 | 0.005 | 0.005 | 0.005 | 0.019 | 0.006 | 0.006 | 5.9 | 5.2 | 0.2 |
| 14925 | 7.9 | 0.14 | 0.12 | 0.135 | 0.005 | 0.005 | 0.005 | 0.008 | 0.007 | 0.007 | 4.4 | 4.0 | 0.2 |
| 14998 | 7.8 | 0.13 | 0.12 | 0.125 | 0.005 | 0.005 | 0.005 | 0.006 | -0.001 | 0.000 | 4.1 | 3.8 | 0.2 |
| 15862 | 7.9 | 0.08 | 0.03 | 0.075 | 0.005 | 0.005 | 0.005 | 0.006 | 0.039 | 0.039 | 2.5 | 2.1 | 0.2 |
| 15870 | 8 | 0.13 | 0.09 | 0.125 | 0.02 | 0.005 | 0.005 | 0.025 | 0.010 | 0.010 | 4.1 | 3.1 | 0.2 |
| 15879 | 8 | 0.12 | 0.09 | 0.115 | 0.02 | 0.005 | 0.005 | 0.019 | 0.006 | 0.006 | 3.8 | 3.0 | 0.2 |
| 15887 | 8 | 0.31 | 0.29 | 0.305 | 0.01 | 0.005 | 0.005 | 0.010 | 0.005 | 0.005 | 9.7 | 9.2 | 0.2 |

Project:
Client
Comments:

## Sample

Id.

MDL
15891
15908
Maximum
Minimum
Mean
Standard Deviation
10 Percentile
25 Percen
75 Percent
90 Percentile

## Interquartile Range (IQR) ${ }^{1}$

Variance
Soefficient of Variation (CoV)

Count
Total
NPR < 1.0 or NPR $=1.0$
$1.0<$ NPR < 2.0
NPR $>2.0$ or NPR $=2.0$
\% NPR < 1.0 or NPR = 1.0 of Total
$\% 1.0$ < NPR < 2.0 of Total
\% NPR > 2.0 or NPR =2.0 of Total

Schaft Creek
Copper Fox Metals Inc.
ABA Data
Sampled by MDAG on Feb 7 '07.
pH of DI water used for paste pH read ???

| Paste pH | S (Total) | S (Sulphide) | S (Sulphide) | Carbonate Leach <br> S (Sulphate) | HCI Leachable <br> S (Sulphate) | S (Sulphate) | $\mathrm{S}\left(\mathrm{BaSO}_{4}\right)$ | S(del ${ }_{\text {actual }}$ ) | S(del) | TAP | SAP | PAP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Unity | (\% Leco) | (\% Leco) | (\% Calc) | (\%) | (\%) | (\% HCI/Carb) | (\%) | (\%) | (\%) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( kg CaCO 3 /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) |
| OA-ELE07 | S-IR08 | S-IR07 | s-CAL06 | S-GRA06 | S-GRA06a |  | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated |
| 0.1 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |  |  |  |  |  |  |  |
| 7.8 | 0.14 | 0.09 | 0.135 | 0.02 | 0.005 | 0.005 | 0.031 | 0.014 | 0.014 | 4.4 | 3.2 | 0.2 |
| 7.8 | 0.22 | 0.2 | 0.215 | 0.02 | 0.005 | 0.005 | 0.006 | 0.009 | 0.009 | 6.9 | 6.5 | 0.2 |
| 7.9 | 0.09 | 0.07 | 0.085 | 0.01 | 0.005 | 0.005 | 0.010 | 0.005 | 0.005 | 2.8 | 2.3 | 0.2 |
| 8.6 | 1.95 | 1.91 | 1.94 | 0.74 | 0.71 | 0.71 | 0.031 | 0.14 | 0.14 | 60.9 | 60.5 | 49.2 |
| 7.6 | 0.02 | 0.02 | 0.015 | 0.005 | 0.005 | 0.005 | 0.0021 | -0.028 | 0 | 0.62 | 0.62 | 0.16 |
| 8.04 | 0.45 | 0.41 | 0.43 | 0.033 | 0.025 | 0.025 | 0.01 | 0.0089 | 0.015 | 14.1 | 13.2 | 6.75 |
| 0.27 | 0.5 | 0.48 | 0.49 | 0.11 | 0.11 | 0.11 | 0.0068 | 0.031 | 0.027 | 15.7 | 15.3 | 13.5 |
| 7.7 | 0.12 | 0.078 | 0.11 | 0.005 | 0.005 | 0.005 | 0.0042 | -0.019 | 0 | 3.69 | 2.9 | 0.16 |
| 7.8 | 0.14 | 0.13 | 0.14 | 0.005 | 0.005 | 0.005 | 0.0042 | -0.0092 | 0 | 4.38 | 4.08 | 0.16 |
| 8 | 0.26 | 0.22 | 0.26 | 0.01 | 0.005 | 0.005 | 0.0084 | 0.0029 | 0.0029 | 8.12 | 7.71 | 0.16 |
| 8.2 | 0.45 | 0.44 | 0.44 | 0.02 | 0.005 | 0.005 | 0.013 | 0.014 | 0.014 | 14.1 | 13.8 | 5.33 |
| 8.4 | 1.34 | 1.09 | 1.12 | 0.03 | 0.006 | 0.006 | 0.019 | 0.044 | 0.044 | 41.9 | 34.7 | 23.4 |
| 0.4 | 0.31 | 0.3 | 0.3 | 0.015 | 0 | 0 | 0.0084 | 0.023 | 0.014 | 9.69 | 9.72 | 5.18 |
| 0.074 | 0.25 | 0.23 | 0.24 | 0.012 | 0.011 | 0.011 | 0.000047 | 0.00095 | 0.00071 | 246 | 234 | 182 |
| 0.37 | 1.93 | 2.08 | 2.11 | 5.72 | 5.79 | 5.79 | 1.24 | 1.97 | 2.67 | 1.93 | 2.09 | 2.25 |
| 0.034 | 1.11 | 1.18 | 1.15 | 3.34 | 4.2 | 4.2 | 0.68 | 3.47 | 1.83 | 1.11 | 1.16 | 2 |
| 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 |

Project:
Client:
Comments:

| Sample <br> Id. | NP | Available NP | Total C | Inorganic <br> C | Inorganic $\mathrm{CO}_{2}$ | Excess C | Total CaNP | Inorganic CaNP | $\begin{aligned} & \text { (Ca) } \\ & \text { CaNP } \end{aligned}$ | $\begin{aligned} & (\mathrm{Ca}+\mathrm{Mg}) \\ & \mathrm{CaNP} \end{aligned}$ | TNNP | Adjusted <br> TNNP | SNNP | Adjusted SNNP | PNNP | Adjusted PNNP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\left(\mathrm{kg} \mathrm{CaCO}_{3} \mathrm{tt}\right)$ | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | (\% Leco) | (\%) | (\%) | (\%) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | $\left(\mathrm{kg} \mathrm{CaCO}_{3}{ }^{\text {t }}\right.$ ) |
| Method | OA-VOL08 | Calculated | C-IR07 | C-GAS05 | C-GAS05 | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated |
| MDL | 1 |  | 0.01 | 0.05 | 0.2 |  |  |  |  |  |  |  |  |  |  |  |
| 14018 | 42 | 32 | 0.4 | 0.38 | 1.4 | 0.02 | 33.3 | 31.8 | 44.5 | 88.5 | 17.0 | 7.0 | 18.0 | 8.0 | 22.3 | 12.3 |
| 14021 | 64 | 54 | 0.76 | 0.72 | 2.6 | 0.04 | 63.3 | 59.1 | 65.4 | 103.3 | 44.6 | 34.6 | 45.1 | 35.1 | 51.5 | 41.5 |
| 14036 | 49 | 39 | 0.52 | 0.48 | 1.8 | 0.04 | 43.3 | 40.9 | 45.9 | 83.4 | 3.1 | -6.9 | 3.6 | -6.4 | 11.2 | 1.2 |
| 14043 | 40 | 30 | 0.33 | 0.21 | 0.8 | 0.12 | 27.5 | 18.2 | 35.0 | 113.2 | 31.9 | 21.9 | 32.2 | 22.2 | 37.2 | 27.2 |
| 14060 | 41 | 31 | 0.29 | 0.28 | 1 | 0.01 | 24.2 | 22.7 | 78.4 | 164.9 | 0.1 | -9.9 | 21.6 | 11.6 | 30.4 | 20.4 |
| 14067 | 49 | 39 | 0.41 | 0.35 | 1.3 | 0.06 | 34.2 | 29.6 | 64.7 | 175.0 | 36.5 | 26.5 | 36.2 | 26.2 | 44.3 | 34.3 |
| 14076 | 66 | 56 | 0.71 | 0.7 | 2.6 | 0.01 | 59.2 | 59.1 | 108.4 | 211.3 | 41.9 | 31.9 | 42.3 | 32.3 | 46.9 | 36.9 |
| 14083 | 74 | 64 | 0.85 | 0.83 | 3 | 0.02 | 70.8 | 68.2 | 100.6 | 173.5 | 28.4 | 18.4 | 29.1 | 19.1 | 33.6 | 23.6 |
| 14099 | 78 | 68 | 0.92 | 0.92 | 3.4 | 0 | 76.7 | 77.3 | 73.7 | 107.4 | 67.4 | 57.4 | 68.2 | 58.2 | 72.4 | 62.4 |
| 14103 | 85 | 75 | 0.9 | 0.87 | 3.2 | 0.03 | 75.0 | 72.8 | 73.2 | 126.3 | 63.4 | 53.4 | 76.8 | 66.8 | 84.8 | 74.8 |
| 14130 | 91 | 81 | 1.18 | 1.19 | 4.4 | 0 | 98.3 | 100.1 | 65.4 | 107.4 | 81.9 | 71.9 | 81.9 | 71.9 | 90.8 | 80.8 |
| 14144 | 116 | 106 | 1.43 | 1.37 | 5 | 0.06 | 119.2 | 113.7 | 93.6 | 141.4 | 107.9 | 97.9 | 108.3 | 98.3 | 115.8 | 105.8 |
| 14148 | 170 | 160 | 1.92 | 1.9 | 7 | 0.02 | 160.0 | 159.2 | 115.6 | 193.4 | 165.6 | 155.6 | 166.2 | 156.2 | 169.8 | 159.8 |
| 14156 | 73 | 63 | 0.88 | 0.86 | 3.2 | 0.02 | 73.3 | 72.8 | 61.7 | 94.2 | 67.7 | 57.7 | 68.0 | 58.0 | 72.8 | 62.8 |
| 14162 | 219 | 209 | 2.3 | 2.28 | 8.4 | 0.02 | 191.7 | 191.0 | 139.6 | 247.5 | 214.9 | 204.9 | 215.3 | 205.3 | 218.8 | 208.8 |
| 14169 | 64 | 54 | 0.7 | 0.69 | 2.5 | 0.01 | 58.3 | 56.9 | 57.9 | 74.4 | 54.6 | 44.6 | 54.8 | 44.8 | 63.8 | 53.8 |
| 14232 | 89 | 79 | 0.93 | 0.87 | 3.2 | 0.06 | 77.5 | 72.8 | 66.4 | 103.9 | 84.3 | 74.3 | 84.6 | 74.6 | 88.8 | 78.8 |
| 14250 | 118 | 108 | 1.14 | 1.12 | 4.1 | 0.02 | 95.0 | 93.2 | 101.6 | 179.0 | 112.1 | 102.1 | 112.1 | 102.1 | 117.8 | 107.8 |
| 14260 | 100 | 90 | 1.03 | 1.02 | 3.7 | 0.01 | 85.8 | 84.1 | 75.9 | 133.1 | 89.4 | 79.4 | 89.4 | 79.4 | 99.8 | 89.8 |
| 14276 | 47 | 37 | 0.43 | 0.25 | 0.9 | 0.18 | 35.8 | 20.5 | 107.6 | 175.2 | 41.7 | 31.7 | 42.6 | 32.6 | 46.8 | 36.8 |
| 14295 | 111 | 101 | 1.05 | 0.95 | 3.5 | 0.1 | 87.5 | 79.6 | 97.6 | 161.5 | 97.3 | 87.3 | 97.5 | 87.5 | 104.9 | 94.9 |
| 14301 | 136 | 126 | 1.56 | 1.54 | 5.7 | 0.02 | 130.0 | 129.6 | 91.4 | 142.5 | 125.4 | 115.4 | 125.7 | 115.7 | 133.9 | 123.9 |
| 14323 | 73 | 63 | 0.88 | 0.84 | 3.1 | 0.04 | 73.3 | 70.5 | 93.6 | 133.2 | 68.3 | 58.3 | 68.7 | 58.7 | 72.8 | 62.8 |
| 14332 | 95 | 85 | 0.84 | 0.74 | 2.7 | 0.1 | 70.0 | 61.4 | 84.7 | 127.5 | 86.9 | 76.9 | 86.9 | 76.9 | 94.8 | 84.8 |
| 14345 | 79 | 69 | 0.73 | 0.44 | 1.6 | 0.29 | 60.8 | 36.4 | 63.7 | 106.1 | 62.8 | 52.8 | 62.8 | 52.8 | 78.8 | 68.8 |
| 14348 | 59 | 49 | 0.61 | 0.6 | 2.2 | 0.01 | 50.8 | 50.0 | 53.7 | 103.5 | 45.3 | 35.3 | 44.9 | 34.9 | 58.8 | 48.8 |
| 14797 | 125 | 115 | 1.43 | 1.39 | 5.1 | 0.04 | 119.2 | 116.0 | 94.4 | 157.0 | 122.5 | 112.5 | 122.8 | 112.8 | 124.8 | 114.8 |
| 14808 | 172 | 162 | 2.23 | 2.21 | 8.1 | 0.02 | 185.8 | 184.2 | 121.6 | 188.7 | 166.4 | 156.4 | 166.7 | 156.7 | 171.8 | 161.8 |
| 14816 | 133 | 123 | 1.59 | 0.27 | 1 | 1.32 | 132.5 | 22.7 | 83.2 | 153.2 | 118.6 | 108.6 | 118.6 | 108.6 | 131.3 | 121.3 |
| 14828 | 143 | 133 | 1.7 | 1.69 | 6.2 | 0.01 | 141.7 | 141.0 | 108.4 | 183.3 | 138.9 | 128.9 | 139.6 | 129.6 | 142.8 | 132.8 |
| 14844 | 75 | 65 | 0.51 | 0.47 | 1.7 | 0.04 | 42.5 | 38.7 | 70.4 | 226.5 | 68.4 | 58.4 | 68.8 | 58.8 | 74.8 | 64.8 |
| 14680 | 102 | 92 | 1.06 | 1.05 | 3.8 | 0.01 | 88.3 | 86.4 | 103.4 | 171.3 | 95.1 | 85.1 | 95.5 | 85.5 | 101.8 | 91.8 |
| 14871 | 88 | 78 | 0.76 | 0.73 | 2.7 | 0.03 | 63.3 | 61.4 | 84.9 | 164.0 | 76.4 | 66.4 | 76.7 | 66.7 | 87.8 | 77.8 |
| 14887 | 119 | 109 | 1.2 | 1.18 | 4.3 | 0.02 | 100.0 | 97.8 | 129.4 | 231.1 | 105.3 | 95.3 | 105.9 | 95.9 | 112.2 | 102.2 |
| 14689 | 53 | 43 | 0.64 | 0.66 | 2.4 | 0 | 53.3 | 54.6 | 54.4 | 77.5 | 31.8 | 21.8 | 31.4 | 21.4 | 38.0 | 28.0 |
| 14695 | 114 | 104 | 1.35 | 1.3 | 4.8 | 0.05 | 112.5 | 109.2 | 99.4 | 161.6 | 109.6 | 99.6 | 109.9 | 99.9 | 113.8 | 103.8 |
| 14742 | 84 | 74 | 0.78 | 0.8 | 2.9 | 0 | 65.0 | 66.0 | 69.4 | 161.6 | 78.1 | 68.1 | 78.1 | 68.1 | 83.8 | 73.8 |
| 14666 | 94 | 84 | 0.77 | 0.74 | 2.7 | 0.03 | 64.2 | 61.4 | 98.1 | 188.7 | 84.0 | 74.0 | 84.3 | 74.3 | 89.0 | 79.0 |
| 14685 | 112 | 102 | 0.95 | 0.91 | 3.3 | 0.04 | 79.2 | 75.1 | 82.7 | 195.1 | 56.1 | 46.1 | 55.8 | 45.8 | 69.7 | 59.7 |
| 14685B | 102 | 92 | 0.85 | 0.84 | 3.1 | 0.01 | 70.8 | 70.5 | 73.7 | 190.6 | 41.1 | 31.1 | 41.5 | 31.5 | 56.1 | 46.1 |
| 14545 | 77 | 67 | 0.63 | 0.59 | 2.2 | 0.04 | 52.5 | 50.0 | 95.4 | 153.0 | 71.1 | 61.1 | 71.9 | 61.9 | 75.8 | 65.8 |
| 14565 | 136 | 126 | 1.33 | 1.28 | 4.7 | 0.05 | 110.8 | 106.9 | 114.4 | 164.2 | 128.8 | 118.8 | 128.5 | 118.5 | 135.8 | 125.8 |
| 14571 | 76 | 66 | 0.76 | 0.75 | 2.8 | 0.01 | 63.3 | 63.7 | 64.7 | 112.9 | 43.5 | 33.5 | 43.8 | 33.8 | 61.3 | 51.3 |
| 14578 | 111 | 101 | 1.25 | 1.26 | 4.6 | 0 | 104.2 | 104.6 | 104.9 | 153.5 | 54.1 | 44.1 | 54.1 | 44.1 | 63.6 | 53.6 |
| 14578B | 122 | 112 | 1.38 | 1.35 | 5 | 0.03 | 115.0 | 113.7 | 107.9 | 160.2 | 61.7 | 51.7 | 62.3 | 52.3 | 72.8 | 62.8 |
| 14598 | 77 | 67 | 0.59 | 0.57 | 2.1 | 0.02 | 49.2 | 47.8 | 83.7 | 174.6 | 72.9 | 62.9 | 72.9 | 62.9 | 75.3 | 65.3 |
| 14893 | 111 | 101 | 1.03 | 1.03 | 3.8 | 0 | 85.8 | 86.4 | 103.9 | 215.9 | 107.6 | 97.6 | 108.5 | 98.5 | 110.8 | 100.8 |
| 14899 | 81 | 71 | 0.68 | 0.65 | 2.4 | 0.03 | 56.7 | 54.6 | 88.4 | 258.4 | 80.4 | 70.4 | 80.4 | 70.4 | 80.8 | 70.8 |
| 14908 | 75 | 65 | 0.56 | 0.56 | 2.1 | 0 | 46.7 | 47.8 | 94.6 | 193.5 | 72.5 | 62.5 | 72.8 | 62.8 | 74.8 | 64.8 |
| 14917 | 66 | 56 | 0.55 | 0.54 | 2 | 0.01 | 45.8 | 45.5 | 57.9 | 133.3 | 60.1 | 50.1 | 60.8 | 50.8 | 65.8 | 55.8 |
| 14925 | 82 | 72 | 0.72 | 0.73 | 2.7 | 0 | 60.0 | 61.4 | 89.9 | 173.9 | 77.6 | 67.6 | 78.0 | 68.0 | 81.8 | 71.8 |
| 14998 | 103 | 93 | 1.05 | 1.04 | 3.8 | 0.01 | 87.5 | 86.4 | 99.4 | 166.5 | 98.9 | 88.9 | 99.3 | 89.3 | 102.8 | 92.8 |
| 15862 | 130 | 120 | 1.34 | 1.34 | 4.9 | 0 | 111.7 | 111.4 | 105.4 | 177.0 | 127.5 | 117.5 | 127.9 | 117.9 | 129.8 | 119.8 |
| 15870 | 151 | 141 | 1.72 | 1.72 | 6.3 | 0 | 143.3 | 143.3 | 115.9 | 188.7 | 146.9 | 136.9 | 147.9 | 137.9 | 150.8 | 140.8 |
| 15879 | 118 | 108 | 1.33 | 1.31 | 4.8 | 0.02 | 110.8 | 109.2 | 120.6 | 198.0 | 114.3 | 104.3 | 115.0 | 105.0 | 117.8 | 107.8 |
| 15887 | 95 | 85 | 0.94 | 0.91 | 3.3 | 0.03 | 78.3 | 75.1 | 102.9 | 168.4 | 85.3 | 75.3 | 85.8 | 75.8 | 94.8 | 84.8 |

Project:
Client
Data:
Comments:

Schaft Creek
Copper Fox Metals Inc.
ABA Data
Sampled by MDAG on Feb 7'07.

| Sample <br> Id. | NP | Available NP | Total C | Inorganic <br> C | Inorganic $\mathrm{CO}_{2}$ | $\begin{aligned} & \text { Excess } \\ & \quad \text { C } \end{aligned}$ | Total CaNP | Inorganic CaNP | (Ca) CaNP | $\begin{aligned} & (\mathrm{Ca}+\mathrm{Mg}) \\ & \text { CaNP } \end{aligned}$ | TNNP | Adjusted TNNP | SNNP | Adjusted SNNP | PNNP | Adjusted PNNP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | (\% Leco) | (\%) | (\%) | (\%) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | $\left(\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}\right)$ | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | (kg CaCO33 ${ }^{\text {t }}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3} / \mathrm{t}$ ) | ( $\mathrm{kg} \mathrm{CaCO}_{3}$ /t) | (kg CaCO3 ${ }_{3}$ t) |
| Method | OA-VOL08 | Calculated | C-IR07 | C-GAS05 | C-GAS05 | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated |
| MDL | 1 |  | 0.01 | 0.05 | 0.2 |  |  |  |  |  |  |  |  |  |  |  |
| 15891 | 128 | 118 | 1.44 | 1.4 | 5.1 | 0.04 | 120.0 | 116.0 | 128.1 | 199.3 | 123.6 | 113.6 | 124.8 | 114.8 | 127.8 | 117.8 |
| 15908 | 121 | 111 | 1.2 | 1.2 | 4.4 | 0 | 100.0 | 100.1 | 112.9 | 189.0 | 114.1 | 104.1 | 114.5 | 104.5 | 120.8 | 110.8 |
| 15911 | 92 | 82 | 0.85 | 0.82 | 3 | 0.03 | 70.8 | 68.2 | 87.9 | 183.0 | 89.2 | 79.2 | 89.7 | 79.7 | 91.8 | 81.8 |
| Maximum | 219 | 209 | 2.3 | 2.28 | 8.4 | 1.32 | 192 | 191 | 140 | 258 | 215 | 205 | 215 | 205 | 219 | 209 |
| Minimum | 40 | 30 | 0.29 | 0.21 | 0.8 | 0 | 24.2 | 18.2 | 35 | 74.4 | 0.062 | -9.94 | 3.61 | -6.39 | 11.2 | 1.16 |
| Mean | 96.5 | 86.5 | 1 | 0.94 | 3.46 | 0.055 | 83.2 | 78.8 | 88.3 | 159 | 82.4 | 72.4 | 83.3 | 73.3 | 89.8 | 79.8 |
| Standard Deviation | 35.2 | 35.2 | 0.44 | 0.46 | 1.67 | 0.17 | 36.9 | 38.1 | 23.1 | 42.2 | 41.1 | 41.1 | 40.4 | 40.4 | 39.3 | 39.3 |
| 10 Percentile | 52.2 | 42.2 | 0.52 | 0.43 | 1.56 | 0 | 43.2 | 35.5 | 57.9 | 103 | 35.6 | 25.6 | 35.4 | 25.4 | 43 | 33 |
| 25 Percentile | 74.5 | 64.5 | 0.7 | 0.66 | 2.4 | 0.01 | 58.8 | 54.6 | 69.9 | 130 | 55.3 | 45.3 | 55.3 | 45.3 | 64.8 | 54.8 |
| Median | 92 | 82 | 0.9 | 0.86 | 3.2 | 0.02 | 75 | 72.8 | 91.4 | 164 | 78.1 | 68.1 | 78.1 | 68.1 | 84.8 | 74.8 |
| 75 Percentile | 118 | 108 | 1.29 | 1.23 | 4.5 | 0.04 | 108 | 102 | 104 | 189 | 109 | 98.8 | 109 | 99.2 | 115 | 105 |
| 90 Percentile | 136 | 126 | 1.57 | 1.43 | 5.22 | 0.068 | 131 | 119 | 116 | 202 | 128 | 118 | 128 | 118 | 134 | 124 |
| Interquartile Range (IQR) ${ }^{1}$ | 43.5 | 43.5 | 0.59 | 0.57 | 2.1 | 0.03 | 48.8 | 47.8 | 34.5 | 58.4 | 53.4 | 53.4 | 53.9 | 53.9 | 50 | 50 |
| Variance | 1237 | 1237 | 0.2 | 0.21 | 2.8 | 0.03 | 1363 | 1450 | 535 | 1781 | 1686 | 1686 | 1630 | 1630 | 1544 | 1544 |
| Skewness | 0.84 | 0.84 | 0.9 | 0.85 | 0.86 | 6.9 | 0.9 | 0.86 | -0.14 | -0.079 | 0.57 | 0.57 | 0.66 | 0.66 | 0.64 | 0.64 |
| Coefficient of Variation (CoV) ${ }^{2}$ | 0.36 | 0.41 | 0.44 | 0.48 | 0.48 | 3.16 | 0.44 | 0.48 | 0.26 | 0.27 | 0.5 | 0.57 | 0.48 | 0.55 | 0.44 | 0.49 |
| Count | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 |

Total 10 or NPR $=1.0$
$1.0<$ NPR < 2.0
NPR > 2.0 or NPR $=2.0$
$\%$ NPR $<1.0$ or NPR $=1.0$ of Tota
$\% 1.0<$ NPR < 2.0 of Total
\% NPR > 2.0 or NPR =2.0 of Total

[^0]Project:
Data:
Comments:

Schaft Creek
Copper Fox Metals Inc.
ABA Data
Sampled by MDAG on Feb 7'07.

| SampleId. | Adjusted |  |  | Adjusted |  | Adjusted |  | Comparison of Fizz Rating \& NP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | TNPR | TNPR | SNPR | SNPR | PNPR | PNPR | Rating |  |
|  |  |  |  |  |  |  | Unity |  |
| Method | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | OA-VoL08 |  |
| MDL |  |  |  |  |  |  |  |  |
| 14018 | 1.68 | 1.28 | 1.75 | 1.33 | 2.13 | 1.62 | 2 | Disagree |
| 14021 | 3.3 | 2.79 | 3.39 | 2.86 | 5.12 | 4.32 | 2 | Agree |
| 14036 | 1.07 | 0.849 | 1.08 | 0.859 | 1.29 | 1.03 | 2 | Disagree |
| 14043 | 4.92 | 3.69 | 5.15 | 3.86 | 14.2 | 10.7 | 2 | Disagree |
| 14060 | 1 | 0.757 | 2.12 | 1.6 | 3.86 | 2.92 | 2 | Disagree |
| 14067 | 3.92 | 3.12 | 3.82 | 3.04 | 10.4 | 8.29 | 2 | Disagree |
| 14076 | 2.74 | 2.33 | 2.78 | 2.36 | 3.45 | 2.93 | 2 | Agree |
| 14083 | 1.62 | 1.4 | 1.65 | 1.42 | 1.83 | 1.58 | 2 | Agree |
| 14099 | 7.34 | 6.4 | 7.95 | 6.93 | 13.8 | 12 | 2 | Agree |
| 14103 | 3.94 | 3.48 | 10.3 | 9.1 | 200 | 200 |  | Disagree |
| 14130 | 10 | 8.94 | 10 | 8.94 | 200 | 200 | 3 | Disagree |
| 14144 | 14.3 | 13 | 15.1 | 13.8 | 200 | 200 | 3 | Agree |
| 14148 | 38.9 | 36.6 | 45.2 | 42.5 | 200 | 200 | 3 | Agree |
| 14156 | 13.7 | 11.9 | 14.7 | 12.7 | 200 | 200 | 3 | Disagree |
| 14162 | 53.9 | 51.4 | 58.4 | 55.7 | 200 | 200 | 3 | Agree |
| 14169 | 6.83 | 5.76 | 6.99 | 5.9 | 200 | 200 | 3 | Disagree |
| 14232 | 19 | 16.9 | 20.2 | 18 | 200 | 200 | 3 | Disagree |
| 14250 | 19.9 | 18.2 | 19.9 | 18.2 | 200 | 200 | 3 | Agree |
| 14260 | 9.41 | 8.47 | 9.41 | 8.47 | 200 | 200 | 3 | Agree |
| 14276 | 8.85 | 6.96 | 10.7 | 8.46 | 200 | 200 | 2 | Disagree |
| 14295 | 8.07 | 7.35 | 8.2 | 7.47 | 18.2 | 16.6 | 3 | Agree |
| 14301 | 12.8 | 11.9 | 13.2 | 12.3 | 66.1 | 61.3 | 3 | Agree |
| 14323 | 15.6 | 13.4 | 16.8 | 14.5 | 200 | 200 | 2 | Agree |
| 14332 | 11.7 | 10.5 | 11.7 | 10.5 | 200 | 200 | 3 | Disagree |
| 14345 | 4.86 | 4.25 | 4.86 | 4.25 | 200 | 200 | 3 | Disagree |
| 14348 | 4.29 | 3.56 | 4.2 | 3.48 | 200 | 200 | 2 | Agree |
| 14797 | 50 | 46 | 56.5 | 52 | 200 | 200 | 3 | Agree |
| 14808 | 30.6 | 28.8 | 32.2 | 30.3 | 200 | 200 | 3 | Agree |
| 14816 | 9.25 | 8.56 | 9.25 | 8.56 | 80.4 | 74.4 | 3 | Agree |
| 14828 | 35.2 | 32.7 | 42.3 | 39.3 | 200 | 200 |  | Agree |
| 14844 | 11.4 | 9.9 | 12 | 10.4 | 200 | 200 | 3 | Disagree |
| 14680 | 14.8 | 13.4 | 15.6 | 14.1 | 200 | 200 | 3 | Agree |
| 14871 | 7.61 | 6.75 | 7.76 | 6.88 | 200 | 200 |  | Disagree |
| 14887 | 8.65 | 7.93 | 9.07 | 8.3 | 17.6 | 16.1 | 3 | Agree |
| 14689 | 2.49 | 2.02 | 2.46 | 1.99 | 3.54 | 2.87 | 2 | Agree |
| 14695 | 26.1 | 23.8 | 27.9 | 25.4 | 200 | 200 | 3 | Agree |
| 14742 | 14.1 | 12.5 | 14.1 | 12.5 | 200 | 200 | 3 | Disagree |
| 14666 | 9.4 | 8.4 | 9.7 | 8.67 | 18.7 | 16.7 | 3 | Disagree |
| 14685 | 2 | 1.82 | 1.99 | 1.81 | 2.65 | 2.41 | 3 | Agree |
| 14685B | 1.67 | 1.51 | 1.69 | 1.52 | 2.22 | 2.01 | 3 | Agree |
| 14545 | 13 | 11.3 | 15 | 13.1 | 62.5 | 54.3 | 3 | Disagree |
| 14565 | 18.9 | 17.5 | 18.1 | 16.8 | 200 | 200 | 3 | Agree |
| 14571 | 2.34 | 2.03 | 2.36 | 2.05 | 5.16 | 4.49 | 3 | Disagree |
| 14578 | 1.95 | 1.78 | 1.95 | 1.78 | 2.34 | 2.13 | 3 | Agree |
| 14578B | 2.02 | 1.86 | 2.04 | 1.88 | 2.48 | 2.27 | 3 | Agree |
| 14598 | 19 | 16.5 | 19 | 16.5 | 46.5 | 40.5 | 3 | Disagree |
| 14893 | 32.3 | 29.4 | 44.4 | 40.4 | 200 | 200 | 3 | Agree |
| 14899 | 130 | 114 | 130 | 114 | 200 | 200 | 3 | Disagree |
| 14908 | 30 | 26 | 34.3 | 29.7 | 200 | 200 | 3 | Disagree |
| 14917 | 11.1 | 9.43 | 12.7 | 10.8 | 200 | 200 |  | Disagree |
| 14925 | 18.7 | 16.5 | 20.7 | 18.2 | 200 | 200 | 3 | Disagree |
| 14998 | 25.4 | 22.9 | 27.5 | 24.8 | 200 | 200 |  | Agree |
| 15862 | 52 | 48 | 60.5 | 55.9 | 200 | 200 | 3 | Agree |
| 15870 | 37.2 | 34.7 | 48.4 | 45.2 | 200 | 200 | 3 | Agree |
| 15879 | 31.5 | 28.8 | 39.3 | 35.9 | 200 | 200 |  | Agree |
| 15887 | 9.81 | 8.77 | 10.3 | 9.23 | 200 | 200 | 3 | Disagree |

Project:
Client:
Comments:

Schaft Creek
Copper Fox Metals Inc.
ABA Data
Sampled by MDAG on Feb 7'07.
$\left.\begin{array}{cccccccc} & & & & & & & \begin{array}{c}\text { Comparison } \\ \text { of Fizz }\end{array} \\ \text { TNPR } & \begin{array}{c}\text { Adjusted } \\ \text { TNPR }\end{array} & \text { SNPR } & \begin{array}{c}\text { Adjusted } \\ \text { SNPR }\end{array} & \text { PNPR } & \begin{array}{c}\text { Adjusted } \\ \text { PNPR }\end{array} & \begin{array}{c}\text { Fizz } \\ \text { Rating } \\ \text { Unity }\end{array} & \begin{array}{c}\text { \& NP }\end{array} \\ \text { Calculated } & \text { Calculated } & \text { Calculated } & \text { Calculated } & \text { Calculated } & \text { Calculated } & \text { OA-voLo8 }\end{array}\right]$
$\begin{array}{llllll}1.694915 & 3.389831 & 0 & 1.694915 & 0 & 0\end{array}$ $\begin{array}{llllllll}8.474576 & 10.16949 & 10.16949 & 13.55932 & 3.389831 & 5.084746\end{array}$ $89.8305186 .44068 \quad 89.8305184 .74576$ 96.61017 94.91525
${ }^{1}$ Interquartile Range $(\mathrm{IQR})=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) = standard deviation divided by mean
NOTE: If data was reported as < detection limit half the detection limit is shown in italics and $w$
TNPR = NP / TAP
Note: If \% S(Total) $<0.01$ then TNPR $=200$
Note: If $\% \mathrm{~S}$ (Total) $>0.01$ and $\mathrm{NP}<=0$ then TNPR $=0.001$
Adjusted TNPR = UNP / TAP
Note: If $\%$ S(Total) $<0.01$ then Adjusted TNPR $=200$
Note: If $\%$ S(Total) $>0.01$ and UNP $<=0$ then Adjusted TNPR $=0.001$
SNPR $=$ NP $/$ SAP
Note: If \% S(Sulphide + del) $<0.01$ then SNPR $=200$
'Note: If $\%$ S(Sulphide + del) $>0.01$ and NP $<=0$ then SNPR $=0.001$
Adjusted SNPR = UNP / SAP
Note: If $\%$ S(Sulphide + del) $<0.01$ then Adjusted SNPR $=200$

PNPR = NP / PAP
Note: If \% Pyrite(Calc) $<0.01$ then PNPR $=200$
Note: If \% Pyrite(Calc) $>0.01$ and NP $<=0$ then PNPR $=0.001$
Adjusted PNPR = UNP / TAP
Note: If \% Pyrite(Calc) < 0.005 then Adjusted PNPR $=200$
Note: If $\%$ Pyrite(Calc) $>0.005$ and UNP $<=0$ then Adjusted PNPR $=0.001$

Project:
Client:
Data:
Comments:

Schaft Creek
Copper Fox Metals Inc.
ICP Metals Data
Sampled by MDAG on Feb 7'07.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

| Sample <br> Id. | Silver Ag (ppm) | Aluminum <br> AI <br> (ppm) | Arsenic As (ppm) | Barium <br> Ba <br> (ppm) | Beryllium Be (ppm) | Bismuth <br> Bi <br> (ppm) | Calcium Ca (ppm) | Cadmium <br> Cd <br> (ppm) | Cerium <br> Ce <br> (ppm) | Cobalt <br> Co <br> (ppm) | Chromium <br> Cr <br> (ppm) | $\begin{aligned} & \text { Cesium } \\ & \text { Cs } \\ & \text { (ppm) } \end{aligned}$ | Copper Cu (ppm) | Iron <br> Fe <br> (ppm) | Gallium Ga (ppm) | Germanium Ge (ppm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Method | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 |
| MDL | 0.01 | 100 | 0.2 | 10 | 0.05 | 0.01 | 100 | 0.02 | 0.01 | 0.1 | 1 | 0.05 | 0.2 | 100 | 0.05 | 0.05 |
| Crustal Abundance: From | 0.037 | 4200 | 1 | 0.4 | 1 | 0.007 | 5100 | 0.035 | 11.5 | 0.1 | 2 | 0.4 | 4 | 3800 | 4 | 0.2 |
| Crustal Abundance: To | 0.11 | 88000 | 13 | 2300 | 3 | 0.01 | 312400 | 0.42 | 345 | 74 | 170 | 6 | 250 | 86500 | 30 | 8 |
| 14018 | 0.88 | 80300 | 15.5 | 1120 | 1.3 | 0.93 | 17800 | 0.02 | 26.5 | 12 | 24 | 5.11 | 1290 | 25800 | 17.8 | 0.09 |
| 14021 | 1.22 | 77000 | 24.5 | 460 | 1.03 | 0.86 | 26200 | 0.11 | 23.2 | 9.7 | 21 | 5.86 | 1740 | 18100 | 16.4 | 0.08 |
| 14036 | 1.43 | 74100 | 30.2 | 500 | 1 | 1.01 | 18400 | 0.01 | 23.8 | 16.6 | 20 | 8.17 | 1920 | 25600 | 16.2 | 0.18 |
| 14043 | 0.7 | 75600 | 10.9 | 230 | 1.03 | 0.4 | 14000 | 0.01 | 13.3 | 14.6 | 31 | 2.39 | 1330 | 28500 | 16.05 | 0.06 |
| 14060 | 0.87 | 79600 | 14.3 | 380 | 0.99 | 0.24 | 31400 | 0.01 | 23.7 | 15.4 | 26 | 4.87 | 2610 | 35900 | 16.25 | 0.09 |
| 14067 | 1.85 | 85100 | 17.3 | 370 | 0.95 | 0.18 | 25900 | 0.03 | 21.5 | 19.9 | 36 | 2.64 | 2460 | 42900 | 17.6 | 0.1 |
| 14076 | 1.32 | 90000 | 15.1 | 410 | 0.8 | 0.62 | 43400 | 0.61 | 22.6 | 23.3 | 33 | 5.75 | 1300 | 54600 | 18.05 | 0.12 |
| 14083 | 0.98 | 88500 | 13.9 | 700 | 0.78 | 0.86 | 40300 | 0.5 | 22.8 | 24 | 49 | 7.97 | 1360 | 57800 | 17.8 | 0.12 |
| 14099 | 1.36 | 72400 | 2.2 | 770 | 0.95 | 1.51 | 29500 | 1.16 | 21.3 | 6.4 | 16 | 9.67 | 1210 | 22300 | 15.1 | 0.07 |
| 14103 | 1.06 | 76000 | 5.6 | 250 | 1.06 | 1.02 | 29300 | 0.03 | 25.9 | 7.8 | 20 | 3.59 | 2630 | 21200 | 16.95 | 0.09 |
| 14130 | 3.33 | 85100 | 2.1 | 440 | 0.62 | 2 | 26200 | 0.01 | 15.5 | 5 | 15 | 3.56 | 5530 | 18000 | 18.25 | 0.08 |
| 14144 | 2.52 | 93900 | 5.1 | 380 | 0.84 | 2.32 | 37500 | 0.01 | 20.7 | 7.7 | 5 | 5.29 | 3410 | 36100 | 20 | 0.1 |
| 14148 | 1.75 | 81100 | 2.6 | 560 | 0.9 | 1.98 | 46300 | 0.01 | 22.7 | 11 | 4 | 4.68 | 2880 | 38300 | 18.75 | 0.1 |
| 14156 | 1.76 | 76900 | 1.1 | 280 | 1.56 | 1.47 | 24700 | 0.01 | 23.3 | 5.4 | 25 | 2.49 | 2090 | 17400 | 20.5 | 0.07 |
| 14162 | 0.53 | 79700 | 2.1 | 510 | 0.92 | 2.13 | 55900 | 0.01 | 25.2 | 20.8 | 71 | 2.12 | 1020 | 42500 | 14.85 | 0.1 |
| 14169 | 2.84 | 76400 | 1.9 | 100 | 1.09 | 6.51 | 23200 | 0.01 | 7.62 | 4.2 | 16 | 1.19 | 3820 | 11800 | 18.85 | 0.05 |
| 14232 | 1.73 | 94400 | 3.5 | 140 | 0.95 | 0.84 | 26600 | 0.01 | 22.2 | 4.7 | 14 | 6.81 | 3370 | 26400 | 19.75 | 0.08 |
| 14250 | 1.66 | 94400 | 3.4 | 170 | 0.75 | 1.14 | 40700 | 0.01 | 24.1 | 8.3 | 12 | 4.65 | 3170 | 45800 | 21 | 0.11 |
| 14260 | 2.92 | 89500 | 2.6 | 170 | 0.73 | 6.57 | 30400 | 0.01 | 21.6 | 7.8 | 3 | 4.9 | 4880 | 42300 | 20 | 0.1 |
| 14276 | 0.8 | 98400 | 7.5 | 1000 | 0.78 | 0.78 | 43100 | 0.13 | 21.2 | 8.8 | 17 | 2.68 | 1490 | 38900 | 20.3 | 0.08 |
| 14295 | 0.51 | 89700 | 3.7 | 110 | 0.7 | 0.2 | 39100 | 0.02 | 18.6 | 18.6 | 12 | 4.81 | 2330 | 47300 | 18.95 | 0.1 |
| 14301 | 0.39 | 87600 | 3.8 | 300 | 0.86 | 0.4 | 36600 | 0.01 | 20.1 | 10.4 | 15 | 3.85 | 2440 | 31300 | 18.05 | 0.09 |
| 14323 | 1.33 | 93600 | 3.3 | 280 | 0.92 | 0.74 | 37500 | 0.01 | 20.5 | 8.8 | 3 | 6.79 | 2250 | 38700 | 20.5 | 0.09 |
| 14332 | 1.36 | 96200 | 2.2 | 210 | 0.88 | 0.62 | 33900 | 0.01 | 23.9 | 7.7 | 3 | 5.41 | 3470 | 35500 | 20.8 | 0.09 |
| 14345 | 2.38 | 97300 | 2.1 | 190 | 0.9 | 2.05 | 25500 | 0.01 | 26.4 | 7.2 | 11 | 4.35 | 6070 | 22100 | 20.4 | 0.09 |
| 14348 | 1 | 94300 | 2.3 | 150 | 0.82 | 1.13 | 21500 | 0.01 | 24.6 | 8.4 | 11 | 4.61 | 4900 | 34700 | 20.1 | 0.09 |
| 14797 | 1.03 | 86900 | 2.5 | 150 | 0.92 | 0.43 | 37800 | 0.01 | 15.4 | 10.5 | 6 | 6.37 | 1750 | 42700 | 19.85 | 0.11 |
| 14808 | 2.27 | 81300 | 0.1 | 170 | 1.58 | 1.73 | 48700 | 0.01 | 21.5 | 9.2 | 6 | 5.38 | 2640 | 37600 | 18.75 | 0.33 |
| 14816 | 2.15 | 82900 | 1.8 | 140 | 0.84 | 2.94 | 33300 | 0.01 | 18.3 | 10.1 | 5 | 5.98 | 3970 | 41300 | 21.4 | 0.12 |
| 14828 | 2.42 | 89200 | 2.4 | 710 | 0.94 | 2.48 | 43400 | 0.01 | 23.8 | 10.3 | 4 | 5.11 | 3260 | 41200 | 20.9 | 0.13 |
| 14844 | 1.35 | 91800 | 3.7 | 300 | 0.67 | 1.02 | 28200 | 0.01 | 15.75 | 19 | 39 | 8.05 | 2990 | 51800 | 22 | 0.12 |
| 14680 | 3.36 | 90500 | 1.8 | 300 | 2.27 | 5.64 | 41400 | 0.01 | 27.1 | 11 | 5 | 10.45 | 3950 | 41400 | 21 | 0.28 |
| 14871 | 1.02 | 96200 | 2.3 | 120 | 0.74 | 1.28 | 34000 | 0.01 | 18.75 | 12.7 | 10 | 5.3 | 3880 | 46100 | 21.4 | 0.11 |
| 14887 | 0.41 | 96900 | 2.9 | 340 | 0.68 | 0.28 | 51800 | 0.01 | 22.1 | 16.2 | 20 | 3.33 | 1990 | 53100 | 20.4 | 0.12 |
| 14689 | 0.38 | 83800 | 1.4 | 120 | 1.01 | 0.44 | 21800 | 0.01 | 29.6 | 5.9 | 10 | 2.38 | 2020 | 14800 | 18.4 | 0.07 |
| 14695 | 0.71 | 97000 | 0.1 | 170 | 0.89 | 1.19 | 39800 | 0.01 | 26.4 | 9.6 | 6 | 7.95 | 1500 | 39900 | 21.4 | 0.24 |
| 14742 | 1.3 | 90600 | 0.5 | 120 | 1.35 | 4.71 | 27800 | 0.01 | 17.2 | 10.4 | 24 | 2.84 | 2100 | 33500 | 20.5 | 0.33 |
| 14666 | 0.37 | 92100 | 4.8 | 330 | 0.78 | 0.13 | 39300 | 0.01 | 19.3 | 21.9 | 21 | 4.19 | 1440 | 53900 | 21.9 | 0.1 |
| 14685 | 1.13 | 85900 | 6.6 | 380 | 1.04 | 0.51 | 33100 | 0.01 | 22.1 | 35.4 | 5 | 5.87 | 4330 | 63900 | 22.7 | 0.1 |
| 14685B | 1 | 83100 | 5.9 | 310 | 1.1 | 0.48 | 29500 | 0.01 | 19.45 | 30.6 | 7 | 5.85 | 4570 | 59700 | 21.8 | 0.11 |
| 14545 | 0.26 | 94700 | 3.4 | 860 | 0.8 | 0.08 | 38200 | 0.01 | 24.1 | 10.3 | 16 | 4.7 | 1210 | 41700 | 21.2 | 0.1 |
| 14565 | 0.47 | 88300 | 3 | 220 | 0.7 | 0.39 | 45800 | 0.01 | 22.7 | 8.7 | 11 | 5.46 | 2670 | 37200 | 18.65 | 0.09 |
| 14571 | 1.92 | 82200 | 3.2 | 430 | 0.99 | 1.04 | 25900 | 0.01 | 20.9 | 12.9 | 7 | 5.37 | 5450 | 26900 | 18.05 | 0.08 |
| 14578 | 0.65 | 86800 | 5.2 | 640 | 1.16 | 0.33 | 42000 | 0.01 | 23.9 | 15.8 | 9 | 6.35 | 2980 | 41600 | 19.4 | 0.1 |
| 14578B | 0.74 | 82400 | 4.5 | 760 | 1 | 0.31 | 43200 | 0.01 | 22.8 | 15.7 | 10 | 6.22 | 3280 | 39200 | 20.4 | 0.11 |
| 14598 | 0.39 | 92500 | 2.7 | 220 | 0.85 | 1.23 | 33500 | 0.01 | 16.15 | 15.9 | 3 | 4.8 | 703 | 46600 | 22.6 | 0.09 |
| 14893 | 0.67 | 92000 | 4.5 | 490 | 0.81 | 0.56 | 41600 | 0.01 | 18.75 | 18.3 | 44 | 5.23 | 1630 | 53400 | 22.6 | 0.11 |
| 14899 | 0.25 | 97000 | 8.1 | 330 | 0.78 | 0.18 | 35400 | 0.01 | 15.8 | 22.6 | 43 | 2.68 | 409 | 56900 | 24.2 | 0.12 |
| 14908 | 0.39 | 95800 | 6.2 | 690 | 0.69 | 0.29 | 37900 | 0.01 | 19.6 | 15 | 39 | 2.29 | 1140 | 53200 | 23.3 | 0.11 |
| 14917 | 2.53 | 85300 | 1.7 | 740 | 1.19 | 1.43 | 23200 | 0.01 | 25.1 | 9.4 | 16 | 2.27 | 3800 | 24200 | 23.5 | 0.1 |
| 14925 | 0.71 | 87800 | 3.5 | 390 | 0.71 | 0.58 | 36000 | 0.01 | 17.85 | 13.9 | 30 | 4.58 | 1610 | 46200 | 22.7 | 0.12 |
| 14998 | 0.72 | 90100 | 3.4 | 280 | 0.63 | 0.53 | 39800 | 0.01 | 20.1 | 12.8 | 6 | 5.88 | 1800 | 43600 | 21.6 | 0.12 |
| 15862 | 0.74 | 87200 | 2.2 | 290 | 0.66 | 0.49 | 42200 | 0.01 | 19.1 | 12.2 | 4 | 5.75 | 1180 | 41600 | 21 | 0.1 |
| 15870 | 1.17 | 81000 | 2.6 | 1030 | 0.46 | 0.54 | 46400 | 0.01 | 20.6 | 10.3 | 27 | 4.53 | 2020 | 39200 | 20.4 | 0.12 |

Project:
Data:
Comments:

| Sample | Silver | Aluminum | Arsenic | Barium | Beryllium | Bismuth | Calcium | Cadmium | Cerium | Cobalt | Chromium | Cesium | Copper | Iron | Gallium | Germanium |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 l . | Ag | Al | As | Ba | Be | Bi | Ca | Cd | Ce | Co | Cr | Cs | Cu | Fe | Ga | Ge |
|  | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) |
| Method | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 |
| MDL | 0.01 | 100 | 0.2 | 10 | 0.05 | 0.01 | 100 | 0.02 | 0.01 | 0.1 | 1 | 0.05 | 0.2 | 100 | 0.05 | 0.05 |
| Crustal Abundance: From | 0.037 | 4200 | 1 | 0.4 | 1 | 0.007 | 5100 | 0.035 | 11.5 | 0.1 | 2 | 0.4 | 4 | 3800 | 4 | 0.2 |
| Crustal Abundance: To | 0.11 | 88000 | 13 | 2300 | 3 | 0.01 | 312400 | 0.42 | 345 | 74 | 170 | 6 | 250 | 86500 | 30 | 8 |
| 15879 | 1.4 | 90600 | 2.4 | 760 | 0.67 | 0.51 | 48300 | 0.01 | 19.85 | 13.6 | 29 | 4.83 | 2150 | 51500 | 21.7 | 0.12 |
| 15887 | 2.42 | 87200 | 2 | 440 | 0.75 | 1.14 | 41200 | 0.01 | 15.05 | 14 | 25 | 5.1 | 5070 | 34600 | 21.4 | 0.12 |
| 15891 | 2.15 | 89500 | 1.7 | 1250 | 0.66 | 0.98 | 51300 | 0.01 | 17.35 | 9.7 | 22 | 5.24 | 2450 | 38500 | 21.4 | 0.11 |
| 15908 | 2.82 | 87100 | 1.5 | 260 | 0.77 | 1.3 | 45200 | 0.01 | 17.95 | 12.7 | 24 | 5.96 | 4260 | 34500 | 20.8 | 0.1 |
| 15911 | 1.2 | 88600 | 2.1 | 410 | 0.7 | 0.56 | 35200 | 0.01 | 19.5 | 14.8 | 33 | 6.92 | 1820 | 46500 | 22.2 | 0.1 |
| Maximum | 3.36 | 98400 | 30.2 | 1250 | 2.27 | 6.57 | 55900 | 1.16 | 29.6 | 35.4 | 71 | 10.4 | 6070 | 63900 | 24.2 | 0.33 |
| Minimum | 0.25 | 72400 | 0.1 | 100 | 0.46 | 0.08 | 14000 | 0.01 | 7.62 | 4.2 | 3 | 1.19 | 409 | 11800 | 14.8 | 0.05 |
| Mean | 1.34 | 87481 | 5.08 | 412 | 0.91 | 1.26 | 35375 | 0.053 | 21 | 13 | 18.3 | 5.04 | 2661 | 38607 | 20 | 0.11 |
| Standard Deviation | 0.82 | 6660 | 5.75 | 273 | 0.28 | 1.42 | 9259 | 0.18 | 3.85 | 6.16 | 13.8 | 1.85 | 1333 | 11942 | 2.14 | 0.054 |
| 10 Percentile | 0.39 | 76980 | 1.66 | 140 | 0.67 | 0.27 | 23200 | 0.01 | 15.8 | 7.04 | 4 | 2.47 | 1210 | 21920 | 16.8 | 0.08 |
| 25 Percentile | 0.71 | 82650 | 2.1 | 215 | 0.74 | 0.46 | 28000 | 0.01 | 18.8 | 8.8 | 6.5 | 4.02 | 1620 | 32400 | 18.5 | 0.09 |
| Median | 1.17 | 88300 | 3 | 330 | 0.86 | 0.86 | 36600 | 0.01 | 21.3 | 11 | 16 | 5.11 | 2440 | 39200 | 20.4 | 0.1 |
| 75 Percentile | 1.81 | 92300 | 5.15 | 505 | 1 | 1.36 | 41800 | 0.01 | 23.8 | 15.8 | 25 | 5.88 | 3440 | 46150 | 21.4 | 0.12 |
| 90 Percentile | 2.52 | 96200 | 14 | 762 | 1.17 | 2.35 | 46320 | 0.03 | 25.3 | 21 | 36.6 | 7.13 | 4632 | 53500 | 22.6 | 0.12 |
| Interquartile Range (IQR) ${ }^{1}$ | 1.1 | 9650 | 3.05 | 290 | 0.26 | 0.9 | 13800 | 0 | 5 | 6.95 | 18.5 | 1.85 | 1820 | 13750 | 2.88 | 0.03 |
| Variance | 0.68 | 44356026 | 33 | 74305 | 0.078 | 2.01 | 85737446 | 0.032 | 14.8 | 38 | 191 | 3.44 | 1775728 | 142622022 | 4.57 | 0.0029 |
| Skewness | 0.77 | -0.38 | 2.61 | 1.23 | 2.42 | 2.57 | -0.14 | 5.11 | -0.65 | 1.37 | 1.33 | 0.42 | 0.68 | -0.24 | -0.49 | 2.96 |
| Coefficient of Variation (CoV) ${ }^{2}$ | 0.61 | 0.076 | 1.13 | 0.66 | 0.31 | 1.13 | 0.26 | 3.38 | 0.18 | 0.47 | 0.76 | 0.37 | 0.5 | 0.31 | 0.11 | 0.47 |
| Count | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 |

$\square$ NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.
${ }^{1}$ Interquartile Range $(\mathrm{IQR})=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) = standard deviation divided by mean
NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.
NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project:
Client:
Comments:

| Sample |
| :--- |
| Id. |
| Method |
| MDL |
| Crustal Abundance: From |
| Crustal Abundance: To |
| 14018 |
| 14021 |
| 14036 |
| 14043 |
| 14060 |
| 14067 |
| 14076 |
| 14083 |
| 14099 |
| 14103 |
| 14130 |
| 14144 |
| 14148 |
| 14156 |
| 14162 |
| 14169 |
| 14232 |
| 14250 |
| 14260 |
| 14276 |
| 14295 |
| 14301 |
| 14323 |
| 14332 |
| 14345 |
| 14348 |
| 14797 |
| 14808 |
| 14816 |
| 14828 |
| 14844 |
| 14680 |
| 14871 |
| 14887 |
| 14689 |
| 14695 |
| 14742 |
| 14666 |
| 14685 |
| $14685 B$ |
| 14545 |
| 14565 |
| 14571 |
| 14578 |
| $14578 B$ |
| 14598 |
| 14893 |
| 14899 |
| 14908 |
| 14917 |
| 14925 |
| 14998 |
| 15862 |
| 15870 |

Schaft Creek
Copper Fox Metals Inc.
ICP Metals Data
Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

| Hafnium Hf | Mercury <br> Hg | Indium In | $\begin{gathered} \text { Potassium } \\ K \end{gathered}$ | Lanthanum <br> La | Lithium Li | Magnesium <br> Mg | Manganese <br> Mn | Molybdenum Mo | Sodium Na | Niobium Nb | Nickel Ni | Phosphorus P | Lead Pb | Rubidium Rb | $\begin{aligned} & \text { Rhenium } \\ & \mathrm{Re} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) |
| ME-MS61 | Hg-CV41 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 |
| 0.1 | 0.01 | 0.005 | 100 | 0.5 | 0.2 | 100 | 5 | 0.05 | 100 | 0.1 | 0.2 | 10 | 0.5 | 0.1 | 0.002 |
| 0.3 | 0.03 | 0.01 | 40 | 10 | 5 | 1600 | 390 | 0.2 | 400 | 0.3 | 2 | 170 | 1 | 0.2 | NA |
| 11 | 0.4 | 0.26 | 48000 | 115 | 66 | 47000 | 6700 | 27 | 40400 | 35 | 225 | 1500 | 80 | 170 | NA |
| 1.9 | 0.01 | 0.065 | 24500 | 12.7 | 8.7 | 10700 | 476 | 36.3 | 31600 | 4.2 | 9.6 | 660 | 52 | 89.4 | 0.036 |
| 1.7 | 0.005 | 0.082 | 22200 | 11.9 | 9.6 | 9200 | 629 | 348 | 23800 | 3.4 | 6.9 | 570 | 91.3 | 129.5 | 0.178 |
| 1.7 | 0.005 | 0.087 | 21300 | 11.9 | 9.5 | 9100 | 475 | 658 | 24700 | 3 | 8.3 | 570 | 19.7 | 119.5 | 0.312 |
| 1.4 | 0.005 | 0.041 | 10300 | 6.8 | 17.7 | 19000 | 446 | 324 | 32900 | 2.6 | 11.6 | 570 | 4.7 | 61.3 | 0.146 |
| 2.2 | 0.005 | 0.053 | 12000 | 11.2 | 19.5 | 21000 | 422 | 220 | 30500 | 3.3 | 15.3 | 1290 | 5.8 | 67.9 | 0.133 |
| 1.6 | 0.005 | 0.046 | 11200 | 10.1 | 26 | 26800 | 779 | 90.6 | 35100 | 2.7 | 16.2 | 1120 | 40.8 | 53.8 | 0.116 |
| 1.9 | 0.01 | 0.06 | 14300 | 10.7 | 22.4 | 25000 | 1585 | 56.2 | 23000 | 2.6 | 15 | 1070 | 236 | 75.1 | 0.136 |
| 1.4 | 0.01 | 0.076 | 30900 | 10.6 | 19.2 | 17700 | 1365 | 13.2 | 13600 | 2.5 | 17.2 | 1070 | 20 | 165 | 0.033 |
| 1.4 | 0.02 | 0.04 | 32000 | 9.9 | 5.3 | 8200 | 1090 | 6.9 | 5400 | 3.2 | 6.5 | 470 | 23.4 | 177.5 | 0.002 |
| 1.9 | 0.01 | 0.072 | 18100 | 12.3 | 7.8 | 12900 | 686 | 231 | 25100 | 2.9 | 10.2 | 620 | 8.2 | 93.2 | 0.185 |
| 0.7 | 0.02 | 0.026 | 18100 | 6.3 | 3.5 | 10200 | 191 | 80.8 | 38300 | 3.8 | 4.1 | 1390 | 3.8 | 54.2 | 0.073 |
| 0.7 | 0.01 | 0.05 | 15600 | 8.7 | 8.3 | 11600 | 451 | 72.5 | 34900 | 5.1 | 4.2 | 1830 | 4.7 | 47.1 | 0.049 |
| 1 | 0.02 | 0.042 | 20600 | 10.6 | 13.3 | 18900 | 429 | 257 | 13800 | 4.2 | 5.5 | 1220 | 3.2 | 61.2 | 0.221 |
| 1.6 | 0.005 | 0.027 | 12200 | 10.8 | 7 | 7900 | 339 | 77.8 | 37400 | 4.5 | 8.1 | 500 | 2.5 | 37.7 | 0.02 |
| 1.9 | 0.005 | 0.062 | 16000 | 11.8 | 17.6 | 26200 | 853 | 479 | 19300 | 4.5 | 35 | 980 | 5.3 | 47.1 | 0.145 |
| 1.4 | 0.02 | 0.036 | 9700 | 2.8 | 3.5 | 4000 | 278 | 176.5 | 47600 | 3.9 | 5.9 | 550 | 7.1 | 28.5 | 0.043 |
| 0.9 | 0.01 | 0.05 | 16800 | 9.7 | 7.4 | 9100 | 189 | 97.4 | 42800 | 4.5 | 2.7 | 1430 | 2.5 | 55.2 | 0.09 |
| 0.8 | 0.01 | 0.053 | 14600 | 11 | 15 | 18800 | 436 | 374 | 38300 | 4.3 | 2.5 | 1450 | 3.3 | 57.8 | 0.346 |
| 0.8 | 0.01 | 0.09 | 15900 | 9.7 | 7.2 | 13900 | 275 | 173 | 38600 | 4 | 2.8 | 1390 | 3.8 | 61.3 | 0.145 |
| 1.2 | 0.005 | 0.073 | 7600 | 9.1 | 11.6 | 16400 | 1085 | 22.8 | 40800 | 4.4 | 1.7 | 1440 | 6.7 | 20.9 | 0.008 |
| 0.9 | 0.02 | 0.054 | 16000 | 8.3 | 12.1 | 15500 | 436 | 11.9 | 33600 | 4.1 | 4.5 | 1360 | 4.4 | 63.7 | 0.002 |
| 1.4 | 0.01 | 0.058 | 19200 | 8.5 | 10.3 | 12400 | 517 | 215 | 27300 | 4.4 | 4.2 | 1380 | 3.6 | 56.5 | 0.137 |
| 1 | 0.005 | 0.037 | 18200 | 8.9 | 7.5 | 9600 | 386 | 67.7 | 35000 | 4.6 | 2.2 | 1410 | 2.7 | 48.2 | 0.05 |
| 1.1 | 0.01 | 0.055 | 20200 | 10.7 | 8.2 | 10400 | 281 | 102 | 32400 | 4.6 | 2.6 | 1470 | 2.8 | 64.7 | 0.072 |
| 0.8 | 0.005 | 0.053 | 24000 | 12.1 | 6.9 | 10300 | 150 | 250 | 36900 | 3.9 | 3.1 | 1380 | 2.3 | 80.6 | 0.15 |
| 0.9 | 0.01 | 0.053 | 18700 | 10.9 | 11.3 | 12100 | 191 | 170.5 | 38200 | 4.4 | 3 | 1520 | 2.3 | 65.9 | 0.135 |
| 0.9 | 0.01 | 0.029 | 19500 | 6.4 | 16 | 15200 | 559 | 212 | 26700 | 4.6 | 4.2 | 1330 | 3.3 | 54.7 | 0.147 |
| 1.2 | 0.06 | 0.037 | 20800 | 10.1 | 11.8 | 16300 | 493 | 580 | 20000 | , | 4.6 | 1080 | 7.6 | 83.3 | 0.936 |
| 0.8 | 0.02 | 0.068 | 20900 | 7.8 | 9.4 | 17000 | 438 | 52.3 | 26700 | 4.9 | 5.2 | 1230 | 2.8 | 59.1 | 0.052 |
| 0.8 | 0.03 | 0.032 | 17500 | 10.7 | 10.2 | 18200 | 507 | 182.5 | 32900 | 5 | 3.9 | 1280 | 5.9 | 65.3 | 0.119 |
| 1.1 | 0.02 | 0.032 | 16900 | 6.9 | 26.3 | 37900 | 319 | 128 | 24600 | 5.9 | 23.4 | 1290 | 2.7 | 63.3 | 0.143 |
| 1.8 | 0.02 | 0.035 | 16000 | 12.7 | 18.9 | 16500 | 493 | 500 | 34600 | 5.1 | 5.5 | 1300 | 5.4 | 84.9 | 0.326 |
| 1 | 0.01 | 0.042 | 12300 | 8.7 | 12.3 | 19200 | 374 | 240 | 44300 | 5.9 | 7.3 | 1230 | 2.7 | 65.6 | 0.109 |
| 1.1 | 0.01 | 0.042 | 11700 | 10.7 | 13 | 24700 | 613 | 8.29 | 35400 | 5.8 | 10.6 | 1200 | 2.8 | 51.1 | 0.003 |
| 1.4 | 0.005 | 0.029 | 16400 | 14.4 | 3.3 | 5600 | 301 | 84.7 | 34300 | 2.7 | 6.4 | 540 | 1.6 | 42.9 | 0.065 |
| 1.8 | 0.01 | 0.0025 | 22100 | 12.5 | 5.8 | 15100 | 611 | 641 | 30000 | 4.7 | 7.6 | 1400 | 3.4 | 83.4 | 0.499 |
| 1.4 | 0.01 | 0.019 | 12800 | 8.2 | 11.2 | 22400 | 401 | 661 | 43600 | 5.4 | 16.2 | 1220 | 20.6 | 62 | 0.436 |
| 1 | 0.005 | 0.048 | 12900 | 8.7 | 27.7 | 22000 | 543 | 28.4 | 35800 | 7 | 15.5 | 1250 | 2.2 | 42.3 | 0.04 |
| 1 | 0.04 | 0.058 | 12100 | 9.5 | 25.9 | 27300 | 364 | 120 | 32000 | 4.5 | 9.1 | 1530 | 2.8 | 47.7 | 0.113 |
| 1.4 | 0.04 | 0.056 | 13200 | 8.7 | 24.9 | 28400 | 327 | 77.4 | 33900 | 4.3 | 7.9 | 1530 | 2.4 | 67.7 | 0.088 |
| 1.5 | 0.005 | 0.055 | 11800 | 11 | 7.9 | 14000 | 273 | 14.05 | 35000 | 5.5 | 1.3 | 1330 | 2.4 | 52.5 | 0.004 |
| 1.2 | 0.005 | 0.069 | 18600 | 10.1 | 9.9 | 12100 | 529 | 12.65 | 29900 | 5.1 | 1.6 | 1270 | 2.3 | 67.6 | 0.011 |
| 1.4 | 0.01 | 0.058 | 14200 | 9.7 | 6.4 | 11700 | 230 | 101 | 32200 | 4.2 | 4.7 | 1030 | 3.6 | 53.4 | 0.062 |
| 1.6 | 0.01 | 0.027 | 15800 | 10.1 | 7.6 | 11800 | 337 | 27 | 31500 | 5 | 6.7 | 1550 | 2.8 | 53.5 | 0.033 |
| 2.2 | 0.01 | 0.028 | 15800 | 9.4 | 8.2 | 12700 | 345 | 31.3 | 32900 | 4.9 | 5.8 | 1470 | 2.4 | 58.1 | 0.04 |
| 0.7 | 0.005 | 0.022 | 12400 | 6.5 | 14.1 | 22100 | 631 | 53.3 | 31400 | 5.9 | 3.9 | 1540 | 2.3 | 26.5 | 0.071 |
| 1.5 | 0.01 | 0.034 | 10200 | 9 | 16.7 | 27200 | 493 | 101 | 36600 | 6.5 | 19.8 | 1260 | 3.1 | 52.4 | 0.033 |
| 0.9 | 0.01 | 0.024 | 7700 | 7 | 26.2 | 41300 | 546 | 19.2 | 34100 | 6.1 | 22.1 | 1260 | 3.3 | 18.9 | 0.014 |
| 1.4 | 0.005 | 0.042 | 13700 | 9 | 17 | 24000 | 527 | 102.5 | 44700 | 7.1 | 18.7 | 1310 | 2.8 | 41.1 | 0.082 |
| 2.3 | 0.01 | 0.023 | 16100 | 11 | 21.2 | 18300 | 379 | 17.15 | 47300 | 4.6 | 8.4 | 1100 | 3.8 | 50.4 | 0.01 |
| 1.2 | 0.01 | 0.045 | 15400 | 7.8 | 16.2 | 20400 | 408 | 27.5 | 35600 | 6.8 | 16 | 1230 | 2.5 | 55 | 0.009 |
| 0.9 | 0.01 | 0.036 | 12500 | 8.6 | 14.9 | 16300 | 452 | 65.2 | 41400 | 4.8 | 2.2 | 1440 | 2.5 | 42.7 | 0.035 |
| 0.7 | 0.01 | 0.027 | 14800 | 8.2 | 12.4 | 17400 | 584 | 74 | 34400 | 5 | 4.4 | 1260 | 2.4 | 40.8 | 0.042 |
| 1 | 0.005 | 0.035 | 18500 | 9.9 | 7.4 | 17700 | 539 | 17.9 | 26200 | 5.6 | 12.4 | 1120 | 3.2 | 70.5 | 0.01 |

Project:
Client:
Comments:

| Sample | Hafnium | Mercury | Indium | Potassium | Lanthanum | Lithium | Magnesium | Manganese | Molybdenum | Sodium | Niobium | Nickel | Phosphorus | Lead | Rubidium | Rhenium |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Id. | Hf | Hg | In | K | La | Li | Mg | Mn | Mo | Na | Nb | Ni | P | Pb | Rb | Re |
|  | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) |
| Method | ME-MS61 | Hg-CV41 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 |
| MDL | 0.1 | 0.01 | 0.005 | 100 | 0.5 | 0.2 | 100 | 5 | 0.05 | 100 | 0.1 | 0.2 | 10 | 0.5 | 0.1 | 0.002 |
| Crustal Abundance: From | 0.3 | 0.03 | 0.01 | 40 | 10 | 5 | 1600 | 390 | 0.2 | 400 | 0.3 | 2 | 170 | 1 | 0.2 | NA |
| Crustal Abundance: To | 11 | 0.4 | 0.26 | 48000 | 115 | 66 | 47000 | 6700 | 27 | 40400 | 35 | 225 | 1500 | 80 | 170 | NA |
| 15879 | 1.2 | 0.01 | 0.035 | 14900 | 9.4 | 10.4 | 18800 | 554 | 20 | 32900 | 6.9 | 15.3 | 1280 | 3.8 | 56.7 | 0.018 |
| 15887 | 1 | 0.01 | 0.044 | 11900 | 6.7 | 11.3 | 15900 | 395 | 165.5 | 39300 | 6.5 | 11.6 | 1090 | 3.5 | 39.8 | 0.213 |
| 15891 | 0.9 | 0.01 | 0.021 | 17200 | 7.7 | 10.8 | 17300 | 558 | 104 | 34900 | 5.4 | 10.8 | 1120 | 3.6 | 60.8 | 0.08 |
| 15908 | 1 | 0.03 | 0.039 | 18000 | 8.4 | 10.9 | 18500 | 433 | 311 | 29000 | 6.1 | 12.6 | 1130 | 2.8 | 69.3 | 0.226 |
| 15911 | 1 | 0.02 | 0.027 | 13800 | 9.2 | 11.6 | 23100 | 402 | 154 | 32500 | 6.6 | 17.7 | 1250 | 2.5 | 69.5 | 0.135 |
| Maximum | 2.3 | 0.06 | 0.09 | 32000 | 14.4 | 27.7 | 41300 | 1585 | 661 | 47600 | 7.1 | 35 | 1830 | 236 | 178 | 0.94 |
| Minimum | 0.7 | 0.005 | 0.0025 | 7600 | 2.8 | 3.3 | 4000 | 150 | 6.9 | 5400 | 2.5 | 1.3 | 470 | 1.6 | 18.9 | 0.002 |
| Mean | 1.26 | 0.013 | 0.045 | 16247 | 9.54 | 12.8 | 17175 | 498 | 162 | 32500 | 4.71 | 9.02 | 1189 | 11.6 | 63.3 | 0.12 |
| Standard Deviation | 0.42 | 0.01 | 0.018 | 4772 | 1.99 | 6.3 | 7171 | 260 | 173 | 8004 | 1.19 | 6.66 | 309 | 32.9 | 28.3 | 0.15 |
| 10 Percentile | 0.8 | 0.005 | 0.026 | 11600 | 6.88 | 6.8 | 9180 | 275 | 16.5 | 23640 | 2.98 | 2.58 | 570 | 2.38 | 40.6 | 0.0098 |
| 25 Percentile | 0.9 | 0.005 | 0.032 | 12650 | 8.45 | 8.05 | 11950 | 354 | 33.8 | 29450 | 4.05 | 4.2 | 1095 | 2.6 | 49.3 | 0.034 |
| Median | 1.2 | 0.01 | 0.042 | 15900 | 9.7 | 11.3 | 16500 | 446 | 101 | 33600 | 4.6 | 6.9 | 1260 | 3.3 | 58.1 | 0.08 |
| 75 Percentile | 1.5 | 0.01 | 0.056 | 18550 | 10.8 | 16.4 | 20700 | 550 | 218 | 36750 | 5.45 | 12.5 | 1390 | 5.35 | 67.8 | 0.14 |
| 90 Percentile | 1.9 | 0.02 | 0.07 | 21460 | 11.9 | 22.9 | 26320 | 705 | 395 | 41680 | 6.5 | 17.3 | 1480 | 20.1 | 85.8 | 0.24 |
| Interquartile Range (IQR) ${ }^{1}$ | 0.6 | 0.005 | 0.024 | 5900 | 2.3 | 8.4 | 8750 | 196 | 184 | 7300 | 1.4 | 8.3 | 295 | 2.75 | 18.5 | 0.11 |
| Variance | 0.17 | 0.0001 | 0.00033 | 22775295 | 3.98 | 39.7 | 51419515 | 67837 | 29834 | 64062759 | 1.41 | 44.3 | 95722 | 1086 | 802 | 0.023 |
| Skewness | 0.68 | 2.59 | 0.42 | 1.01 | -0.45 | 0.84 | 0.98 | 2.21 | 1.63 | -0.9 | 0.088 | 1.43 | -1 | 5.92 | 2.14 | 3.26 |
| Coefficient of Variation (CoV) ${ }^{2}$ | 0.33 | 0.81 | 0.4 | 0.29 | 0.21 | 0.49 | 0.42 | 0.52 | 1.07 | 0.25 | 0.25 | 0.74 | 0.26 | 2.84 | 0.45 | 1.24 |
| Count | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 |

Schaft Creek
Copper Fox Metals Inc.
ICP Metals Data
Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.
3.36 NOTE: if data is boxed, then data is 3 times the maximum crustal abundance.
${ }^{1}$ Interquartile Range (IQR) $=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) $=$ standard deviation divided by mean
NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.
NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project:
Client:
Comments:

Schaft Creek
Copper Fox Metals Inc.
ICP Metals Data
Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

| Sample | Sulphur | Antimony | Scandium | Selenium | Tin | Strontium | Tantalum | Tellurium | Thorium | Titanium | Thallium | Uranium | Vanadium | Tungsten | Yttrium | Zinc | Zirconium |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Id. | S | Sb | Sc | Se | Sn | Sr | Ta | Te | Th | Ti | TI | U | V | W | Y | Zn | Zr |
|  | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) |
| Method | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 |
| MDL | 100 | 0.05 | 1 | 1 | 0.2 | 0.2 | 0.05 | 0.05 | 0.2 | 50 | 0.02 | 0.1 | 1 | 0.1 | 0.1 | 2 | 0.5 |
| Crustal Abundance: From | 240 | 0.1 | NA | 0.05 | 0.5 | 1 | 0.8 | NA | 0.004 | 300 | 0.16 | 0.45 | 20 | 0.6 | 20 | 16 | 19 |
| Crustal Abundance: To | 2400 | 1.5 | NA | 0.6 | 6 | 2000 | 4.2 | NA | 17 | 13800 | 2.3 | 3.7 | 250 | 2.2 | 90 | 165 | 500 |
| 14018 | 8800 | 3.69 | 7.9 | 2 | 1.1 | 428 | 0.32 | 0.26 | 3.7 | 2400 | 0.6 | 2.3 | 70 | 12.8 | 10.8 | 41 | 50.3 |
| 14021 | 7000 | 6.36 | 7.7 | 2 | 1.2 | 173 | 0.28 | 0.09 | 3.3 | 2080 | 0.75 | 1.9 | 65 | 18.4 | 12.5 | 56 | 45.5 |
| 14036 | 16000 | 7.99 | 7.3 | 4 | 1.5 | 235 | 0.21 | 0.72 | 3.3 | 1970 | 0.71 | 1.9 | 67 | 25 | 10.2 | 41 | 41.3 |
| 14043 | 2800 | 4.34 | 10.2 | 2 | 1 | 276 | 0.22 | 0.07 | 2.3 | 2190 | 0.42 | 1.4 | 102 | 27 | 7.6 | 45 | 40.3 |
| 14060 | 14800 | 2.49 | 16.5 | 3 | 1 | 423 | 0.22 | 0.06 | 2.4 | 4100 | 0.44 | 1.6 | 155 | 30.1 | 17.1 | 27 | 66.3 |
| 14067 | 4300 | 3.8 | 21.1 | 4 | 1.1 | 410 | 0.17 | 0.06 | 1.5 | 4170 | 0.38 | 1.1 | 182 | 12.1 | 17.5 | 71 | 49.5 |
| 14076 | 9500 | 5.5 | 24.4 | 2 | 1.2 | 365 | 0.18 | 0.18 | 1.9 | 4540 | 0.47 | 1 | 197 | 6.5 | 19.9 | 163 | 55.8 |
| 14083 | 16000 | 5.68 | 24.7 | 2 | 1.6 | 232 | 0.16 | 0.27 | 1.7 | 4480 | 0.95 | 0.9 | 204 | 10.3 | 19.5 | 127 | 40.6 |
| 14099 | 3600 | 3.71 | 5 | 1 | 0.6 | 88 | 0.24 | 0.05 | 2.7 | 1670 | 1.04 | 1.9 | 47 | 17.4 | 8.2 | 205 | 33.7 |
| 14103 | 7700 | 4.72 | 10.2 | 3 | 1.1 | 197.5 | 0.24 | 0.05 | 3 | 2220 | 0.67 | 1.8 | 119 | 20.2 | 10.4 | 67 | 51.2 |
| 14130 | 3200 | 1.25 | 6.3 | 5 | 0.9 | 288 | 0.22 | 0.51 | 0.8 | 2800 | 0.28 | 0.3 | 73 | 5.6 | 12.7 | 26 | 19.7 |
| 14144 | 2800 | 2.5 | 6.8 | 4 | 0.9 | 343 | 0.29 | 0.54 | 0.9 | 3760 | 0.27 | 0.5 | 91 | 4 | 16.2 | 46 | 19.6 |
| 14148 | 1400 | 2.35 | 11.4 | 3 | 1.2 | 223 | 0.25 | 0.27 | 0.8 | 3780 | 0.31 | 0.9 | 146 | 4.9 | 15.6 | 40 | 28.9 |
| 14156 | 1700 | 1.66 | 5.6 | 3 | 1.1 | 259 | 0.33 | 0.09 | 3.1 | 1900 | 0.17 | 1.9 | 47 | 10.5 | 8.5 | 35 | 39.3 |
| 14162 | 1500 | 2.42 | 21.4 | 2 | 1.2 | 239 | 0.28 | 0.17 | 1.8 | 4270 | 0.22 | 1.1 | 159 | 5.2 | 15.7 | 67 | 59.6 |
| 14169 | 3200 | 1.63 | 5.9 | 3 | 1.9 | 207 | 0.3 | 0.46 | 2.8 | 1960 | 0.15 | 1.7 | 65 | 13 | 6.3 | 24 | 36.9 |
| 14232 | 1600 | 3.64 | 6.8 | 3 | 1.1 | 345 | 0.27 | 0.23 | 0.9 | 3290 | 0.3 | 0.5 | 87 | 3.5 | 14.5 | 21 | 23.6 |
| 14250 | 2000 | 3.46 | 12.1 | 3 | 1.4 | 424 | 0.25 | 0.29 | 0.8 | 4350 | 0.28 | 0.5 | 236 | 3.3 | 16.9 | 38 | 18.3 |
| 14260 | 3700 | 2.5 | 11.4 | 6 | 1.6 | 402 | 0.23 | 0.85 | 0.7 | 4050 | 0.31 | 0.5 | 144 | 4.5 | 14.3 | 36 | 17.6 |
| 14276 | 1700 | 10.95 | 7.2 | 2 | 1 | 798 | 0.28 | 0.07 | 1 | 4100 | 0.14 | 0.6 | 112 | 4.9 | 17.8 | 112 | 29.9 |
| 14295 | 4900 | 3.4 | 14.1 | 2 | 1.8 | 336 | 0.25 | 0.08 | 0.7 | 4240 | 0.38 | 0.7 | 154 | 15.6 | 14.8 | 34 | 23.5 |
| 14301 | 3500 | 2.57 | 11 | 3 | 1.6 | 209 | 0.26 | 0.13 | 1 | 3620 | 0.3 | 0.6 | 117 | 10.5 | 14.7 | 38 | 47.1 |
| 14323 | 1500 | 2.29 | 6.5 | 2 | 1.3 | 391 | 0.27 | 0.17 | 0.8 | 3310 | 0.31 | 0.4 | 94 | 3.3 | 15.5 | 29 | 29.3 |
| 14332 | 2700 | 1.94 | 6.9 | 2 | 1.4 | 355 | 0.27 | 0.19 | 0.9 | 3260 | 0.32 | 0.5 | 103 | 3.5 | 16.6 | 31 | 32.2 |
| 14345 | 5600 | 2.33 | 7.3 | 5 | 3.8 | 274 | 0.24 | 0.29 | 0.9 | 2970 | 0.41 | 0.6 | 101 | 14.5 | 14.8 | 27 | 20 |
| 14348 | 4800 | 2.53 | 6.8 | 3 | 1.7 | 276 | 0.27 | 0.19 | 0.9 | 3190 | 0.4 | 0.5 | 74 | 5.8 | 13.9 | 40 | 22.1 |
| 14797 | 700 | 4.83 | 11 | 3 | 1.2 | 234 | 0.28 | 0.15 | 0.6 | 4150 | 0.38 | 0.3 | 152 | 5.7 | 12 | 42 | 20.9 |
| 14808 | 1900 | 5.13 | 9.8 | 7 | 1.4 | 221 | 0.24 | 0.45 | 1 | 3260 | 0.43 | 0.7 | 117 | 4.5 | 14.5 | 34 | 34 |
| 14816 | 4700 | 3.45 | 10.9 | 5 | 1.7 | 285 | 0.28 | 0.77 | 0.7 | 3810 | 0.36 | 0.4 | 144 | 6.2 | 13.1 | 49 | 18.4 |
| 14828 | 1400 | 1.72 | 11.4 | 6 | 1.1 | 404 | 0.29 | 0.5 | 0.8 | 3940 | 0.29 | 0.4 | 141 | 3.3 | 17.5 | 32 | 20.7 |
| 14844 | 2200 | 5.28 | 17.9 | 4 | 1.4 | 265 | 0.33 | 0.23 | 1 | 5590 | 0.49 | 0.6 | 262 | 3.3 | 13 | 40 | 30.5 |
| 14680 | 2200 | 5.2 | 12.8 | 8 | 1.4 | 348 | 0.3 | 0.77 | 1.1 | 4040 | 0.43 | 0.7 | 151 | 4.8 | 17.8 | 38 | 64.4 |
| 14871 | 3800 | 4.15 | 12.7 | 4 | 1.7 | 405 | 0.31 | 0.19 | 1 | 4990 | 0.32 | 0.7 | 183 | 6 | 15.3 | 43 | 22.6 |
| 14887 | 5400 | 1.41 | 14 | 2 | 1.3 | 424 | 0.33 | 0.09 | 1.2 | 4960 | 0.28 | 0.7 | 188 | 5.2 | 15.1 | 39 | 22.8 |
| 14689 | 7900 | 1.27 | 5.3 | 3 | 0.9 | 141 | 0.21 | 0.15 | 3.1 | 1580 | 0.18 | 1.6 | 51 | 3 | 8.3 | 16 | 33.4 |
| 14695 | 1600 | 3.83 | 11.9 | 5 | 1.5 | 226 | 0.25 | 0.18 | 1 | 4310 | 0.23 | 0.9 | 161 | 6 | 14.9 | 49 | 48.5 |
| 14742 | 2100 | 2.37 | 15.2 | 7 | 1.9 | 302 | 0.34 | 0.23 | 1.6 | 4690 | 0.25 | 0.9 | 215 | 6.6 | 12 | 53 | 32.7 |
| 14666 | 3800 | 3.07 | 15.1 | 3 | 1.5 | 416 | 0.41 | 0.06 | 1.3 | 5070 | 0.27 | 1 | 209 | 8 | 15.4 | 38 | 27.7 |
| 14685 | 21000 | 3.51 | 25.5 | 6 | 2.2 | 393 | 0.26 | 0.15 | 1.3 | 7690 | 0.32 | 1 | 269 | 5.5 | 14.5 | 43 | 35 |
| 14685B | 20400 | 3.19 | 23.4 | 5 | 1.9 | 374 | 0.25 | 0.14 | 1.4 | 7930 | 0.37 | 0.9 | 276 | 5.2 | 13.6 | 46 | 43.4 |
| 14545 | 1900 | 1.48 | 8.5 | 1 | 1.4 | 409 | 0.36 | 0.05 | 1.5 | 3980 | 0.26 | 0.8 | 90 | 4.2 | 16.3 | 26 | 44.7 |
| 14565 | 2600 | 4.4 | 8.3 | 2 | 1.4 | 259 | 0.32 | 0.14 | 1.3 | 3800 | 0.37 | 0.6 | 80 | 4.7 | 16.9 | 16 | 32.5 |
| 14571 | 11100 | 2.6 | 7.8 | 5 | 1.4 | 312 | 0.28 | 0.15 | 2.3 | 3170 | 0.26 | 1.3 | 86 | 4.8 | 11.2 | 34 | 42 |
| 14578 | 21300 | 2.42 | 11 | 4 | 1.4 | 324 | 0.33 | 0.11 | 1.8 | 4630 | 0.29 | 1.2 | 112 | 4.1 | 15.9 | 19 | 56 |
| 14578B | 21100 | 2.47 | 11.3 | 4 | 1.4 | 330 | 0.3 | 0.09 | 2 | 4430 | 0.32 | 1.2 | 111 | 4.1 | 17.1 | 19 | 74.1 |
| 14598 | 1500 | 1.89 | 8.4 | 2 | 0.9 | 569 | 0.36 | 0.06 | 0.6 | 4330 | 0.28 | 0.4 | 131 | 2.7 | 13.2 | 47 | 22.7 |
| 14893 | 1100 | 6.95 | 20.1 | 3 | 1.7 | 379 | 0.36 | 0.12 | 1.3 | 6030 | 0.25 | 1.5 | 283 | 9.3 | 15.3 | 49 | 40.7 |
| 14899 | 200 | 3.09 | 19.4 | 2 | 1 | 366 | 0.34 | 0.06 | 1 | 5850 | 0.16 | 0.6 | 262 | 8.2 | 13.8 | 52 | 25.5 |
| 14908 | 900 | 4.87 | 19 | 2 | 1.6 | 479 | 0.39 | 0.1 | 1.6 | 5910 | 0.22 | 1.2 | 268 | 12.1 | 16.7 | 42 | 34.7 |
| 14917 | 1900 | 4.6 | 17.7 | 4 | 1.7 | 309 | 0.3 | 0.26 | 2.8 | 4580 | 0.22 | 1.7 | 178 | 8.9 | 16.1 | 44 | 74.3 |
| 14925 | 1500 | 6.54 | 15.5 | 3 | 1.7 | 353 | 0.38 | 0.11 | 1.4 | 5090 | 0.29 | 0.7 | 224 | 5.1 | 15 | 52 | 31 |
| 14998 | 1300 | 5.17 | 10.8 | 3 | 1.4 | 412 | 0.26 | 0.16 | 0.7 | 4460 | 0.3 | 0.6 | 152 | 13.5 | 16.6 | 41 | 22.5 |
| 15862 | 800 | 2.81 | 11.3 | 2 | 1.1 | 327 | 0.29 | 0.12 | 0.7 | 4050 | 0.29 | 0.3 | 146 | 2.9 | 14 | 49 | 17.8 |
| 15870 | 1400 | 6.6 | 14.3 | 3 | 1.4 | 234 | 0.31 | 0.15 | 1.3 | 4460 | 0.36 | 0.8 | 203 | 6.1 | 16.1 | 53 | 23.4 |

Project:
Client:
Comments:
Sample
Id.
Method
MDL
Crustal Abundance: From
Crustal Abundance: To Crustal Abundance: To

## 15887 <br> 15891 <br> 15908 <br> 15911

## Minimum <br> Mean

Standard Deviation
Percentile
25 Percentile
Median
75 Percentile
90 Percentile

Varianc
Skewnes
Coefficient of Variation (CoV) ${ }^{2}$
Count

Schaft Creek
Copper Fox Metals Inc.
ICP Metals Data
Sampled by MDAG on Feb 7'07.
Rare earth elements may not be totally soluble in MS61 method.
ICP-MS: Interference: Samples with Molybdenum >100ppm will cause a low bias on Cadmium-MS61<1ppm
Interference: Mo>400ppm on ICP-MS Cd,ICP-AES results shown.

| Sulphur S | Antimony Sb | Scandium Sc | Selenium Se | $\begin{aligned} & \text { Tin } \\ & \mathrm{Sn} \end{aligned}$ | Strontium Sr | Tantalum Ta | Tellurium Te | Thorium Th | Titanium Ti | Thallium TI | Uranium U | Vanadium V | Tungsten W | Yttrium Y | $\begin{aligned} & \text { Zinc } \\ & \text { Zn } \end{aligned}$ | $\begin{aligned} & \text { Zirconium } \\ & \quad \mathrm{Zr} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) |
| ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 | ME-MS61 |
| 100 | 0.05 | 1 | 1 | 0.2 | 0.2 | 0.05 | 0.05 | 0.2 | 50 | 0.02 | 0.1 | 1 | 0.1 | 0.1 | 2 | 0.5 |
| 240 | 0.1 | NA | 0.05 | 0.5 | 1 | 0.8 | NA | 0.004 | 300 | 0.16 | 0.45 | 20 | 0.6 | 20 | 16 | 19 |
| 2400 | 1.5 | NA | 0.6 | 6 | 2000 | 4.2 | NA | 17 | 13800 | 2.3 | 3.7 | 250 | 2.2 | 90 | 165 | 500 |
| 1200 | 7.41 | 17.1 | 3 | 1.3 | 373 | 0.39 | 0.16 | 1.5 | 5450 | 0.28 | 0.9 | 246 | 3.3 | 16 | 63 | 27.3 |
| 3300 | 5.99 | 15.3 | 5 | 1.7 | 402 | 0.34 | 0.37 | 1 | 5100 | 0.24 | 0.7 | 214 | 3.6 | 13.6 | 42 | 23.2 |
| 1400 | 7.05 | 15 | 4 | 1.3 | 382 | 0.3 | 0.23 | 1.1 | 4920 | 0.31 | 0.6 | 213 | 5.3 | 15.1 | 51 | 19.4 |
| 2200 | 6.21 | 14.2 | 5 | 1.5 | 288 | 0.32 | 0.29 | 1.2 | 4740 | 0.34 | 0.8 | 207 | 5.4 | 15.5 | 43 | 26.1 |
| 900 | 4.97 | 17.9 | 3 | 1.3 | 335 | 0.37 | 0.13 | 1.5 | 5430 | 0.29 | 0.7 | 248 | 3 | 15.3 | 49 | 26.4 |
| 21300 | 11 | 25.5 | 8 | 3.8 | 798 | 0.41 | 0.85 | 3.7 | 7930 | 1.04 | 2.3 | 283 | 30.1 | 19.9 | 205 | 74.3 |
| 200 | 1.25 | 5 | 1 | 0.6 | 88 | 0.16 | 0.05 | 0.6 | 1580 | 0.14 | 0.3 | 47 | 2.7 | 6.3 | 16 | 17.6 |
| 4966 | 3.93 | 12.6 | 3.46 | 1.41 | 330 | 0.29 | 0.22 | 1.5 | 4086 | 0.35 | 0.93 | 152 | 8.08 | 14.4 | 48.1 | 34.9 |
| 5631 | 1.97 | 5.39 | 1.53 | 0.44 | 108 | 0.055 | 0.19 | 0.81 | 1307 | 0.17 | 0.5 | 66.7 | 6.18 | 2.86 | 32 | 14.5 |
| 1180 | 1.71 | 6.74 | 2 | 1 | 219 | 0.22 | 0.06 | 0.7 | 2168 | 0.22 | 0.4 | 69.4 | 3.3 | 10.4 | 25.6 | 19.7 |
| 1500 | 2.45 | 7.85 | 2 | 1.1 | 259 | 0.25 | 0.095 | 0.9 | 3275 | 0.27 | 0.6 | 97.5 | 4.15 | 13.2 | 34 | 23 |
| 2700 | 3.51 | 11.4 | 3 | 1.4 | 335 | 0.28 | 0.16 | 1.3 | 4150 | 0.31 | 0.8 | 146 | 5.5 | 15 | 42 | 32.2 |
| 5150 | 5.15 | 15.4 | 4 | 1.6 | 398 | 0.32 | 0.26 | 1.8 | 4715 | 0.38 | 1.2 | 206 | 10.4 | 16.2 | 49 | 42.7 |
| 15040 | 6.55 | 20.3 | 5.2 | 1.72 | 423 | 0.36 | 0.5 | 2.84 | 5478 | 0.51 | 1.72 | 251 | 16 | 17.2 | 67 | 55.8 |
| 3650 | 2.7 | 7.55 | 2 | 0.5 | 138 | 0.075 | 0.17 | 0.9 | 1440 | 0.11 | 0.6 | 108 | 6.25 | 3 | 15 | 19.7 |
| 31711935 | 3.88 | 29.1 | 2.36 | 0.19 | 11719 | 0.0031 | 0.037 | 0.66 | 1709027 | 0.03 | 0.25 | 4454 | 38.2 | 8.16 | 1027 | 211 |
| 1.91 | 1.03 | 0.69 | 0.9 | 2.75 | 1.22 | 0.037 | 1.81 | 1.15 | 0.35 | 2.21 | 0.95 | 0.29 | 1.9 | -0.91 | 3.21 | 1 |
| 1.13 | 0.5 | 0.43 | 0.44 | 0.31 | 0.33 | 0.19 | 0.86 | 0.54 | 0.32 | 0.49 | 0.53 | 0.44 | 0.76 | 0.2 | 0.67 | 0.42 |
| 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 |
| 3.36 | NOTE: if | ta is box | d, then dat | s 3 times | he maximu | crustal ab | undance. |  |  |  |  |  |  |  |  |  |

${ }^{1}$ Interquartile Range (IQR) $=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) = standard deviation divided by mean
NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.
NOTE: If data was reported as > detection limit the detection limit is shown in bold and was used in subsequent calculations.

Project:
Data:
Comments:

| Sample <br> Id. | $\begin{gathered} \mathrm{Al}_{2} \mathrm{O}_{3} \\ (\%) \end{gathered}$ |  |  | $\mathrm{Cr}_{2} \mathrm{O}_{3}$ <br> (\%) | $\mathrm{Fe}_{2} \mathrm{O}_{3}$ <br> (\%) | $\mathrm{K}_{2} \mathrm{O}$ (\%) | MgO <br> (\%) | $\underset{(\%)}{\text { MnO }}$ | $\mathrm{Na}_{2} \mathrm{O}$ <br> (\%) | $\mathrm{P}_{2} \mathrm{O}_{5}$ (\%) | $\mathrm{SiO}_{2}$ <br> (\%) | SrO |  | LOI | Total <br> (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Method | $\underset{\text { ME-XRF06 }}{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{\text {(\%) }}$ | (\%) ME-XRF06 | $\stackrel{(\%)}{\text { ME-XRF06 }}$ | $\underset{\text { ME-XRF06 }}{(\%)}$ | $\underset{\text { ME-XRF06 }}{(\%)}$ | ${ }_{\text {ME-XRF06 }}^{(\%)}$ | $\underset{\text { ME-XRF06 }}{(\%)}$ |
| MDL | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |  |  |
| 14018 | 16.2 | 0.13 | 2.53 | 0.005 | 3.77 | 2.92 | 1.74 | 0.05 | 4.01 | 0.14 | 62.92 | 0.05 | 0.42 | 3.69 | 98.58 |
| 14021 | 14.75 | 0.05 | 3.56 | 0.005 | 2.62 | 2.59 | 1.47 | 0.07 | 2.96 | 0.12 | 65.03 | 0.02 | 0.36 | 4.86 | 98.47 |
| 14036 | 14.93 | 0.06 | 2.56 | 0.005 | 3.72 | 2.51 | 1.51 | 0.05 | 3.13 | 0.12 | 64.89 | 0.03 | 0.38 | 4.53 | 98.43 |
| 14043 | 15.21 | 0.03 | 1.98 | 0.005 | 4.23 | 1.18 | 3.06 | 0.05 | 4.13 | 0.12 | 64.74 | 0.03 | 0.41 | 3.53 | 98.71 |
| 14060 | 15.16 | 0.04 | 4.27 | 0.005 | 5.14 | 1.42 | 3.28 | 0.05 | 3.71 | 0.26 | 58.18 | 0.05 | 0.73 | 6.18 | 98.48 |
| 14067 | 16.07 | 0.04 | 3.54 | 0.01 | 6.18 | 1.29 | 4.07 | 0.09 | 4.15 | 0.22 | 57.69 | 0.04 | 0.7 | 4.08 | 98.17 |
| 14076 | 16.09 | 0.05 | 5.61 | 0.005 | 7.43 | 1.58 | 3.72 | 0.19 | 2.64 | 0.21 | 55.56 | 0.04 | 0.72 | 5.1 | 98.95 |
| 14083 | 16.4 | 0.08 | 5.33 | 0.005 | 8.26 | 3.49 | 2.82 | 0.17 | 1.62 | 0.21 | 53.34 | 0.02 | 0.74 | 6.28 | 98.77 |
| 14099 | 15.15 | 0.1 | 4.16 | 0.005 | 3.38 | 3.94 | 1.47 | 0.14 | 0.73 | 0.11 | 63.71 | 0.01 | 0.31 | 5.67 | 98.89 |
| 14103 | 15 | 0.03 | 4.03 | 0.005 | 3.11 | 2.07 | 2.04 | 0.08 | 2.99 | 0.13 | 61.55 | 0.02 | 0.41 | 6.91 | 98.38 |
| 14130 | 17.11 | 0.06 | 3.59 | 0.005 | 2.6 | 2.11 | 1.61 | 0.02 | 4.61 | 0.28 | 60.15 | 0.03 | 0.53 | 5.91 | 98.62 |
| 14144 | 18.29 | 0.04 | 4.95 | 0.005 | 5.05 | 1.84 | 1.81 | 0.05 | 4.05 | 0.36 | 53.8 | 0.04 | 0.63 | 7.48 | 98.40 |
| 14148 | 16.83 | 0.07 | 6.26 | 0.005 | 5.63 | 2.49 | 3.13 | 0.05 | 1.72 | 0.26 | 52 | 0.03 | 0.64 | 9.85 | 98.97 |
| 14156 | 15.34 | 0.03 | 3.29 | 0.005 | 2.46 | 1.41 | 1.21 | 0.03 | 4.53 | 0.1 | 64.96 | 0.03 | 0.29 | 4.66 | 98.35 |
| 14162 | 14.36 | 0.06 | 7.5 | 0.01 | 5.92 | 1.79 | 3.97 | 0.1 | 2.27 | 0.2 | 50.21 | 0.02 | 0.69 | 11.1 | 98.20 |
| 14169 | 15.54 | 0.01 | 3.15 | 0.005 | 1.69 | 1.07 | 0.61 | 0.03 | 5.76 | 0.12 | 66.91 | 0.02 | 0.31 | 3.74 | 98.97 |
| 14232 | 19.47 | 0.02 | 3.67 | 0.005 | 3.86 | 2.01 | 1.48 | 0.02 | 5.31 | 0.3 | 56.55 | 0.04 | 0.61 | 5.19 | 98.54 |
| 14250 | 18.02 | 0.02 | 5.47 | 0.005 | 6.59 | 1.67 | 2.87 | 0.05 | 4.48 | 0.28 | 51.91 | 0.04 | 0.75 | 6.29 | 98.45 |
| 14260 | 17.85 | 0.02 | 4.18 | 0.005 | 6.23 | 1.9 | 2.21 | 0.03 | 4.77 | 0.28 | 54.62 | 0.04 | 0.72 | 5.77 | 98.63 |
| 14276 | 19.76 | 0.12 | 5.87 | 0.005 | 5.6 | 0.86 | 2.56 | 0.14 | 4.97 | 0.29 | 54.07 | 0.08 | 0.67 | 3.49 | 98.49 |
| 14295 | 17.5 | 0.01 | 5.22 | 0.005 | 6.81 | 1.83 | 2.43 | 0.05 | 4 | 0.27 | 53.53 | 0.03 | 0.73 | 6.48 | 98.90 |
| 14301 | 17.72 | 0.03 | 4.93 | 0.005 | 4.47 | 2.34 | 2 | 0.06 | 3.33 | 0.28 | 54.86 | 0.02 | 0.7 | 7.95 | 98.70 |
| 14323 | 19.07 | 0.03 | 5.02 | 0.005 | 5.54 | 2.1 | 1.55 | 0.04 | 4.17 | 0.28 | 54.65 | 0.04 | 0.56 | 5.5 | 98.56 |
| 14332 | 19.78 | 0.02 | 4.67 | 0.005 | 5.19 | 2.46 | 1.71 | 0.03 | 4.03 | 0.3 | 54.16 | 0.04 | 0.6 | 5.57 | 98.57 |
| 14345 | 19.52 | 0.02 | 3.44 | 0.005 | 3.18 | 2.73 | 1.64 | 0.01 | 4.47 | 0.28 | 57.5 | 0.03 | 0.58 | 5.16 | 98.57 |
| 14348 | 19.93 | 0.02 | 3.09 | 0.005 | 5.12 | 2.25 | 1.97 | 0.02 | 4.79 | 0.31 | 54.97 | 0.03 | 0.61 | 5.01 | 98.13 |
| 14797 | 18.18 | 0.02 | 5.12 | 0.005 | 6.2 | 2.28 | 2.46 | 0.06 | 3.22 | 0.27 | 51.74 | 0.03 | 0.7 | 8.21 | 98.50 |
| 14808 | 15.54 | 0.02 | 6.64 | 0.005 | 5.44 | 2.49 | 2.62 | 0.06 | 2.5 | 0.23 | 52.62 | 0.02 | 0.56 | 10.2 | 98.95 |
| 14816 | 17.11 | 0.02 | 4.56 | 0.005 | 6.06 | 2.5 | 2.78 | 0.05 | 3.25 | 0.26 | 53.34 | 0.03 | 0.65 | 7.62 | 98.24 |
| 14828 | 17.1 | 0.08 | 5.7 | 0.005 | 5.75 | 1.94 | 2.73 | 0.06 | 3.81 | 0.25 | 51.87 | 0.04 | 0.63 | 8.24 | 98.21 |
| 14844 | 17.61 | 0.04 | 3.8 | 0.005 | 7.4 | 1.98 | 5.94 | 0.03 | 2.92 | 0.26 | 52.79 | 0.03 | 0.93 | 5.17 | 98.91 |
| 14680 | 17.54 | 0.03 | 5.54 | 0.01 | 6.31 | 1.81 | 2.5 | 0.06 | 4.05 | 0.26 | 53.34 | 0.04 | 0.67 | 6.08 | 98.24 |
| 14871 | 18.56 | 0.01 | 4.62 | 0.005 | 6.55 | 1.36 | 2.87 | 0.04 | 5.16 | 0.24 | 53.53 | 0.04 | 0.82 | 4.77 | 98.58 |
| 14887 | 17.6 | 0.04 | 6.71 | 0.005 | 7.31 | 1.24 | 3.61 | 0.07 | 4.05 | 0.23 | 50.56 | 0.04 | 0.79 | 6.23 | 98.49 |
| 14689 | 15.75 | 0.01 | 2.71 | 0.005 | 1.96 | 1.91 | 0.91 | 0.03 | 4.34 | 0.11 | 66.25 | 0.02 | 0.33 | 3.81 | 98.15 |
| 14695 | 17.98 | 0.02 | 4.98 | 0.005 | 5.19 | 2.57 | 2.41 | 0.07 | 3.57 | 0.26 | 53.38 | 0.02 | 0.68 | 7.34 | 98.48 |
| 14742 | 18.48 | 0.02 | 3.84 | 0.005 | 4.8 | 1.49 | 3.39 | 0.04 | 5.21 | 0.25 | 54.87 | 0.03 | 0.86 | 4.97 | 98.26 |
| 14666 | 17.45 | 0.04 | 5.2 | 0.005 | 7.38 | 1.53 | 3.59 | 0.06 | 4.43 | 0.25 | 53.21 | 0.04 | 0.84 | 4.88 | 98.91 |
| 14685 | 16.54 | 0.05 | 4.49 | 0.005 | 8.92 | 1.47 | 4.51 | 0.04 | 4.03 | 0.31 | 49.87 | 0.04 | 1.38 | 7.01 | 98.67 |
| 14685B | 16.58 | 0.04 | 4.16 | 0.005 | 9.45 | 1.54 | 4.37 | 0.04 | 3.98 | 0.3 | 50.4 | 0.04 | 1.38 | 5.99 | 98.28 |
| 14545 | 18.58 | 0.1 | 5.18 | 0.005 | 5.98 | 1.37 | 2.17 | 0.03 | 4.2 | 0.27 | 56.26 | 0.04 | 0.65 | 4.1 | 98.94 |
| 14565 | 17.23 | 0.02 | 6.05 | 0.005 | 5.25 | 2.14 | 1.89 | 0.06 | 3.57 | 0.26 | 53.85 | 0.03 | 0.63 | 7.44 | 98.43 |
| 14571 | 16.48 | 0.05 | 3.51 | 0.005 | 3.99 | 1.76 | 2.03 | 0.02 | 4.32 | 0.22 | 59.95 | 0.04 | 0.59 | 5.14 | 98.11 |
| 14578 | 16.78 | 0.07 | 5.57 | 0.005 | 5.71 | 1.89 | 1.99 | 0.04 | 4 | 0.31 | 54.01 | 0.03 | 0.86 | 7.27 | 98.54 |
| 14578B | 16.4 | 0.09 | 5.75 | 0.005 | 5.95 | 1.84 | 1.97 | 0.04 | 3.91 | 0.3 | 54.47 | 0.03 | 0.82 | 6.61 | 98.19 |
| 14598 | 19.18 | 0.02 | 4.52 | 0.005 | 6.5 | 1.54 | 3.79 | 0.07 | 3.95 | 0.31 | 52.94 | 0.06 | 0.74 | 5.22 | 98.85 |
| 14893 | 17.39 | 0.05 | 5.57 | 0.005 | 7.59 | 1.11 | 4.07 | 0.06 | 4.23 | 0.25 | 50.42 | 0.04 | 1 | 6.37 | 98.16 |
| 14899 | 18.24 | 0.04 | 4.77 | 0.005 | 8.14 | 0.9 | 6.3 | 0.06 | 3.94 | 0.25 | 48.95 | 0.04 | 0.97 | 5.91 | 98.52 |
| 14908 | 17.57 | 0.08 | 4.99 | 0.005 | 7.49 | 1.51 | 3.56 | 0.06 | 5.09 | 0.26 | 52.92 | 0.05 | 0.97 | 3.87 | 98.43 |
| 14917 | 16.75 | 0.09 | 3.18 | 0.005 | 3.43 | 1.86 | 2.74 | 0.04 | 5.62 | 0.22 | 59.61 | 0.03 | 0.8 | 3.75 | 98.13 |
| 14925 | 17.48 | 0.04 | 4.83 | 0.005 | 6.57 | 1.8 | 3.11 | 0.05 | 4.16 | 0.25 | 54.26 | 0.04 | 0.88 | 4.77 | 98.25 |
| 14998 | 17.84 | 0.03 | 5.3 | 0.005 | 6.2 | 1.39 | 2.47 | 0.05 | 4.81 | 0.28 | 53.76 | 0.04 | 0.72 | 5.99 | 98.89 |
| 15862 | 17.45 | 0.03 | 5.66 | 0.005 | 6.02 | 1.73 | 2.74 | 0.07 | 4.12 | 0.26 | 52.87 | 0.03 | 0.68 | 7.2 | 98.87 |
| 15870 | 15.28 | 0.12 | 6.1 | 0.005 | 5.48 | 2.09 | 2.68 | 0.06 | 3.07 | 0.23 | 54.41 | 0.03 | 0.74 | 8.21 | 98.51 |
| 15879 | 17.04 | 0.09 | 6.38 | 0.005 | 7.37 | 1.69 | 2.84 | 0.06 | 3.81 | 0.25 | 50.72 | 0.04 | 0.9 | 7.09 | 98.29 |
| 15887 | 17.84 | 0.05 | 5.62 | 0.005 | 5.41 | 1.4 | 2.46 | 0.04 | 4.64 | 0.22 | 54.43 | 0.04 | 0.86 | 5.38 | 98.40 |

Project:
Client
Data:
Comments:

Schaft Creek
Copper Fox Metals Inc.
Whole Rock by XRF
Sampled by MDAG on Feb 7'07.

| Sample |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Id. | $\mathrm{Al}_{2} \mathrm{O}_{3}$ | BaO | $\mathrm{CaO}$ | $\mathrm{Cr}_{2} \mathrm{O}_{3}$ | $\mathrm{Fe}_{2} \mathrm{O}_{3}$ | $\mathrm{K}_{2} \mathrm{O}$ | $\mathrm{MgO}$ | MnO | $\mathrm{Na}_{2} \mathrm{O}$ | $\mathrm{P}_{2} \mathrm{O}_{5}$ | $\mathrm{SiO}_{2}$ | SrO | $\mathrm{TiO}_{2}$ | LOI | Total |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Method | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 | ME-XRF06 |
| MDL | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 |  |  |
| 15891 | 17.63 | 0.15 | 6.76 | 0.005 | 5.43 | 1.99 | 2.66 | 0.06 | 4.12 | 0.23 | 51.38 | 0.04 | 0.86 | 7.61 | 98.93 |
| 15908 | 17.38 | 0.03 | 6.09 | 0.005 | 4.92 | 2.09 | 2.86 | 0.05 | 3.44 | 0.23 | 53.48 | 0.03 | 0.81 | 7.13 | 98.55 |
| 15911 | 17.39 | 0.05 | 4.88 | 0.005 | 6.78 | 1.62 | 3.54 | 0.05 | 3.89 | 0.25 | 52.8 | 0.04 | 0.91 | 5.87 | 98.08 |
| Maximum | 19.9 | 0.15 | 7.5 | 0.01 | 9.45 | 3.94 | 6.3 | 0.19 | 5.76 | 0.36 | 66.9 | 0.08 | 1.38 | 11.1 |  |
| Minimum | 14.4 | 0.01 | 1.98 | 0.005 | 1.69 | 0.86 | 0.61 | 0.01 | 0.73 | 0.1 | 49 | 0.01 | 0.29 | 3.49 |  |
| Mean | 17.2 | 0.048 | 4.76 | 0.0053 | 5.54 | 1.89 | 2.69 | 0.057 | 3.91 | 0.24 | 55.5 | 0.035 | 0.7 | 6.02 |  |
| Standard Deviation | 1.37 | 0.033 | 1.19 | 0.0011 | 1.7 | 0.58 | 1.08 | 0.033 | 0.95 | 0.06 | 4.56 | 0.011 | 0.22 | 1.65 |  |
| 10 Percentile | 15.2 | 0.02 | 3.17 | 0.005 | 3.17 | 1.28 | 1.5 | 0.03 | 2.86 | 0.12 | 50.7 | 0.02 | 0.4 | 3.86 |  |
| 25 Percentile | 16.3 | 0.02 | 3.82 | 0.005 | 4.64 | 1.5 | 1.97 | 0.04 | 3.5 | 0.22 | 52.8 | 0.03 | 0.6 | 4.92 |  |
| Median | 17.4 | 0.04 | 4.93 | 0.005 | 5.63 | 1.84 | 2.62 | 0.05 | 4.03 | 0.25 | 54 | 0.04 | 0.7 | 5.91 |  |
| 75 Percentile | 17.9 | 0.06 | 5.59 | 0.005 | 6.56 | 2.12 | 3.2 | 0.06 | 4.45 | 0.28 | 57 | 0.04 | 0.82 | 7.11 |  |
| 90 Percentile | 19.1 | 0.092 | 6.13 | 0.005 | 7.44 | 2.52 | 3.99 | 0.082 | 4.99 | 0.3 | 63.9 | 0.04 | 0.91 | 8 |  |
| Interquartile Range (IQR) ${ }^{1}$ | 1.62 | 0.04 | 1.77 | 0 | 1.93 | 0.62 | 1.24 | 0.02 | 0.94 | 0.06 | 4.19 | 0.01 | 0.21 | 2.18 |  |
| Variance | 1.88 | 0.0011 | 1.43 | 1.2E-06 | 2.89 | 0.33 | 1.18 | 0.0011 | 0.9 | 0.0036 | 20.8 | 0.00012 | 0.047 | 2.72 |  |
| Skewness | -0.0061 | 1.24 | -0.16 | 4.2 | -0.21 | 1.03 | 1.01 | 2.22 | -0.92 | -0.99 | 1.15 | 1.02 | 0.6 | 0.79 |  |
| Coefficient of Variation (CoV) ${ }^{2}$ | 0.08 | 0.68 | 0.25 | 0.21 | 0.31 | 0.31 | 0.4 | 0.59 | 0.24 | 0.25 | 0.082 | 0.32 | 0.31 | 0.27 |  |
| Count | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 | 59 |  |

${ }^{1}$ Interquartile Range $(I Q R)=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) $=$ standard deviation divided by mean
NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.

Project:
Client:
Comments:

Schaft Creek
Copper Fox Metals Inc.
Calculated Mineralogy
Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Calculated | Calculated | Calculated | Calculated | Calculated | Calculated | Calculated |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S (Pyrite) | S (Chalcopyrite) | S (Arsenopyrite) | S (Galena) | S (Cinnibar) | S (Molybdenite) | S (Sphalerite) |
| $\mathrm{FeS}_{2}$ | $\mathrm{CuFeS}_{2}+\mathrm{CuS}_{2}$ | FeAsS +AsS | PbS | HgS | $\mathrm{MoS}_{2}$ | ZnS |

${ }_{(\%)}$
(\%)

| 0.632 | 0.130 |
| :--- | :--- |
| 0.400 | 0.176 |
| 1.211 | 0.194 |
| 0.090 | 0.134 |
| 0.340 | 0.264 |
| 0.151 | 0.248 |
| 0.612 | 0.131 |
| 1.293 | 0.137 |
| 0.181 | 0.122 |
| -0.021 | 0.266 |
| -0.275 | 0.559 |
| -0.105 | 0.344 |
| -0.190 | 0.291 |
| -0.059 | 0.211 |
| -0.018 | 0.103 |
| -0.106 | 0.386 |
| -0.207 | 0.340 |
| -0.157 | 0.320 |
| -0.166 | 0.493 |
| -0.018 | 0.151 |
| 0.195 | 0.235 |
| 0.066 | 0.246 |
| -0.095 | 0.227 |
| -0.099 | 0.351 |
| -0.111 | 0.613 |
| -0.058 | 0.495 |
| -0.122 | 0.177 |
| -0.136 | 0.267 |
| 0.053 | 0.401 |
| -0.235 | 0.329 |
| -0.113 | 0.302 |
| -0.226 | 0.399 |
| -0.047 | 0.392 |
| 0.216 | 0.201 |
| 0.479 | 0.204 |
| -0.066 | 0.152 |
| -0.069 | 0.212 |
| 0.161 | 0.145 |
| 1.352 | 0.437 |
| 1.467 | 0.462 |
| 0.039 | 0.122 |
| -0.032 | 0.270 |
| 0.471 | 0.551 |
| 1.516 | 0.301 |
| 1.575 | 0.331 |
| 0.053 | 0.071 |
| -0.094 | 0.165 |
| -0.026 | 0.041 |
| -0.054 | 0.115 |
| -0.221 | 0.384 |
| -0.041 | 0.163 |
| -0.068 | 0.182 |
| -0.058 | 0.119 |
| -0.108 | 0.204 |
| -0.126 | 0.217 |
| -0.231 | 0.512 |
| -0.153 | 0.247 |
| -0.245 | 0.430 |
|  |  |

0.00067
0.00081
$\begin{array}{ll}0.00081 & 0.000000160 \\ 0.00142 & 0.000\end{array}$

| 0.000000160 | 0.0024 | 0.0021 |
| :--- | :--- | :--- |
| 0.000000080 | 0.0232 | 0.0028 |
| 0.000000080 | 0.0439 | 0.0021 |
| 0.000000080 | 0.0216 | 0.0023 |
| 0.000000080 | 0.0147 | 0.0014 |
| 0.000000080 | 0.0060 | 0.0036 |
| 0.000000160 | 0.0037 | 0.0082 |
| 0.000000160 | 0.0009 | 0.0064 |
| 0.000000320 | 0.0005 | 0.0103 |
| 0.000000160 | 0.0154 | 0.0034 |
| 0.000000320 | 0.0054 | 0.0013 |
| 0.000000160 | 0.0048 | 0.0023 |
| 0.000000320 | 0.0171 | 0.0020 |
| 0.000000080 | 0.0052 | 0.0018 |
| 0.000000080 | 0.0319 | 0.0034 |
| 0.000000320 | 0.0118 | 0.0012 |
| 0.000000160 | 0.0065 | 0.0011 |
| 0.000000160 | 0.0249 | 0.0019 |
| 0.000000160 | 0.0115 | 0.0018 |
| 0.000000080 | 0.0015 | 0.0056 |
| 0.000000320 | 0.0008 | 0.0017 |
| 0.000000160 | 0.0143 | 0.0019 |
| 0.000000080 | 0.0045 | 0.0015 |
| 0.000000160 | 0.0068 | 0.0016 |
| 0.000000080 | 0.0167 | 0.0014 |
| 0.000000160 | 0.0114 | 0.0020 |
| 0.000000160 | 0.0141 | 0.0021 |
| 0.000000960 | 0.0387 | 0.0017 |
| 0.000000320 | 0.0035 | 0.0025 |
| 0.000000480 | 0.0122 | 0.0016 |
| 0.000000320 | 0.0085 | 0.0020 |
| 0.000000320 | 0.0333 | 0.0019 |
| 0.000000160 | 0.0160 | 0.0022 |
| 0.000000160 | 0.0006 | 0.0020 |
| 0.000000080 | 0.0056 | 0.0008 |
| 0.000000160 | 0.0427 | 0.0025 |
| 0.000000160 | 0.0441 | 0.0027 |
| 0.000000080 | 0.0019 | 0.0019 |
| 0.000000640 | 0.0080 | 0.0022 |
| 0.000000640 | 0.0052 | 0.0023 |
| 0.000000080 | 0.0009 | 0.0013 |
| 0.000000080 | 0.0008 | 0.0008 |
| 0.000000160 | 0.0067 | 0.0017 |
| 0.000000160 | 0.0018 | 0.0010 |
| 0.000000160 | 0.0021 | 0.0010 |
| 0.000000080 | 0.0036 | 0.0024 |
| 0.000000160 | 0.0067 | 0.0025 |
| 0.000000160 | 0.0013 | 0.0026 |
| 0.000000080 | 0.0068 | 0.0021 |
| 0.000000160 | 0.0011 | 0.0022 |
| 0.0000000160 | 0.0018 | 0.0026 |
| 0.000000160 | 0.0043 | 0.0021 |
| 0.000000160 | 0.0049 | 0.0025 |
| 0.000000080 | 0.0012 | 0.0027 |
| 0.000000160 | 0.0013 | 0.0032 |
| 0.000000160 | 0.0110 | 0.0021 |
| 0.000000160 | 0.0069 | 0.0026 |
| 0.000000480 | 0.0207 | 0.0022 |
|  |  |  |

## Project:

Client:
Comments:

## Sample

Id.

15911

Maximum
Minimu
Standard Deviation
10 Percentile
25 Percentile
25 Percen
Median
75 Percentile
90 Percentile
Interquartile Range (IQR) ${ }^{1}$
Variance
Skewness
Coefficient of Variation (CoV) ${ }^{2}$
Count

Schaft Creek
Copper Fox Metals Inc.
Calculated Mineralogy
Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Calculated S (Pyrite) | Calculated S (Chalcopyrite) | Calculated $S$ (Arsenopyrite) | Calculated <br> S (Galena) | Calculated <br> S (Cinnibar) | Calculated S (Molybdenite) | Calculated S (Sphalerite) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{FeS}_{2}$ | $\mathrm{CuFeS}_{2}+\mathrm{CuS}_{2}$ | FeAsS + AsS | Pbs | HgS | $\mathrm{MoS}_{2}$ | ZnS |
| (\%) | (\%) | (\%) | (\%) | (\%) | (\%) | (\%) |
| -0.122 | 0.184 | 0.00009 | 0.00004 | 0.000000320 | 0.0103 | 0.0025 |
| 1.58 | 0.61 | 0.0013 | 0.0037 | 0.00000096 | 0.044 | 0.01 |
| -0.28 | 0.041 | 0.0000043 | 0.000025 | 0.00000008 | 0.00046 | 0.0008 |
| 0.14 | 0.27 | 0.00022 | 0.00018 | 0.0000002 | 0.011 | 0.0024 |
| 0.48 | 0.13 | 0.00025 | 0.00051 | 0.00000016 | 0.012 | 0.0016 |
| -0.21 | 0.12 | 0.000071 | 0.000037 | 0.00000008 | 0.0011 | 0.0013 |
| -0.12 | 0.16 | 0.00009 | 0.00004 | 0.00000008 | 0.0023 | 0.0017 |
| -0.054 | 0.25 | 0.00013 | 0.000051 | 0.00000016 | 0.0067 | 0.0021 |
| 0.17 | 0.35 | 0.00022 | 0.000083 | 0.00000016 | 0.014 | 0.0024 |
| 0.75 | 0.47 | 0.0006 | 0.00031 | 0.00000032 | 0.026 | 0.0034 |
| 0.29 | 0.18 | 0.00013 | 0.000043 | 0.00000008 | 0.012 | 0.00075 |
| 0.23 | 0.018 | 0.000000061 | 0.00000026 | 2.7E-14 | 0.00013 | 0.0000026 |
| 1.99 | 0.68 | 2.61 | 5.92 | 2.59 | 1.63 | 3.21 |
| 3.39 | 0.5 | 1.13 | 2.84 | 0.81 | 1.07 | 0.67 |
| 59 | 59 | 59 | 59 | 59 | 59 | 59 |

Calculated S (Pyrite) (\%) =
\% S (Sulphide) + S (del) - S (Chalcopyrite) - S (Arsenopyrite) - S (Galena) - S (Cinnibar) - S (Molybdenite) - S (Spr Calculated S (Chalcopyrite) CuFeS2 + CuS2 (\%) = (1 / 0.99) * Copper (ppm) / 10000
Calculated S (Arsenopyrite) FeAsS + AsS (\%) = (1 / 2.33) * Iron (\%) / 10000
Calculated S (Galena) PbS (\%) $=(1 / 6.45) * \operatorname{Iron}(\mathrm{ppm}) / 10000$
Calculated $S($ Cinnibar $) \mathrm{HgS}(\%)=(1 / 6.25) *$ Gallium $(\mathrm{ppm}) / 10000$
Calculated S (Molybdenite) MoS2 $(\%)=(1 / 1.5)$ * Germanium (ppm) / 10000
Calculated S (Sphalerite) ZnS (\%) = (1/2) * Hafnium (ppm) / 10000

Project:
Data:
Comments:

Schaft Creek

Sample
Sam.
Id.

14018
14021
14036
14043
14060
14067
14076
14083
14099
14103
14130
14144
14148
14156
14162
14169
14232
14250
14260
14276
14295
14301
14323
14332
14345
14348
14797
14808
14816
14828
14844
14680
14871
14887
14689
14695
14742
14666
14685
$14685 B$
14545
14565
14571
14578
$14578 B$
14598
14893
14899
14908
14917
14925
14998
15862
15870
15879
15887
15891
15908

Whole Rock
\(\left.$$
\begin{array}{ccc}\begin{array}{c}\text { Whole Rock } \\
\text { Al }\end{array} & \begin{array}{c}\text { ICP } \\
\text { (ppm) }\end{array} & \begin{array}{c}\text { Al } \\
\text { (ppm) }\end{array}
$$ <br>
Difference <br>

(\%)^{3}\end{array}\right]\)| 85735 | 80300 | -6.34 |
| :---: | :---: | :---: |
| 78061 | 77000 | -1.36 |
| 79014 | 74100 | -6.22 |
| 80495 | 75600 | -6.08 |
| 80231 | 79600 | -0.79 |
| 85047 | 85100 | 0.06 |
| 85153 | 90000 | 5.69 |
| 86793 | 88500 | 1.97 |
| 80178 | 72400 | -9.70 |
| 79384 | 76000 | -4.26 |
| 90551 | 85100 | -6.02 |
| 96796 | 93900 | -2.99 |
| 89069 | 8100 | -8.95 |
| 81183 | 76900 | -5.28 |
| 75997 | 79700 | 4.87 |
| 82242 | 76400 | -7.10 |
| 103041 | 94400 | -8.39 |
| 95367 | 94400 | -1.01 |
| 94467 | 89500 | -5.26 |
| 104755 | 98400 | -5.91 |
| 92615 | 89700 | -3.15 |
| 93779 | 87600 | -6.59 |
| 100924 | 93600 | -7.26 |
| 104681 | 96200 | -8.10 |
| 103305 | 97300 | -5.81 |
| 105475 | 94300 | -10.59 |
| 96213 | 86900 | -9.68 |
| 82242 | 81300 | -1.15 |
| 90551 | 82900 | -8.45 |
| 90498 | 89200 | -1.43 |
| 93197 | 91800 | -1.50 |
| 92826 | 90500 | -2.51 |
| 98225 | 96200 | -2.06 |
| 93144 | 96900 | 4.03 |
| 83353 | 83800 | 0.54 |
| 95155 | 97000 | 1.94 |
| 97801 | 90600 | -7.36 |
| 92350 | 92100 | -0.27 |
| 87534 | 85900 | -1.87 |
| 87746 | 83100 | -5.29 |
| 98330 | 94700 | -3.69 |
| 91186 | 88300 | -3.16 |
| 87217 | 82200 | -5.75 |
| 88804 | 86800 | -2.26 |
| 86793 | 82400 | -5.06 |
| 101506 | 92500 | -8.87 |
| 92033 | 92000 | -0.04 |
| 96531 | 97000 | 0.49 |
| 92985 | 95800 | 3.03 |
| 88646 | 85300 | -3.77 |
| 92509 | 87800 | -5.09 |
| 94414 | 90100 | -4.57 |
| 92350 | 87200 | -5.58 |
| 80866 | 81000 | 0.17 |
| 90180 | 90600 | 0.47 |
| 94414 | 87200 | -7.64 |
| 93303 | 89500 | -4.08 |
| 91980 | 87100 | -5.31 |
|  |  |  |

Whole Rock ICP
Ba * (ppm)
1164
448

1164
448
537
269
358
358
448
717
896
269
537
358
627
269
537
90
179
179
179
1075
90
269
269
179
179
179
179
179
179
717
358
269
90
358
90
179
179
358
448
358
896
179
448
627
806
179
448
358
717
806
358
269
269
107
806
4
13
273
-

| Whole Rock <br> Ca <br> (ppm) | ICP <br> Ca <br> (ppm) |
| :---: | :---: |
| 18082 | 17800 |
| 25443 | 26200 |
| 18296 | 18400 |
| 14151 | 14000 |
| 30517 | 31400 |
| 25300 | 25900 |
| 40094 | 43400 |
| 38093 | 40300 |
| 29731 | 29500 |
| 28802 | 29300 |
| 25657 | 26200 |
| 35377 | 37500 |
| 44740 | 46300 |
| 23513 | 24700 |
| 53602 | 55900 |
| 22513 | 23200 |
| 26229 | 26600 |
| 39094 | 40700 |
| 29874 | 30400 |
| 41952 | 43100 |
| 37307 | 39100 |
| 35234 | 36700 |
| 35878 | 37500 |
| 33376 | 33900 |
| 24585 | 25500 |
| 22084 | 21500 |
| 36592 | 37800 |
| 47456 | 48700 |
| 32590 | 33300 |
| 40738 | 43400 |
| 27158 | 28200 |
| 39594 | 41400 |
| 33019 | 34000 |
| 47956 | 51800 |
| 19368 | 21800 |
| 35592 | 39800 |
| 27444 | 27800 |
| 37164 | 39300 |
| 32090 | 33100 |
| 29731 | 29500 |
| 37021 | 38200 |
| 43239 | 45800 |
| 25086 | 25900 |
| 39808 | 42000 |
| 41095 | 43200 |
| 32304 | 33500 |
| 39808 | 41600 |
| 34091 | 35400 |
| 35663 | 37900 |
| 22727 | 23200 |
| 34520 | 36000 |
| 37879 | 39800 |
| 40452 | 42200 |
| 43596 | 46400 |
| 45597 | 48300 |
| 40166 | 41200 |
| 48313 | 51300 |
| 43525 | 45200 |

Differ

Whole Rock ICP

[^1]Whole Ro
Fe *
$\stackrel{\mathrm{CP}}{\mathrm{Fe}}$
Difference
$(\%)^{3}$

| 34 | 24 |
| :---: | :---: |
| 34 | 21 |
| 34 | 20 |
| 34 | 31 |
| 34 | 26 |
| 68 | 36 |
| 34 | 33 |
| 34 | 49 |
| 34 | 16 |
| 34 | 20 |
| 34 | 15 |
| 34 | 5 |
| 34 | 4 |
| 34 | 25 |
| 68 | 71 |
| 34 | 16 |
| 34 | 14 |
| 34 | 12 |
| 34 | 3 |
| 34 | 17 |
| 34 | 12 |
| 34 | 15 |
| 34 | 3 |
| 34 | 3 |
| 34 | 11 |
| 34 | 11 |
| 34 | 6 |
| 34 | 6 |
| 34 | 5 |
| 34 | 4 |
| 34 | 39 |
| 68 | 5 |
| 34 | 10 |
| 34 | 20 |
| 34 | 10 |
| 34 | 6 |
| 34 | 24 |
| 34 | 21 |
| 34 | 5 |
| 34 | 7 |
| 34 | 16 |
| 34 | 11 |
| 34 | 7 |
| 34 | 9 |
| 34 | 10 |
| 34 | 3 |
| 34 | 44 |
| 34 | 43 |
| 34 | 39 |
| 34 | 16 |
| 34 | 30 |
| 34 | 6 |
| 34 | 4 |
| 34 | 27 |
| 34 | 29 |
| 34 | 25 |
| 34 | 22 |
| 34 | 24 |
|  |  |


| -29.85 <br> -38.62 <br> -41.54 <br> -9.38 <br> -24.00 <br> -47.38 <br> -3.54 <br> 43.23 <br> -53.23 <br> -41.54 <br> -56.15 <br> -85.38 <br> -88.31 <br> -26.92 <br> 3.77 <br> -53.23 <br> -59.08 <br> -64.92 <br> -91.23 <br> -50.31 <br> -64.92 <br> -56.15 <br> -91.23 <br> -91.23 <br> -67.85 <br> -67.85 <br> -82.46 <br> -82.46 <br> -85.38 <br> -88.31 <br> 14.00 <br> -92.69 <br> -70.77 <br> -41.54 <br> -70.77 <br> -82.46 <br> -29.85 <br> -38.62 <br> -85.38 <br> -79.54 <br> -53.23 <br> -67.85 <br> -79.54 <br> -73.69 <br> -70.77 <br> -91.23 <br> 28.62 <br> 25.69 <br> 14.00 <br> -53.23 <br> -12.31 <br> -82.46 <br> -88.31 <br> -21.08 <br> -15.23 <br> -26.92 <br> -35.69 <br> -29.85 |
| :--- |


| 26369 | 25800 | -2.16 |
| :--- | :--- | :--- |
| 18325 | 18100 | -1.23 |
| 26019 | 25600 | -1.61 |
| 29586 | 28500 | -3.67 |
| 35951 | 35900 | -0.14 |
| 43225 | 42900 | -0.75 |
| 51968 | 54600 | 5.06 |
| 57773 | 57800 | 0.05 |
| 23641 | 22300 | -5.67 |
| 21752 | 21200 | -2.54 |
| 18185 | 18000 | -1.02 |
| 35322 | 36100 | 2.20 |
| 39378 | 38300 | -2.74 |
| 17206 | 17400 | 1.13 |
| 41407 | 42500 | 2.64 |
| 11820 | 11800 | -0.17 |
| 26998 | 26400 | -2.22 |
| 46093 | 45800 | -0.64 |
| 43575 | 42300 | -2.93 |
| 39168 | 38900 | -0.69 |
| 47632 | 47300 | -0.70 |
| 31265 | 31300 | 0.11 |
| 38749 | 38700 | -0.13 |
| 36301 | 35500 | -2.21 |
| 22242 | 22100 | -0.64 |
| 35811 | 34700 | -3.10 |
| 43365 | 42700 | -1.53 |
| 38049 | 37600 | -1.18 |
| 42386 | 41300 | -2.56 |
| 40218 | 41200 | 2.44 |
| 51758 | 51800 | 0.08 |
| 44134 | 41400 | -6.20 |
| 45813 | 46100 | 0.63 |
| 51129 | 53100 | 3.86 |
| 13709 | 14800 | 7.96 |
| 36301 | 39900 | 9.92 |
| 33573 | 33500 | -0.22 |
| 51618 | 53900 | 4.42 |
| 62390 | 63900 | 2.42 |
| 66097 | 59700 | -9.68 |
| 41826 | 41700 | -0.30 |
| 36720 | 37200 | 1.31 |
| 27908 | 26900 | -3.61 |
| 39938 | 41600 | 4.16 |
| 41616 | 39200 | -5.81 |
| 45463 | 46600 | 2.50 |
| 53087 | 53400 | 0.59 |
| 56934 | 56900 | -0.06 |
| 52388 | 53200 | 1.55 |
| 23991 | 24200 | 0.87 |
| 45933 | 46200 | 0.54 |
| 43365 | 43600 | 0.54 |
| 42106 | 41600 | -1.20 |
| 38329 | 39200 | 2.27 |
| 51548 | 51500 | -0.09 |
| 37840 | 34600 | -8.56 |
| 37979 | 38500 | 1.37 |
| 34412 | 34500 | 0.25 |
|  |  |  |

Project:
Client
Comments:

Schaft Creek
Copper Fox Metals Inc.
QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses
Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Sample Id. | Whole Rock Al * (ppm) | $\begin{aligned} & \text { ICP } \\ & \text { AI } \\ & \text { (ppm) } \end{aligned}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock $B a$ * (ppm) | $\begin{gathered} \text { ICP } \\ \text { Ba } \\ (\mathrm{ppm}) \end{gathered}$ | Difference $(\%)^{3}$ | Whole Rock Ca* (ppm) | $\begin{gathered} \text { ICP } \\ \text { Ca } \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock Cr * (ppm) | $\begin{gathered} \text { ICP } \\ \text { Cr } \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock Fe * (ppm) | $\begin{aligned} & \text { ICP } \\ & \mathrm{Fe} \\ & (\mathrm{ppm}) \end{aligned}$ | Difference <br> (\%) ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15911 | 92033 | 88600 | -3.73 | 448 | 410 | -8.45 | 34877 | 35200 | 0.93 | 34 | 33 | -3.54 | 47422 | 46500 | -1.94 |
| Maximum |  |  | 5.69 |  |  | 34 |  |  | 12.6 |  |  | 43.2 |  |  | 9.92 |
| Minimum |  |  | -10.6 |  |  | -33 |  |  | -2.64 |  |  | -92.7 |  |  | -9.68 |
| Mean |  |  | -3.63 |  |  | -1.63 |  |  | 3.76 |  |  | -49.3 |  |  | -0.32 |
| Standard Deviation |  |  | 3.81 |  |  | 13 |  |  | 2.74 |  |  | 35 |  |  | 3.33 |
| 10 Percentile |  |  | -8.4 |  |  | -16.3 |  |  | 0.85 |  |  | -88.3 |  |  | -3.62 |
| 25 Percentile |  |  | -6.15 |  |  | -8.04 |  |  | 2.27 |  |  | -81 |  |  | -2.05 |
| Median |  |  | -4.08 |  |  | -4.17 |  |  | 3.72 |  |  | -53.2 |  |  | -0.17 |
| 75 Percentile |  |  | -1.08 |  |  | 5.14 |  |  | 5.1 |  |  | -28.4 |  |  | 1.22 |
| 90 Percentile |  |  | 0.82 |  |  | 12.8 |  |  | 6.3 |  |  | -2.08 |  |  | 2.88 |
| Interquartile Range (IQR) ${ }^{1}$ |  |  | 5.07 |  |  | 13.2 |  |  | 2.82 |  |  | 52.6 |  |  | 3.27 |
| Variance |  |  | 14.5 |  |  | 169 |  |  | 7.52 |  |  | 1223 |  |  | 11.1 |
| Skewness |  |  | 0.41 |  |  | 0.66 |  |  | 0.57 |  |  | 0.76 |  |  | 0.066 |
| Coefficient of Variation (CoV) ${ }^{2}$ |  |  | -1.05 |  |  | -7.96 |  |  | 0.73 |  |  | -0.71 |  |  | -10.3 |
| Count |  |  | 59 |  |  | 59 |  |  | 59 |  |  | 59 |  |  | 59 |

${ }^{1}$ Interquartile Range $(\mathrm{IQR})=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) = standard deviation divided by mean
${ }^{3}$ Difference (\%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

Al (Whole Rock) $=\left(\mathrm{Al}_{2} \mathrm{O}_{3}{ }^{\star} 2 \star 10000 \star 26.98\right) /(2 \star 26.98+3 \star 16)$ $\mathrm{Ba}($ Whole Rock $)=(\mathrm{BaO} * 10000 * 137.34) /(137.34+16)$ Ca (Whole Rock) $=\left(\mathrm{CaO}^{*} 10000 * 40.08\right) /(40.08+16)$
Cr (Whole Rock) $=\left(\mathrm{Cr}_{2} \mathrm{O}_{3}{ }^{*} 2^{*} 10000 * 52.00\right) /(2 * 52.00+3 * 16)$
$\mathrm{Fe}($ Whole Rock $)=\left(\mathrm{Fe}_{2} \mathrm{O}_{3}{ }^{*}{ }^{\star} 10000 * 55.85\right) /\left(2 \star 55.85+3^{*} 16\right)$

Project:
Data:
Comments:

Schaft Creek
Copper Fox Metals Inc.
QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses
Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Sample <br> Id. | Whole Rock K * (ppm) | $\begin{gathered} \text { ICP } \\ \text { K } \\ (\mathrm{ppm}) \end{gathered}$ | Difference $(\%)^{3}$ | Whole Rock Mg * (ppm) | ICP <br> Mg <br> (ppm) | Difference <br> $(\%)^{3}$ | Whole Rock Mn * (ppm) | $\begin{aligned} & \text { ICP } \\ & \text { Mn } \\ & (\mathrm{ppm}) \end{aligned}$ | Difference $(\%)^{3}$ | Whole Rock Na * (ppm) | $\begin{gathered} \text { ICP } \\ \mathrm{Na} \\ \text { (ppm) } \end{gathered}$ | Difference $(\%)^{3}$ | Whole Rock P* (ppm) | $\begin{aligned} & \text { ICP } \\ & \text { P } \\ & (\mathrm{ppm}) \end{aligned}$ | Difference <br> $(\%)^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14018 | 24239 | 24500 | 1.08 | 10494 | 10700 | 1.97 | 387 | 476 | 22.92 | 29748 | 31600 | 6.22 | 611 | 660 | 8.03 |
| 14021 | 21500 | 22200 | 3.26 | 8865 | 9200 | 3.78 | 542 | 629 | 16.03 | 21959 | 23800 | 8.38 | 524 | 570 | 8.85 |
| 14036 | 20836 | 21300 | 2.23 | 9106 | 9100 | -0.07 | 387 | 475 | 22.67 | 23220 | 24700 | 6.37 | 524 | 570 | 8.85 |
| 14043 | 9795 | 10300 | 5.15 | 18454 | 19000 | 2.96 | 387 | 446 | 15.18 | 30638 | 32900 | 7.38 | 524 | 570 | 8.85 |
| 14060 | 11788 | 12000 | 1.80 | 19781 | 21000 | 6.16 | 387 | 422 | 8.98 | 27523 | 30500 | 10.82 | 1135 | 1290 | 13.70 |
| 14067 | 10708 | 11200 | 4.59 | 24545 | 26800 | 9.19 | 697 | 779 | 11.76 | 30787 | 35100 | 14.01 | 960 | 1120 | 16.66 |
| 14076 | 13116 | 14300 | 9.03 | 22434 | 25000 | 11.44 | 1471 | 1585 | 7.72 | 19585 | 23000 | 17.44 | 916 | 1070 | 16.76 |
| 14083 | 28971 | 30900 | 6.66 | 17007 | 17700 | 4.08 | 1317 | 1365 | 3.68 | 12018 | 13600 | 13.16 | 916 | 1070 | 16.76 |
| 14099 | 32706 | 32000 | -2.16 | 8865 | 8200 | -7.50 | 1084 | 1090 | 0.53 | 5416 | 5400 | -0.29 | 480 | 470 | -2.09 |
| 14103 | 17183 | 18100 | 5.33 | 12303 | 12900 | 4.85 | 620 | 686 | 10.72 | 22181 | 25100 | 13.16 | 567 | 620 | 9.29 |
| 14130 | 17515 | 18100 | 3.34 | 9710 | 10200 | 5.05 | 155 | 191 | 23.31 | 34199 | 38300 | 11.99 | 1222 | 1390 | 13.76 |
| 14144 | 15274 | 15600 | 2.13 | 10916 | 11600 | 6.27 | 387 | 451 | 16.47 | 30045 | 34900 | 16.16 | 1571 | 1830 | 16.49 |
| 14148 | 20670 | 20600 | -0.34 | 18876 | 18900 | 0.13 | 387 | 429 | 10.79 | 12760 | 13800 | 8.15 | 1135 | 1220 | 7.53 |
| 14156 | 11705 | 12200 | 4.23 | 7297 | 7900 | 8.26 | 232 | 339 | 45.91 | 33606 | 37400 | 11.29 | 436 | 500 | 14.58 |
| 14162 | 14859 | 16000 | 7.68 | 23942 | 26200 | 9.43 | 774 | 853 | 10.14 | 16840 | 19300 | 14.61 | 873 | 980 | 12.29 |
| 14169 | 8882 | 9700 | 9.21 | 3679 | 4000 | 8.73 | 232 | 278 | 19.65 | 42731 | 47600 | 11.40 | 524 | 550 | 5.03 |
| 14232 | 16685 | 16800 | 0.69 | 8926 | 9100 | 1.95 | 155 | 189 | 22.02 | 39392 | 42800 | 8.65 | 1309 | 1430 | 9.23 |
| 14250 | 13863 | 14600 | 5.32 | 17308 | 18800 | 8.62 | 387 | 436 | 12.59 | 33235 | 38300 | 15.24 | 1222 | 1450 | 18.67 |
| 14260 | 15772 | 15900 | 0.81 | 13328 | 13900 | 4.29 | 232 | 275 | 18.36 | 35386 | 38600 | 9.08 | 1222 | 1390 | 13.76 |
| 14276 | 7139 | 7600 | 6.46 | 15439 | 16400 | 6.23 | 1084 | 1085 | 0.07 | 36870 | 40800 | 10.66 | 1266 | 1440 | 13.79 |
| 14295 | 15191 | 16000 | 5.33 | 14655 | 15500 | 5.77 | 387 | 436 | 12.59 | 29674 | 33600 | 13.23 | 1178 | 1360 | 15.43 |
| 14301 | 19425 | 19200 | -1.16 | 12062 | 12400 | 2.81 | 465 | 517 | 11.26 | 24704 | 27300 | 10.51 | 1222 | 1380 | 12.94 |
| 14323 | 17432 | 18200 | 4.40 | 9348 | 9600 | 2.70 | 310 | 386 | 24.60 | 30935 | 35000 | 13.14 | 1222 | 1410 | 15.40 |
| 14332 | 20421 | 20200 | -1.08 | 10313 | 10400 | 0.85 | 232 | 281 | 20.94 | 29897 | 32400 | 8.37 | 1309 | 1470 | 12.29 |
| 14345 | 22662 | 24000 | 5.90 | 9890 | 10300 | 4.14 | 77 | 150 | 93.68 | 33161 | 36900 | 11.28 | 1222 | 1380 | 12.94 |
| 14348 | 18678 | 18700 | 0.12 | 11881 | 12100 | 1.85 | 155 | 191 | 23.31 | 35535 | 38200 | 7.50 | 1353 | 1520 | 12.36 |
| 14797 | 18927 | 19500 | 3.03 | 14836 | 15200 | 2.46 | 465 | 559 | 20.30 | 23888 | 26700 | 11.77 | 1178 | 1330 | 12.88 |
| 14808 | 20670 | 20800 | 0.63 | 15801 | 16300 | 3.16 | 465 | 493 | 6.10 | 18546 | 20000 | 7.84 | 1004 | 1080 | 7.60 |
| 14816 | 20753 | 20900 | 0.71 | 16766 | 17000 | 1.40 | 387 | 438 | 13.11 | 24110 | 26700 | 10.74 | 1135 | 1230 | 8.41 |
| 14828 | 16104 | 17500 | 8.67 | 16464 | 18200 | 10.54 | 465 | 507 | 9.11 | 28265 | 32900 | 16.40 | 1091 | 1280 | 17.33 |
| 14844 | 16436 | 16900 | 2.82 | 35823 | 37900 | 5.80 | 232 | 319 | 37.30 | 21662 | 24600 | 13.56 | 1135 | 1290 | 13.70 |
| 14680 | 15025 | 16000 | 6.49 | 15077 | 16500 | 9.44 | 465 | 493 | 6.10 | 30045 | 34600 | 15.16 | 1135 | 1300 | 14.58 |
| 14871 | 11290 | 12300 | 8.95 | 17308 | 19200 | 10.93 | 310 | 374 | 20.73 | 38280 | 44300 | 15.73 | 1047 | 1230 | 17.44 |
| 14887 | 10293 | 11700 | 13.67 | 21771 | 24700 | 13.45 | 542 | 613 | 13.07 | 30045 | 35400 | 17.82 | 1004 | 1200 | 19.56 |
| 14689 | 15855 | 16400 | 3.44 | 5488 | 5600 | 2.04 | 232 | 301 | 29.55 | 32196 | 34300 | 6.53 | 480 | 540 | 12.50 |
| 14695 | 21334 | 22100 | 3.59 | 14534 | 15100 | 3.89 | 542 | 611 | 12.71 | 26484 | 30000 | 13.28 | 1135 | 1400 | 23.39 |
| 14742 | 12369 | 12800 | 3.49 | 20444 | 22400 | 9.57 | 310 | 401 | 29.45 | 38651 | 43600 | 12.81 | 1091 | 1220 | 11.83 |
| 14666 | 12701 | 12900 | 1.57 | 21650 | 22000 | 1.61 | 465 | 543 | 16.86 | 32864 | 35800 | 8.93 | 1091 | 1250 | 14.58 |
| 14685 | 12203 | 12100 | -0.84 | 27199 | 27300 | 0.37 | 310 | 364 | 17.50 | 29897 | 32000 | 7.04 | 1353 | 1530 | 13.10 |
| 14685B | 12784 | 13200 | 3.26 | 26354 | 28400 | 7.76 | 310 | 327 | 5.56 | 29526 | 33900 | 14.82 | 1309 | 1530 | 16.87 |
| 14545 | 11373 | 11800 | 3.76 | 13087 | 14000 | 6.98 | 232 | 273 | 17.50 | 31158 | 35000 | 12.33 | 1178 | 1330 | 12.88 |
| 14565 | 17764 | 18600 | 4.70 | 11398 | 12100 | 6.16 | 465 | 529 | 13.84 | 26484 | 29900 | 12.90 | 1135 | 1270 | 11.93 |
| 14571 | 14610 | 14200 | -2.81 | 12242 | 11700 | -4.43 | 155 | 230 | 48.49 | 32048 | 32200 | 0.47 | 960 | 1030 | 7.29 |
| 14578 | 15689 | 15800 | 0.71 | 12001 | 11800 | -1.68 | 310 | 337 | 8.79 | 29674 | 31500 | 6.15 | 1353 | 1550 | 14.58 |
| 14578B | 15274 | 15800 | 3.44 | 11881 | 12700 | 6.90 | 310 | 345 | 11.37 | 29006 | 32900 | 13.42 | 1309 | 1470 | 12.29 |
| 14598 | 12784 | 12400 | -3.00 | 22857 | 22100 | -3.31 | 542 | 631 | 16.39 | 29303 | 31400 | 7.16 | 1353 | 1540 | 13.84 |
| 14893 | 9214 | 10200 | 10.70 | 24545 | 27200 | 10.82 | 465 | 493 | 6.10 | 31380 | 36600 | 16.63 | 1091 | 1260 | 15.50 |
| 14899 | 7471 | 7700 | 3.07 | 37994 | 41300 | 8.70 | 465 | 546 | 17.50 | 29229 | 34100 | 16.67 | 1091 | 1260 | 15.50 |
| 14908 | 12535 | 13700 | 9.30 | 21470 | 24000 | 11.79 | 465 | 527 | 13.41 | 37760 | 44700 | 18.38 | 1135 | 1310 | 15.46 |
| 14917 | 15440 | 16100 | 4.27 | 16524 | 18300 | 10.75 | 310 | 379 | 22.34 | 41692 | 47300 | 13.45 | 960 | 1100 | 14.58 |
| 14925 | 14942 | 15400 | 3.07 | 18756 | 20400 | 8.77 | 387 | 408 | 5.36 | 30861 | 35600 | 15.36 | 1091 | 1230 | 12.75 |
| 14998 | 11539 | 12500 | 8.33 | 14896 | 16300 | 9.43 | 387 | 452 | 16.73 | 35683 | 41400 | 16.02 | 1222 | 1440 | 17.85 |
| 15862 | 14361 | 14800 | 3.06 | 16524 | 17400 | 5.30 | 542 | 584 | 7.73 | 30564 | 34400 | 12.55 | 1135 | 1260 | 11.05 |
| 15870 | 17349 | 18500 | 6.63 | 16162 | 17700 | 9.51 | 465 | 539 | 16.00 | 22775 | 26200 | 15.04 | 1004 | 1120 | 11.59 |
| 15879 | 14029 | 14900 | 6.21 | 17127 | 18800 | 9.77 | 465 | 554 | 19.22 | 28265 | 32900 | 16.40 | 1091 | 1280 | 17.33 |
| 15887 | 11622 | 11900 | 2.40 | 14836 | 15900 | 7.17 | 310 | 395 | 27.51 | 34422 | 39300 | 14.17 | 960 | 1090 | 13.54 |
| 15891 | 16519 | 17200 | 4.12 | 16042 | 17300 | 7.84 | 465 | 558 | 20.08 | 30564 | 34900 | 14.19 | 1004 | 1120 | 11.59 |
| 15908 | 17349 | 18000 | 3.75 | 17248 | 18500 | 7.26 | 387 | 433 | 11.82 | 25520 | 29000 | 13.64 | 1004 | 1130 | 12.59 |

Comments:

## Sample

Id.

15911
Maximum
Minimum
Mean
Standard Deviation
10 Percentile
25 Percentile
25 Percentile
5 Percen
75 Percentile

Interquartile Range (IQR) ${ }^{1}$
Variance

Coefficient of Variation (CoV) ${ }^{2}$
Count

Schaft Creek
Copper Fox Metals Inc.
QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses
Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Whole Rock K * (ppm) | $\begin{gathered} \text { ICP } \\ \text { K } \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> $(\%)^{3}$ | Whole Rock Mg * (ppm) | $\begin{gathered} \mathrm{ICP} \\ \mathrm{Mg} \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock Mn * (ppm) | $\begin{gathered} \mathrm{ICP} \\ \mathrm{Mn} \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 13448 | 13800 | 2.62 | 21349 | 23100 | 8.20 | 387 | 402 | 3.81 |
|  |  | 13.7 |  |  | 13.5 |  |  | 93.7 |
|  |  | -3 |  |  | -7.5 |  |  | 0.07 |
|  |  | 3.79 |  |  | 5.46 |  |  | 17.4 |
|  |  | 3.41 |  |  | 4.3 |  |  | 13.8 |
|  |  | -0.44 |  |  | 0.32 |  |  | 5.99 |
|  |  | 1.69 |  |  | 2.58 |  |  | 10.4 |
|  |  | 3.44 |  |  | 6.16 |  |  | 16 |
|  |  | 5.62 |  |  | 8.75 |  |  | 20.8 |
|  |  | 8.72 |  |  | 10.6 |  |  | 27.9 |
|  |  | 3.93 |  |  | 6.17 |  |  | 10.4 |
|  |  | 11.6 |  |  | 18.5 |  |  | 192 |
|  |  | 0.37 |  |  | -0.65 |  |  | 3.24 |
|  |  | 0.9 |  |  | 0.79 |  |  | 0.8 |
|  |  | 59 |  |  | 59 |  |  | 59 |


| Whole Rock <br> $\mathrm{Na}{ }^{*}$ <br> $(\mathrm{ppm})$ | ICP <br> Na <br> $(\mathrm{ppm})$ | Difference <br> $(\%)^{3}$ |
| :---: | :---: | :---: |
| 28858 | 32500 | 12.62 |
|  |  | 18.4 |
|  |  | -0.29 |
|  |  | 11.8 |
|  |  | 3.98 |
|  |  | 6.94 |
|  |  | 8.79 |
|  |  | 12.8 |
|  |  | 14.7 |
|  |  |  |
|  |  | 5.92 |
|  |  | 15.8 |
|  |  | -0.85 |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |


| Whole Rock <br> $\mathrm{P}^{\star}$ <br> $(\mathrm{ppm})$ | ICP <br> P | Difference <br> $(\mathrm{ppm})$ |
| :---: | :---: | :---: |
| $(\%)^{3}$ |  |  |
| 1091 | 1250 | 14.58 |
|  |  |  |
|  |  | 23.4 |
|  |  | -2.09 |
|  |  | 13.1 |
|  |  |  |
|  |  | 8.94 |
|  |  | 11.7 |
|  |  | 13.5 |
|  |  | 17.4 |
|  |  | 17.3 |
|  |  | 3.73 |
|  |  | 15.6 |
|  |  | -0.86 |
|  |  | 0.3 |
|  |  |  |

${ }^{1}$ Interquartile Range $(I Q R)=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) = standard deviation divided by mean
${ }^{3}$ Difference (\%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis

K (Whole Rock) $=\left(\mathrm{K}_{2} \mathrm{O} * 2 * 10000 * 39.09\right) /(39.09 * 2+16)$
Mg (Whole Rock) $=\left(\mathrm{MgO}^{*} 10000 * 24.31\right) /(24.31+16)$
Mn (Whole Rock) $=\left(\mathrm{MnO}^{*} 10000 * 54.94\right) /(54.94+16)$
Na (Whole Rock) $=\left(\mathrm{Na}_{2} \mathrm{O} * 2 * 10000 * 22.99\right) /(22.99 * 2+16)$
P (Whole Rock) $=\left(\mathrm{P}_{2} \mathrm{O} 5^{*} 2^{*} 10000 * 30.97\right) /(2 * 30.97+5 * 16)$

Project
Client
Comments:

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Sampled by MDAG on Feb 7'07.
For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Sample <br> Id. | Whole Rock Si * (ppm) | $\begin{gathered} \text { ICP } \\ \text { Si } \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock Sr * (ppm) | $\begin{gathered} \text { ICP } \\ \mathrm{Sr} \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | $\begin{gathered} \text { Leco } \\ \mathrm{S}(\mathrm{Total})^{\star \star} \\ (\mathrm{ppm}) \end{gathered}$ | $\begin{gathered} \text { ICP } \\ \mathrm{S} \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock <br> Ti * <br> (ppm) | $\begin{gathered} \text { ICP } \\ \text { Ti } \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14018 | 294129 |  |  | 423 | 428 | 1.23 | 8000 | 8800 | 10.00 | 2518 | 2400 | -4.68 |
| 14021 | 303993 |  |  | 169 | 173 | 2.30 | 6200 | 7000 | 12.90 | 2158 | 2080 | -3.62 |
| 14036 | 303338 |  |  | 254 | 235 | -7.36 | 14700 | 16000 | 8.84 | 2278 | 1970 | -13.52 |
| 14043 | 302637 |  |  | 254 | 276 | 8.80 | 2600 | 2800 | 7.69 | 2458 | 2190 | -10.90 |
| 14060 | 271971 |  |  | 423 | 423 | 0.05 | 13100 | 14800 | 12.98 | 4376 | 4100 | -6.31 |
| 14067 | 269681 |  |  | 338 | 410 | 21.22 | 4000 | 4300 | 7.50 | 4196 | 4170 | -0.63 |
| 14076 | 259724 |  |  | 338 | 365 | 7.91 | 7700 | 9500 | 23.38 | 4316 | 4540 | 5.18 |
| 14083 | 249346 |  |  | 169 | 232 | 37.18 | 14600 | 16000 | 9.59 | 4436 | 4480 | 0.99 |
| 14099 | 297822 |  |  | 85 | 88 | 4.07 | 3400 | 3600 | 5.88 | 1858 | 1670 | -10.14 |
| 14103 | 287725 |  |  | 169 | 198 | 16.78 | 6900 | 7700 | 11.59 | 2458 | 2220 | -9.68 |
| 14130 | 281180 |  |  | 254 | 288 | 13.53 | 2900 | 3200 | 10.34 | 3177 | 2800 | -11.88 |
| 14144 | 251496 |  |  | 338 | 343 | 1.41 | 2600 | 2800 | 7.69 | 3777 | 3760 | -0.45 |
| 14148 | 243082 |  |  | 254 | 223 | -12.09 | 1400 | 1400 | 0.00 | 3837 | 3780 | -1.48 |
| 14156 | 303666 |  |  | 254 | 259 | 2.10 | 1700 | 1700 | 0.00 | 1739 | 1900 | 9.29 |
| 14162 | 234714 |  |  | 169 | 239 | 41.32 | 1300 | 1500 | 15.38 | 4137 | 4270 | 3.23 |
| 14169 | 312781 |  |  | 169 | 207 | 22.40 | 3000 | 3200 | 6.67 | 1858 | 1960 | 5.46 |
| 14232 | 264352 |  |  | 338 | 345 | 2.00 | 1500 | 1600 | 6.67 | 3657 | 3290 | -10.03 |
| 14250 | 242661 |  |  | 338 | 424 | 25.36 | 1900 | 2000 | 5.26 | 4496 | 4350 | -3.25 |
| 14260 | 255330 |  |  | 338 | 402 | 18.85 | 3400 | 3700 | 8.82 | 4316 | 4050 | -6.17 |
| 14276 | 252759 |  |  | 676 | 798 | 17.97 | 1700 | 1700 | 0.00 | 4017 | 4100 | 2.08 |
| 14295 | 250234 |  |  | 254 | 336 | 32.45 | 4400 | 4900 | 11.36 | 4376 | 4240 | -3.12 |
| 14301 | 256452 |  |  | 169 | 209 | 23.58 | 3400 | 3500 | 2.94 | 4196 | 3620 | -13.74 |
| 14323 | 255470 |  |  | 338 | 391 | 15.60 | 1500 | 1500 | 0.00 | 3357 | 3310 | -1.41 |
| 14332 | 253179 |  |  | 338 | 355 | 4.96 | 2600 | 2700 | 3.85 | 3597 | 3260 | -9.37 |
| 14345 | 268793 |  |  | 254 | 274 | 8.01 | 5200 | 5600 | 7.69 | 3477 | 2970 | -14.58 |
| 14348 | 256966 |  |  | 254 | 276 | 8.80 | 4400 | 4800 | 9.09 | 3657 | 3190 | -12.77 |
| 14797 | 241867 |  |  | 254 | 234 | -7.76 | 800 | 700 | -12.50 | 4196 | 4150 | -1.11 |
| 14808 | 245980 |  |  | 169 | 221 | 30.68 | 1800 | 1900 | 5.56 | 3357 | 3260 | -2.90 |
| 14816 | 249346 |  |  | 254 | 285 | 12.35 | 4600 | 4700 | 2.17 | 3897 | 3810 | -2.23 |
| 14828 | 242474 |  |  | 338 | 404 | 19.44 | 1300 | 1400 | 7.69 | 3777 | 3940 | 4.32 |
| 14844 | 246775 |  |  | 254 | 265 | 4.46 | 2100 | 2200 | 4.76 | 5575 | 5590 | 0.26 |
| 14680 | 249346 |  |  | 338 | 348 | 2.89 | 2200 | 2200 | 0.00 | 4017 | 4040 | 0.58 |
| 14871 | 250234 |  |  | 338 | 405 | 19.74 | 3700 | 3800 | 2.70 | 4916 | 4990 | 1.51 |
| 14887 | 236351 |  |  | 338 | 424 | 25.36 | 4400 | 5400 | 22.73 | 4736 | 4960 | 4.73 |
| 14689 | 309696 |  |  | 169 | 141 | -16.63 | 6800 | 7900 | 16.18 | 1978 | 1580 | -20.14 |
| 14695 | 249533 |  |  | 169 | 226 | 33.63 | 1400 | 1600 | 14.29 | 4077 | 4310 | 5.73 |
| 14742 | 256498 |  |  | 254 | 302 | 19.05 | 1900 | 2100 | 10.53 | 5156 | 4690 | -9.03 |
| 14666 | 248738 |  |  | 338 | 416 | 22.99 | 3200 | 3800 | 18.75 | 5036 | 5070 | 0.68 |
| 14685 | 233125 |  |  | 338 | 393 | 16.19 | 17900 | 21000 | 17.32 | 8273 | 7690 | -7.05 |
| 14685B | 235603 |  |  | 338 | 374 | 10.57 | 19500 | 20400 | 4.62 | 8273 | 7930 | -4.15 |
| 14545 | 262996 |  |  | 338 | 409 | 20.92 | 1900 | 1900 | 0.00 | 3897 | 3980 | 2.14 |
| 14565 | 251730 |  |  | 254 | 259 | 2.10 | 2300 | 2600 | 13.04 | 3777 | 3800 | 0.61 |
| 14571 | 280246 |  |  | 338 | 312 | -7.76 | 10400 | 11100 | 6.73 | 3537 | 3170 | -10.38 |
| 14578 | 252478 |  |  | 254 | 324 | 27.72 | 18200 | 21300 | 17.03 | 5156 | 4630 | -10.20 |
| 14578B | 254628 |  |  | 254 | 330 | 30.09 | 19300 | 21100 | 9.33 | 4916 | 4430 | -9.88 |
| 14598 | 247476 |  |  | 507 | 569 | 12.15 | 1300 | 1500 | 15.38 | 4436 | 4330 | -2.40 |
| 14893 | 235696 |  |  | 338 | 379 | 12.05 | 1100 | 1100 | 0.00 | 5995 | 6030 | 0.58 |
| 14899 | 228824 |  |  | 338 | 366 | 8.21 | 200 | 200 | 0.00 | 5815 | 5850 | 0.60 |
| 14908 | 247383 |  |  | 423 | 479 | 13.29 | 800 | 900 | 12.50 | 5815 | 5910 | 1.63 |
| 14917 | 278656 |  |  | 254 | 309 | 21.81 | 1900 | 1900 | 0.00 | 4796 | 4580 | -4.50 |
| 14925 | 253647 |  |  | 338 | 353 | 4.37 | 1400 | 1500 | 7.14 | 5276 | 5090 | -3.52 |
| 14998 | 251309 |  |  | 338 | 412 | 21.81 | 1300 | 1300 | 0.00 | 4316 | 4460 | 3.33 |
| 15862 | 247149 |  |  | 254 | 327 | 28.90 | 800 | 800 | 0.00 | 4077 | 4050 | -0.65 |
| 15870 | 254348 |  |  | 254 | 234 | -7.76 | 1300 | 1400 | 7.69 | 4436 | 4460 | 0.53 |
| 15879 | 237098 |  |  | 338 | 373 | 10.28 | 1200 | 1200 | 0.00 | 5395 | 5450 | 1.01 |
| 15887 | 254441 |  |  | 338 | 402 | 18.85 | 3100 | 3300 | 6.45 | 5156 | 5100 | -1.08 |
| 15891 | 240184 |  |  | 338 | 382 | 12.94 | 1400 | 1400 | 0.00 | 5156 | 4920 | -4.57 |
| 15908 | 250001 |  |  | 254 | 288 | 13.53 | 2200 | 2200 | 0.00 | 4856 | 4740 | -2.39 |

## Project:

Comments:

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QA/QC Data - Comparison on ICP Metals and Whole Rock Analyses
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For drillhole 05CF240, changed northing from 6359873 to 6358873 to reflect drillhole location on provided maps.

| Sample <br> Id. | Whole Rock Si * <br> (ppm) | $\begin{gathered} \text { ICP } \\ \mathrm{Si} \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock Sr * <br> (ppm) | $\begin{gathered} \text { ICP } \\ \mathrm{Sr} \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | $\begin{gathered} \text { Leco } \\ \mathrm{S}\left(\text { Total) }{ }^{* *}\right. \\ (\mathrm{ppm}) \end{gathered}$ | $\begin{gathered} \text { ICP } \\ \mathrm{S} \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ | Whole Rock Ti * (ppm) | $\begin{gathered} \text { ICP } \\ \text { Ti } \\ (\mathrm{ppm}) \end{gathered}$ | Difference <br> (\%) ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15911 | 246822 |  |  | 338 | 335 | -0.96 | 900 | 900 | 0.00 | 5455 | 5430 | -0.47 |
| Maximum |  |  | NA |  |  | 41.3 |  |  | 23.4 |  |  | 9.29 |
| Minimum |  |  | NA |  |  | -16.6 |  |  | -12.5 |  |  | -20.1 |
| Mean |  |  | NA |  |  | 12.8 |  |  | 7.05 |  |  | -3.22 |
| Standard Deviation |  |  | NA |  |  | 12.6 |  |  | 6.66 |  |  | 6.05 |
| 10 Percentile |  |  | NA |  |  | -2.24 |  |  | 0 |  |  | -11.1 |
| 25 Percentile |  |  | NA |  |  | 3.48 |  |  | 0 |  |  | -8.04 |
| Median |  |  | NA |  |  | 12.9 |  |  | 7.14 |  |  | -2.23 |
| 75 Percentile |  |  | NA |  |  | 21.5 |  |  | 10.9 |  |  | 0.65 |
| 90 Percentile |  |  | NA |  |  | 29.1 |  |  | 15.5 |  |  | 3.53 |
| Interquartile Range (IQR) ${ }^{1}$ |  |  | NA |  |  | 18 |  |  | 10.9 |  |  | 8.69 |
| Variance |  |  | NA |  |  | 159 |  |  | 44.4 |  |  | 36.6 |
| Skewness |  |  | NA |  |  | -0.061 |  |  | 0.13 |  |  | -0.52 |
| Coefficient of Variation (CoV) ${ }^{2}$ |  |  | NA |  |  | 0.99 |  |  | 0.94 |  |  | -1.88 |
| Count |  |  | 0 |  |  | 59 |  |  | 59 |  |  | 59 |

${ }^{1}$ Interquartile Range (IQR) $=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
${ }^{2}$ Coefficient of Variation (CoV) = standard deviation divided by mean
${ }^{3}$ Difference (\%) = (ICP - Whole Rock) * 100 / Whole Rock

* Element calculated from Whole Rock XRF analysis
$\mathrm{Si}($ Whole Rock $)=\left(\mathrm{SiO}_{2}{ }^{*} 10000 * 28.09\right) /(28.09+2 \star 16)$ $\mathrm{Sr}($ Whole Rock $)=\left(\mathrm{SrO}^{*} 10000 * 87.62\right) /(87.62+16)$
Ti (Whole Rock) $=\left(\mathrm{TiO}_{2}{ }^{* 10000 * 47.9) /(47.9+2 \star 16)}\right.$
**S (Total) $=$ S (Leco \%) * 10000

| Sample <br> Id. | Carbonate Leach S (Sulphate) <br> (\%) | HCI Leachable S (Sulphate) <br> (\%) | $\begin{gathered} \text { RPD } \\ (\%) \end{gathered}$ | S (Sulphide) <br> (\% Leco) | \%S(Sulphide) Calculated from Carbonate Leach S (Sulphate) (\%) | $\begin{gathered} \text { RPD } \\ (\%) \end{gathered}$ | S (Sulphide) <br> (\% Leco) | \%S(Sulphide) Calculated from HCI Leachable S (Sulphate) <br> (\%) | RPD (\%) | (\% Leco/Calc)/ <br> S (Sulphide)/ <br> S (Total)*100 <br> (\%) | Carbonate Leach <br> S (Sulphate)/ <br> S (Total)*100 <br> (\%) | HCl Leachable <br> S (Sulphate)/ <br> S (Total)*100 <br> (\%) | $\begin{gathered} \text { S(BaSO4)/ } \\ \text { S (Total)*100 } \end{gathered}$ (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14018 | 0.02 | 0.005 | 120.00 | 0.69 | 0.78 | 12.24 | 0.69 | 0.795 | 14.14 | 86.25 | 2.50 | 0.63 | 3.40 |
| 14021 | 0.03 | 0.005 | 142.86 | 0.6 | 0.59 | 1.68 | 0.6 | 0.615 | 2.47 | 96.77 | 4.84 | 0.81 | 1.69 |
| 14036 | 0.02 | 0.005 | 120.00 | 1.39 | 1.45 | 4.23 | 1.39 | 1.465 | 5.25 | 94.56 | 1.36 | 0.34 | 0.85 |
| 14043 | 0.02 | 0.005 | 120.00 | 0.22 | 0.24 | 8.70 | 0.22 | 0.255 | 14.74 | 84.62 | 7.69 | 1.92 | 2.41 |
| 14060 | 0.74 | 0.71 | 4.14 | 0.62 | 0.57 | 8.40 | 0.62 | 0.6 | 3.28 | 47.33 | 56.49 | 54.20 | 0.64 |
| 14067 | 0.01 | 0.005 | 66.67 | 0.41 | 0.39 | 5.00 | 0.41 | 0.395 | 3.73 | 102.50 | 2.50 | 1.25 | 2.09 |
| 14076 | 0.01 | 0.005 | 66.67 | 0.76 | 0.76 | 0.00 | 0.76 | 0.765 | 0.66 | 98.70 | 1.30 | 0.65 | 1.36 |
| 14083 | 0.03 | 0.005 | 142.86 | 1.35 | 1.43 | 5.76 | 1.35 | 1.455 | 7.49 | 92.47 | 2.05 | 0.34 | 1.15 |
| 14099 | 0.03 | 0.005 | 142.86 | 0.28 | 0.31 | 10.17 | 0.28 | 0.335 | 17.89 | 82.35 | 8.82 | 1.47 | 6.15 |
| 14103 | 0.45 | 0.42 | 6.90 | 0.25 | 0.24 | 4.08 | 0.25 | 0.27 | 7.69 | 36.23 | 65.22 | 60.87 | 0.91 |
| 14130 | 0.03 | 0.005 | 142.86 | 0.29 | 0.26 | 10.91 | 0.29 | 0.285 | 1.74 | 100.00 | 10.34 | 1.72 | 4.33 |
| 14144 | 0.02 | 0.005 | 120.00 | 0.2 | 0.24 | 18.18 | 0.2 | 0.255 | 24.18 | 76.92 | 7.69 | 1.92 | 3.22 |
| 14148 | 0.02 | 0.005 | 120.00 | 0.04 | 0.12 | 100.00 | 0.04 | 0.135 | 108.57 | 28.57 | 14.29 | 3.57 | 10.45 |
| 14156 | 0.04 | 0.005 | 155.56 | 0.14 | 0.13 | 7.41 | 0.14 | 0.165 | 16.39 | 82.35 | 23.53 | 2.94 | 3.69 |
| 14162 | 0.02 | 0.005 | 120.00 | 0.12 | 0.11 | 8.70 | 0.12 | 0.125 | 4.08 | 92.31 | 15.38 | 3.85 | 9.65 |
| 14169 | 0.01 | 0.005 | 66.67 | 0.29 | 0.29 | 0.00 | 0.29 | 0.295 | 1.71 | 96.67 | 3.33 | 1.67 | 0.70 |
| 14232 | 0.005 | 0.005 | 0.00 | 0.14 | 0.145 | 3.51 | 0.14 | 0.145 | 3.51 | 93.33 | 3.33 | 3.33 | 2.79 |
| 14250 | 0.01 | 0.005 | 66.67 | 0.19 | 0.18 | 5.41 | 0.19 | 0.185 | 2.67 | 100.00 | 5.26 | 2.63 | 2.20 |
| 14260 | 0.01 | 0.005 | 66.67 | 0.34 | 0.33 | 2.99 | 0.34 | 0.335 | 1.48 | 100.00 | 2.94 | 1.47 | 1.23 |
| 14276 | 0.01 | 0.005 | 66.67 | 0.14 | 0.16 | 13.33 | 0.14 | 0.165 | 16.39 | 82.35 | 5.88 | 2.94 | 14.76 |
| 14295 | 0.005 | 0.005 | 0.00 | 0.41 | 0.435 | 5.92 | 0.41 | 0.435 | 5.92 | 93.18 | 1.14 | 1.14 | 0.48 |
| 14301 | 0.01 | 0.005 | 66.67 | 0.32 | 0.33 | 3.08 | 0.32 | 0.335 | 4.58 | 94.12 | 2.94 | 1.47 | 1.84 |
| 14323 | 0.005 | 0.005 | 0.00 | 0.13 | 0.145 | 10.91 | 0.13 | 0.145 | 10.91 | 86.67 | 3.33 | 3.33 | 4.18 |
| 14332 | 0.01 | 0.005 | 66.67 | 0.26 | 0.25 | 3.92 | 0.26 | 0.255 | 1.94 | 100.00 | 3.85 | 1.92 | 1.61 |
| 14345 | 0.005 | 0.005 | 0.00 | 0.52 | 0.515 | 0.97 | 0.52 | 0.515 | 0.97 | 100.00 | 0.96 | 0.96 | 0.80 |
| 14348 | 0.01 | 0.005 | 66.67 | 0.45 | 0.43 | 4.55 | 0.45 | 0.435 | 3.39 | 102.27 | 2.27 | 1.14 | 0.95 |
| 14797 | 0.005 | 0.005 | 0.00 | 0.05 | 0.075 | 40.00 | 0.05 | 0.075 | 40.00 | 62.50 | 6.25 | 6.25 | 5.23 |
| 14808 | 0.005 | 0.005 | 0.00 | 0.16 | 0.175 | 8.96 | 0.16 | 0.175 | 8.96 | 88.89 | 2.78 | 2.78 | 2.32 |
| 14816 | 0.005 | 0.01 | 66.67 | 0.46 | 0.455 | 1.09 | 0.46 | 0.45 | 2.20 | 100.00 | 1.09 | 2.17 | 0.91 |
| 14828 | 0.02 | 0.005 | 120.00 | 0.1 | 0.11 | 9.52 | 0.1 | 0.125 | 22.22 | 76.92 | 15.38 | 3.85 | 12.87 |
| 14844 | 0.005 | 0.01 | 66.67 | 0.2 | 0.205 | 2.47 | 0.2 | 0.2 | 0.00 | 95.24 | 2.38 | 4.76 | 3.98 |
| 14680 | 0.01 | 0.005 | 66.67 | 0.2 | 0.21 | 4.88 | 0.2 | 0.215 | 7.23 | 90.91 | 4.55 | 2.27 | 2.85 |
| 14871 | 0.02 | 0.005 | 120.00 | 0.32 | 0.35 | 8.96 | 0.32 | 0.365 | 13.14 | 86.49 | 5.41 | 1.35 | 0.57 |
| 14887 | 0.01 | 0.03 | 100.00 | 0.42 | 0.43 | 2.35 | 0.42 | 0.41 | 2.41 | 95.45 | 2.27 | 6.82 | 1.90 |
| 14689 | 0.01 | 0.005 | 66.67 | 0.69 | 0.67 | 2.94 | 0.69 | 0.675 | 2.20 | 101.47 | 1.47 | 0.74 | 0.31 |
| 14695 | 0.005 | 0.005 | 0.00 | 0.13 | 0.135 | 3.77 | 0.13 | 0.135 | 3.77 | 92.86 | 3.57 | 3.57 | 2.99 |
| 14742 | 0.005 | 0.005 | 0.00 | 0.19 | 0.185 | 2.67 | 0.19 | 0.185 | 2.67 | 100.00 | 2.63 | 2.63 | 2.20 |
| 14666 | 0.01 | 0.005 | 66.67 | 0.31 | 0.31 | 0.00 | 0.31 | 0.315 | 1.60 | 96.88 | 3.13 | 1.56 | 2.61 |
| 14685 | 0.01 | 0.005 | 66.67 | 1.8 | 1.78 | 1.12 | 1.8 | 1.785 | 0.84 | 100.56 | 0.56 | 0.28 | 0.58 |
| 14685B | 0.01 | 0.005 | 66.67 | 1.8 | 1.94 | 7.49 | 1.8 | 1.945 | 7.74 | 92.31 | 0.51 | 0.26 | 0.43 |
| 14545 | 0.01 | 0.005 | 66.67 | 0.13 | 0.18 | 32.26 | 0.13 | 0.185 | 34.92 | 68.42 | 5.26 | 2.63 | 11.00 |
| 14565 | 0.005 | 0.005 | 0.00 | 0.24 | 0.225 | 6.45 | 0.24 | 0.225 | 6.45 | 104.35 | 2.17 | 2.17 | 1.82 |
| 14571 | 0.02 | 0.005 | 120.00 | 1.03 | 1.02 | 0.98 | 1.03 | 1.035 | 0.48 | 99.04 | 1.92 | 0.48 | 1.01 |
| 14578 | 0.02 | 0.005 | 120.00 | 1.82 | 1.8 | 1.10 | 1.82 | 1.815 | 0.28 | 100.00 | 1.10 | 0.27 | 0.80 |
| 14578B | 0.03 | 0.005 | 142.86 | 1.91 | 1.9 | 0.52 | 1.91 | 1.925 | 0.78 | 98.96 | 1.55 | 0.26 | 0.97 |
| 14598 | 0.01 | 0.005 | 66.67 | 0.13 | 0.12 | 8.00 | 0.13 | 0.125 | 3.92 | 100.00 | 7.69 | 3.85 | 3.22 |
| 14893 | 0.005 | 0.04 | 155.56 | 0.08 | 0.105 | 27.03 | 0.08 | 0.07 | 13.33 | 72.73 | 4.55 | 36.36 | 9.50 |
| 14899 | 0.005 | 0.005 | 0.00 | 0.02 | 0.015 | 28.57 | 0.02 | 0.015 | 28.57 | 100.00 | 25.00 | 25.00 | 41.82 |
| 14908 | 0.005 | 0.005 | 0.00 | 0.07 | 0.075 | 6.90 | 0.07 | 0.075 | 6.90 | 87.50 | 6.25 | 6.25 | 20.91 |
| 14917 | 0.005 | 0.005 | 0.00 | 0.16 | 0.185 | 14.49 | 0.16 | 0.185 | 14.49 | 84.21 | 2.63 | 2.63 | 9.90 |
| 14925 | 0.005 | 0.005 | 0.00 | 0.12 | 0.135 | 11.76 | 0.12 | 0.135 | 11.76 | 85.71 | 3.57 | 3.57 | 5.97 |
| 14998 | 0.005 | 0.005 | 0.00 | 0.12 | 0.125 | 4.08 | 0.12 | 0.125 | 4.08 | 92.31 | 3.85 | 3.85 | 4.82 |
| 15862 | 0.005 | 0.005 | 0.00 | 0.03 | 0.075 | 85.71 | 0.03 | 0.075 | 85.71 | 37.50 | 6.25 | 6.25 | 7.84 |
| 15870 | 0.02 | 0.005 | 120.00 | 0.09 | 0.11 | 20.00 | 0.09 | 0.125 | 32.56 | 69.23 | 15.38 | 3.85 | 19.30 |
| 15879 | 0.02 | 0.005 | 120.00 | 0.09 | 0.1 | 10.53 | 0.09 | 0.115 | 24.39 | 75.00 | 16.67 | 4.17 | 15.68 |
| 15887 | 0.01 | 0.005 | 66.67 | 0.29 | 0.3 | 3.39 | 0.29 | 0.305 | 5.04 | 93.55 | 3.23 | 1.61 | 3.37 |
| 15891 | 0.02 | 0.005 | 120.00 | 0.09 | 0.12 | 28.57 | 0.09 | 0.135 | 40.00 | 64.29 | 14.29 | 3.57 | 22.40 |
| 15908 | 0.02 | 0.005 | 120.00 | 0.2 | 0.2 | 0.00 | 0.2 | 0.215 | 7.23 | 90.91 | 9.09 | 2.27 | 2.85 |

Sampled by MDAG on Feb 7 '07.

| Carbonate Leach S (Sulphate) <br> (\%) | HCl Leachable S (Sulphate) <br> (\%) | RPD <br> (\%) | S (Sulphide) <br> (\% Leco) | \%S(Sulphide) Calculated from Carbonate Leach S (Sulphate) (\%) | RPD <br> (\%) | S (Sulphide) <br> (\% Leco) | \%S(Sulphide) Calculated from HCl Leachable S (Sulphate) <br> (\%) | RPD (\%) | (\% Leco/Calc)/ <br> S (Sulphide)/ <br> S (Total)*100 <br> (\%) | Carbonate Leach <br> S (Sulphate)/ <br> S (Total)*100 <br> (\%) | HCl Leachable S (Sulphate)/ <br> S (Total)*100 <br> (\%) | $\begin{gathered} \text { S(BaSO4)/ } \\ \text { S (Total)*100 } \end{gathered}$ <br> (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.01 | 0.005 | 66.67 | 0.07 | 0.08 | 13.33 | 0.07 | 0.085 | 19.35 | 77.78 | 11.11 | 5.56 | 11.62 |
|  |  | 156 |  |  | 100 |  |  | 109 | 104.00 | 65.20 | 60.90 | 41.80 |
|  |  | 0 |  |  | 0 |  |  | 1.4E-14 | 28.60 | 0.51 | 0.26 | 0.31 |
|  |  | 70.3 |  |  | 11.2 |  |  | 12.6 | 87 | 7.67 | 5.29 | 5.39 |
|  |  | 52.4 |  |  | 17.7 |  |  | 19 | 16.9 | 11.5 | 11.3 | 7.2 |
|  |  | 0 |  |  | 0.97 |  |  | 0.94 | 67.6 | 1.27 | 0.45 | 0.69 |
|  |  | 2.07 |  |  | 2.96 |  |  | 2.44 | 82.4 | 2.33 | 1.3 | 1.08 |
|  |  | 66.7 |  |  | 5.92 |  |  | 5.92 | 92.5 | 3.57 | 2.27 | 2.79 |
|  |  | 120 |  |  | 10.9 |  |  | 14.6 | 99.5 | 7.69 | 3.85 | 6.06 |
|  |  | 143 |  |  | 27.3 |  |  | 29.4 | 100 | 15.4 | 6.25 | 13.2 |
|  |  | 118 |  |  | 7.95 |  |  | 12.2 | 17.2 | 5.37 | 2.55 | 4.99 |
|  |  | 2743 |  |  | 312 |  |  | 362 | 287 | 131 | 128 | 51.9 |
|  |  | -0.11 |  |  | 3.71 |  |  | 3.4 | -1.87 | 3.72 | 3.99 | 2.89 |
|  |  | 0.74 |  |  | 1.58 |  |  | 1.51 | 0.19 | 1.49 | 2.14 | 1.34 |
|  |  | 59 |  |  | 59 |  |  | 59 | 59 | 59 | 59 | 59 |

Comments:

Schaft Creek
Copper Fox Metals Inc.
QA/QC Data - Sulphur and NP Species
Sampled by MDAG on Feb $7^{\prime} 07$.

| $\begin{gathered} \text { Ratio } \\ \text { NP / } \\ \text { Inorganic CaNP } \end{gathered}$ | Ratio NP / (Ca) CaNP | $\begin{gathered} \text { Ratio } \\ \mathrm{NP} / \\ (\mathrm{Ca}+\mathrm{Mg}) \mathrm{CaNP} \end{gathered}$ | Ratio Inorganic CaNP / (Ca) CaNP | Ratio Inorganic CaNP (Ca+Mg) CaNP |
| :---: | :---: | :---: | :---: | :---: |
| 1.32 | 0.94 | 0.47 | 0.72 | 0.36 |
| 1.08 | 0.98 | 0.62 | 0.90 | 0.57 |
| 1.20 | 1.07 | 0.59 | 0.89 | 0.49 |
| 2.20 | 1.14 | 0.35 | 0.52 | 0.16 |
| 1.80 | 0.52 | 0.25 | 0.29 | 0.14 |
| 1.66 | 0.76 | 0.28 | 0.46 | 0.17 |
| 1.12 | 0.61 | 0.31 | 0.55 | 0.28 |
| 1.08 | 0.74 | 0.43 | 0.68 | 0.39 |
| 1.01 | 1.06 | 0.73 | 1.05 | 0.72 |
| 1.17 | 1.16 | 0.67 | 0.99 | 0.58 |
| 0.91 | 1.39 | 0.85 | 1.53 | 0.93 |
| 1.02 | 1.24 | 0.82 | 1.21 | 0.80 |
| 1.07 | 1.47 | 0.88 | 1.38 | 0.82 |
| 1.00 | 1.18 | 0.77 | 1.18 | 0.77 |
| 1.15 | 1.57 | 0.88 | 1.37 | 0.77 |
| 1.13 | 1.10 | 0.86 | 0.98 | 0.76 |
| 1.22 | 1.34 | 0.86 | 1.10 | 0.70 |
| 1.27 | 1.16 | 0.66 | 0.92 | 0.52 |
| 1.19 | 1.32 | 0.75 | 1.11 | 0.63 |
| 2.30 | 0.44 | 0.27 | 0.19 | 0.12 |
| 1.39 | 1.14 | 0.69 | 0.82 | 0.49 |
| 1.05 | 1.49 | 0.95 | 1.42 | 0.91 |
| 1.04 | 0.78 | 0.55 | 0.75 | 0.53 |
| 1.55 | 1.12 | 0.75 | 0.73 | 0.48 |
| 2.17 | 1.24 | 0.74 | 0.57 | 0.34 |
| 1.18 | 1.10 | 0.57 | 0.93 | 0.48 |
| 1.08 | 1.32 | 0.80 | 1.23 | 0.74 |
| 0.93 | 1.41 | 0.91 | 1.51 | 0.98 |
| 5.85 | 1.60 | 0.87 | 0.27 | 0.15 |
| 1.01 | 1.32 | 0.78 | 1.30 | 0.77 |
| 1.94 | 1.06 | 0.33 | 0.55 | 0.17 |
| 1.18 | 0.99 | 0.60 | 0.84 | 0.50 |
| 1.43 | 1.04 | 0.54 | 0.72 | 0.37 |
| 1.22 | 0.92 | 0.52 | 0.76 | 0.42 |
| 0.97 | 0.97 | 0.68 | 1.00 | 0.70 |
| 1.04 | 1.15 | 0.71 | 1.10 | 0.68 |
| 1.27 | 1.21 | 0.52 | 0.95 | 0.41 |
| 1.53 | 0.96 | 0.50 | 0.63 | 0.33 |
| 1.49 | 1.35 | 0.57 | 0.91 | 0.38 |
| 1.45 | 1.38 | 0.54 | 0.96 | 0.37 |
| 1.54 | 0.81 | 0.50 | 0.52 | 0.33 |
| 1.27 | 1.19 | 0.83 | 0.93 | 0.65 |
| 1.19 | 1.18 | 0.67 | 0.98 | 0.56 |
| 1.06 | 1.06 | 0.72 | 1.00 | 0.68 |
| 1.07 | 1.13 | 0.76 | 1.05 | 0.71 |
| 1.61 | 0.92 | 0.44 | 0.57 | 0.27 |
| 1.28 | 1.07 | 0.51 | 0.83 | 0.40 |
| 1.48 | 0.92 | 0.31 | 0.62 | 0.21 |
| 1.57 | 0.79 | 0.39 | 0.50 | 0.25 |
| 1.45 | 1.14 | 0.50 | 0.79 | 0.34 |
| 1.34 | 0.91 | 0.47 | 0.68 | 0.35 |
| 1.19 | 1.04 | 0.62 | 0.87 | 0.52 |
| 1.17 | 1.23 | 0.73 | 1.06 | 0.63 |
| 1.05 | 1.30 | 0.80 | 1.24 | 0.76 |
| 1.08 | 0.98 | 0.60 | 0.91 | 0.55 |
| 1.27 | 0.92 | 0.56 | 0.73 | 0.45 |
| 1.10 | 1.00 | 0.64 | 0.91 | 0.58 |
| 1.21 | 1.07 | 0.64 | 0.89 | 0.53 |

Project:
Client:
Data:
Comments:
chaft Creek
Copper Fox Metals Inc.
QA/QC Data - Sulphur and NP Species
Sampled by MDAG on Feb 7'07.

| Sample <br> Id. | $\begin{gathered} \text { Ratio } \\ \text { NP / } \\ \text { Inorganic CaNP } \end{gathered}$ | Ratio NP / (Ca) CaNP | $\begin{gathered} \text { Ratio } \\ \mathrm{NP} / \\ (\mathrm{Ca}+\mathrm{Mg}) \mathrm{CaNP} \end{gathered}$ | Ratio Inorganic CaNP / (Ca) CaNP | Ratio Inorganic CaNP (Ca+Mg) CaNP |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 15911 | 1.35 | 1.05 | 0.50 | 0.78 | 0.37 |
| Maximum | 5.85 | 1.60 | 0.95 | 1.53 | 0.98 |
| Minimum | 0.91 | 0.44 | 0.25 | 0.19 | 0.12 |
| Mean | 1.37 | 1.09 | 0.62 | 0.88 | 0.51 |
| Standard Deviation | 0.67 | 0.24 | 0.18 | 0.3 | 0.22 |
| 10 Percentile | 1.02 | 0.79 | 0.35 | 0.52 | 0.2 |
| 25 Percentile | 1.08 | 0.97 | 0.5 | 0.7 | 0.36 |
| Median | 1.2 | 1.1 | 0.62 | 0.9 | 0.5 |
| 75 Percentile | 1.45 | 1.24 | 0.76 | 1.05 | 0.69 |
| 90 Percentile | 1.69 | 1.39 | 0.86 | 1.25 | 0.77 |
| Interquartile Range (IQR) ${ }^{1}$ | 0.37 | 0.27 | 0.25 | 0.35 | 0.33 |
| Variance | 0.45 | 0.056 | 0.033 | 0.088 | 0.047 |
| Skewness | 5.47 | -0.33 | -0.24 | 0.039 | 0.089 |
| Coefficient of Variation (CoV) ${ }^{2}$ | 0.49 | 0.22 | 0.29 | 0.34 | 0.43 |
| Count | 59 | 59 | 59 | 59 | 59 |


[^0]:    ${ }^{1}$ Interquartile Range (IQR) $=75^{\text {th }}$ percentile minus $25^{\text {th }}$ percentile
    ${ }^{2}$ Coefficient of Variation (CoV) = standard deviation divided by mean
    NOTE: If data was reported as < detection limit half the detection limit is shown in italics and was used in subsequent calculations.
    Total CaNP $=\% \mathrm{C} * 10 * 100.09 / 12.01$
    Inorganic CaNP $=\% \mathrm{CO}_{2}$ * 10 * 100.09 / 44.01
    (Ca) CaNP $=(\mathrm{Ca}(\mathrm{ppm}) * 100.09 / 40.08) / 1000$
    $(\mathrm{Ca}+\mathrm{Mg}) \mathrm{CaNP}=((\mathrm{Ca}(\mathrm{ppm}) * 100.09 / 40.08)+(\mathrm{Mg}(\mathrm{ppm}) * 100.09 / 24.31)) / 1000$
    TNNP = NP - TAP
    Adjusted TNNP = Available NP - TAP
    SNNP = NP - SAP
    Adjusted SNNP = Available NP - SAP
    PNNP = NP - PAP
    Adjusted PNNP = Available NP - PAP

[^1]:    Difference

